

Electronic supplementary materials

for <https://doi.org/10.1631/jzus.A2300026>

Bifurcation control of solid angle car-following model through a time-delay feedback method

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Eqs. (S1)–(S13)

Section S1 Specific solution process of the controlled SAM

Considering the periodic boundary, Eq. (13) is simplified to the matrix form:

$$\begin{pmatrix} \dot{\eta} \\ \dot{\xi} \end{pmatrix} = \begin{pmatrix} \delta \mathbf{I} & -\beta \mathbf{A} \\ \mathbf{I} & \mathbf{O} \end{pmatrix} \begin{pmatrix} \eta \\ \xi \end{pmatrix} + \begin{pmatrix} -M \varepsilon \mathbf{I} & \mathbf{O} \\ \mathbf{O} & \mathbf{O} \end{pmatrix} \begin{pmatrix} \eta(t-\tau) \\ \xi(t-\tau) \end{pmatrix} \quad (\text{S1})$$

where $\eta = (\eta_1(t), \eta_2(t), \dots, \eta_N(t))^T$, $\xi = (\xi_1(t), \xi_2(t), \dots, \xi_N(t))^T$; \mathbf{O} is the zero matrix of $N \times N$. The form of matrix \mathbf{A} is as follows:

$$\mathbf{A} = \begin{pmatrix} 1 & -1 & 0 & \dots & 0 & 0 \\ 0 & 1 & -1 & \dots & 0 & 0 \\ \vdots & \vdots & \vdots & & \vdots & \vdots \\ 0 & 0 & 0 & \dots & 1 & -1 \\ -1 & 0 & 0 & \dots & 0 & 1 \end{pmatrix} \quad (\text{S2})$$

The corresponding characteristic equation of Eq. (20) can be derived as follows:

$$\left[\lambda^2 - \delta \lambda + M \varepsilon e^{-\tau \lambda} \lambda + \beta \right]^N - [\beta]^N = 0 \quad (\text{S3})$$

Therefore, we can obtain:

$$\left[\frac{\lambda^2 - \delta \lambda + M \varepsilon e^{-\tau \lambda} \lambda + \beta}{\beta} \right]^N = 1 \quad (\text{S4})$$

The transformation of Eq. (23) can obtain:

$$\lambda^2 - \delta\lambda + M\varepsilon e^{-\tau\lambda} \lambda + \beta = \beta \left(\cos \frac{2k\pi}{N} + i \sin \frac{2k\pi}{N} \right) \quad (\text{S5})$$

where $k \in \{1, 2, \dots, N\}$ is the wave number of the oscillation.

Inserting $\lambda = \mu + i\omega$ into Eq. (24):

$$\begin{cases} \mu^2 - \omega^2 - \delta\mu + M\varepsilon e^{-\tau\mu} (\mu c_\tau + \omega s_\tau) + \beta = \beta c_k \\ 2\mu\omega - \varepsilon\omega + M\varepsilon e^{-\tau\mu} (\omega c_\tau - \mu s_\tau) + \beta = \beta s_k \end{cases} \quad (\text{S6})$$

where $c_k = \cos \frac{2k\pi}{N}$, $s_k = \sin \frac{2k\pi}{N}$, $c_\tau = \cos \tau_2 \omega$, $s_\tau = \sin \tau_2 \omega$.

Section S2 Specific improvement procedures of definite integral method

Step 1 Inserting $\lambda = i\omega$ into Eq. (17) and separating the real part of $i^{-n} f(i\omega)$ yields:

$$R(\omega) = \text{Re}(i^{-n} f(i\omega)) = \omega^2 - M\varepsilon\omega s_\tau - \beta + \beta c_k \quad (\text{S7})$$

where n represents the highest degree of the characteristic equation Eq. (24).

Step 2 According to Eq. (26), all positive roots $W = \{\omega_1, \omega_2, \dots, \omega_m\}$ of $R(\omega) = 0$ exist. Take the maximum value of the set W as ω_{\max} , and choose any $T_0 > \omega_{\max}$ as the upper limit of the definite integral.

Step 3 Considering $\Re(\omega) = \text{Re}(f'(i\omega) / f(i\omega))$, the integrand $\Re(\omega)$ is transformed into:

$$\begin{aligned} \Re(\omega) &= \text{Re} \left(\frac{f'(i\omega)}{f(i\omega)} \right) \\ &= \frac{\text{Re}(f'(i\omega))\text{Re}(f(i\omega)) + \text{Im}(f'(i\omega))\text{Im}(f(i\omega))}{[\text{Re}(f(i\omega))]^2 + [\text{Im}(f(i\omega))]^2} \end{aligned} \quad (\text{S8})$$

where the specific expression of the real part $\text{Re}(f'(i\omega))$ and imaginary part $\text{Im}(f'(i\omega))$ of $f'(i\omega)$ are as follows:

$$\text{Re}(f'(i\omega)) = -\delta + M\varepsilon c_\tau - M\varepsilon\tau s_\tau \quad (\text{S9})$$

$$\text{Im}(f'(i\omega)) = 2\omega - M\varepsilon s_\tau - M\varepsilon\tau\omega c_\tau \quad (\text{S10})$$

where the specific expression of the real part $\text{Re}(f(i\omega))$ and imaginary part $\text{Im}(f(i\omega))$ of $f(i\omega)$ are as follows:

$$\text{Re}(f(i\omega)) = -\omega^2 + M\varepsilon\omega s_\tau + \beta - \beta c_k \quad (\text{S11})$$

$$\text{Im}(f(i\omega)) = -\delta\omega + M\varepsilon\omega c_\tau - \beta s_k \quad (\text{S12})$$

Step 4 The following definite integrals are introduced into the product function T_0 in step 2 and the

product function $\Re(\omega)$ in step 3, respectively, and yield:

$$F(0, T_0)_k = \int_0^{T_0} \Re(\omega) d\omega \quad (\text{S13})$$

For every k and $k \neq N$, the total number $II_k(\tau)$ of eigenvalues with positive real part is:

$$II_k(\tau) = \text{round}\left(\frac{n}{2} - \frac{F(0, T_0)_k}{\pi}\right) \quad (\text{S14})$$

Step 5 In summary, if $II(\tau) = 0$ is stable under the control of time delay τ . Otherwise, unstable oscillation of the system occurs.