



Review:

A survey of drag and heat reduction in supersonic flows by a counterflowing jet and its combinations^{*}

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Abstract: Drag reduction and thermal protection is very important for hypersonic vehicles, and a counterflowing jet and its combinations is one of the most promising drag and heat release reduction strategies. In the current survey, research progress on the drag and heat release reduction induced by a counterflowing jet and its combinations is summarized. Three combinatorial configurations are considered, namely the combination of the counterflowing jet and a forward-facing cavity, the combination of the counterflowing jet and an aerospike, and the combination of the counterflowing jet and energy deposition. In conclusion, some recommendations are provided, especially for jet instability protection, for the tradeoff between drag and heat release reductions, and for the critical points for the operational and geometric parameters in the flow mode transition.

Key words: Hypersonic vehicle, Drag reduction, Heat release reduction, Counterflowing jet, Forward-facing cavity, Energy deposition

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1 Introduction

Drag reduction and thermal protection on the surface of a hypersonic vehicle becomes especially important when the vehicle enters the atmosphere at high speed (Ho and Paull, 2006), as shown in Fig. 1 (Pezzella, 2012). Such vehicles include hypervelocity projectiles, reentry vehicles (Ohtake, 1998; Huang *et al.*, 2012b), and hypersonic aircraft (Huang *et al.*, 2011). Fig. 1 shows the heat flux comparison for three typical reentry loading environments. It is clearly shown that the maximum heat flux for the reusable first stage is the lowest, but even that is above 100 kW/m^2 . Therefore, damage on the nose of

the vehicle induced by high temperature and high pressure must be prevented.

The wave drag force is more than half of the total drag force when the vehicle flies at hypersonic speed, and increases sharply with increasing freestream Mach number. Therefore, the overall drag reduction is focused on the reduction of the wave drag force (Bushnell, 2004). At the same time, the maximum heat flux usually occurs at the stagnation point of the nose of the vehicle, and it has a strong relationship with the value of the wave drag force. Therefore, most attention should be paid to the physical parameter distributions of the nose, i.e., the wall static pressure and the heat flux.

Recently, many techniques, for example, concentrated energy deposition along the stagnation streamline, a retractable aerospike ahead of the blunt body, and a counterflowing jet in the stagnation zone of the blunt body (Gerdroodbary and Hosseinalipour, 2010), have been proposed to reduce the drag and heat release, and they can be categorized into passive

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and active approaches according as to whether the method can be controlled or not. The passive approach is the retractable aerospike installed ahead of the blunt body employed to reduce the intensity of the shock wave. Ahmed and Qin (2011) provided a detailed review on the spiked hypersonic vehicle, and they also pointed out that some areas in this field need further investigation. Active approaches are energy deposition along the stagnation streamline and a counterflowing jet in the stagnation zone of the blunt body. Because of the difficulty of its engineering implementation, the investigation of the energy deposition method has remained a theoretical one. Knight (2008) has reviewed the research on the aerodynamic drag reduction induced by energy deposition. In the counterflowing jet flow field, small scale vortical structures mainly occur in the jet column, and the large scale vortices develop gradually in a recirculation zone when the jet terminates through a Mach disk and reverses its orientation as a conical free shear layer. The recirculation zone ahead of the blunt body has a great impact on heat flux reduction, and on reduction of the drag force.

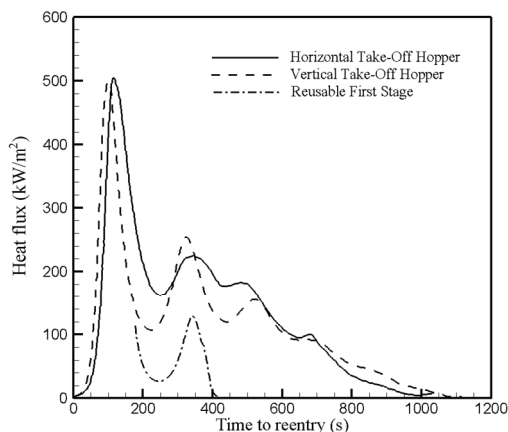


Fig. 1 Heat flux comparison for three typical reentry loading environments. Reprinted from (Pezzella, 2012), Copyright 2012, with permission from Elsevier Masson SAS

To the best of the author's knowledge, research on the drag and heat release reduction induced by a counterflowing jet and its combinations has not been summarized in the open literature, and it is very important to explore the information in its drag and heat release reduction mechanism. As is well known, there are many influencing factors in the transverse

injection flow field (Karagozian, 2010; Huang and Yan, 2013), namely the operational and geometric parameters, and variation of these parameters will result in some reduction in the drag force and heat flux as well.

In the current survey, progress in research on a counterflowing jet and its combinations has been reviewed. These combinations include the combination of the counterflowing jet and an aerospike, the combination of the counterflowing jet and energy deposition, and the combination of the counterflowing jet and a forward-facing cavity. Finally, some recommendations on the areas requiring urgent investigation have been made.

2 Counterflowing jet

The flowfield around a blunt body with a counterflowing jet was categorized by Finley (1966) into three conditions, namely steady, unsteady, and transitional, and these are the same as are observed around a blunt body with an aerospike (Feszty *et al.*, 2004; Panaras and Drikakis, 2009). Venukumar *et al.* (2006) conducted an experiment on the drag force reduction induced by a counterflowing jet, and a reduction of about 45% was possible for larger values of the jet pressure ratio (Fig. 2). In their study, the jet pressure ratio (PR) is defined as the ratio of the jet total pressure to the pitot pressure of the test flow, namely,

$$PR = P_{0j} / P_{0\infty}, \quad (1)$$

where P_{0j} and $P_{0\infty}$ are the total pressures of the jet and the test flow, respectively.

However, they only considered steady flow fields with jet pressure ratios much larger than the critical value, which is 6.5 when the freestream Mach number is 8.0. The static pressure is 220 Pa and the static temperature is 150 K. The critical value of the jet pressure ratio is employed to categorise the counterflowing jet flow fields, and the counterflowing jet flow field is steady when the jet pressure ratio is larger than that critical value. Further, the freestream enthalpy has a great impact on the drag force reduction as well, and the drag force reduction

increases with the increase in stagnation enthalpy (Fig. 3) (Kulkarni and Reddy, 2008). However, the physical mechanism is still not clear, in particular how the freestream enthalpy affects the drag force is not fully understood and it needs to be explored further. At the same time, the jet stagnation temperature has proved to be important in drag force reduction (Ganiev *et al.*, 2000), and the drag force reduction value varies with it. The influence of the total pressure ratio on the heat release reduction of a blunt body with counterflowing jets has been analyzed experimentally by Hayashi *et al.* (2006), and the total pressure ratio is defined as the ratio of the jet total pressure to the freestream total pressure. In their experiments, steady and unsteady conditions are both

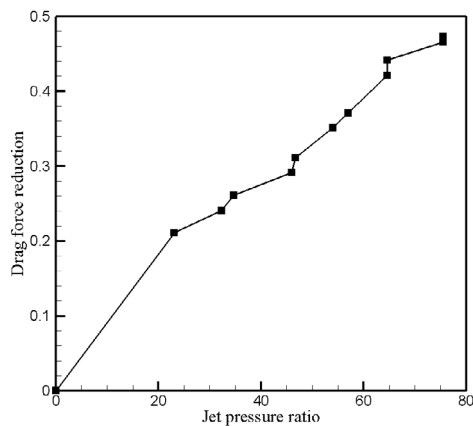


Fig. 2 Drag force reduction for different jet pressure ratios of the Mach 8 test flow. Reprinted from (Venukumar *et al.*, 2006), Copyright 2006, with permission from AIP Publishing LLC

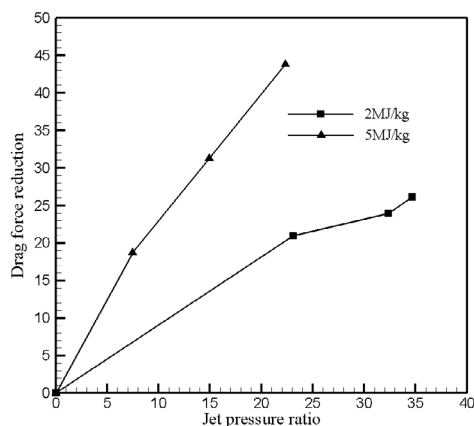


Fig. 3 Comparison of drag force reduction for Mach 8 flow with different freestream enthalpies. Reprinted from (Kulkarni and Reddy, 2008), Copyright 2008, with permission from AIP Publishing LLC

taken into consideration. The results obtained show that the unsteady condition has no visible impact on the heat release reduction, but the heat release reduction increases with the increase of the total pressure ratio at the steady condition. Li and Eri (2007) and Wang Z.Q. *et al.* (2010) have analyzed numerically the influences of the pressure ratio and the counterflowing nozzle diameter ratio on the aerodynamic heating reduction.

The heat release reduction of a blunt body with micro-jets has been investigated experimentally by Sriram and Jagadeesh (2009) with effective area kept constant. Their experiments have been performed at freestream Mach number 5.9 with a stagnation enthalpy of 1.84 MJ/kg. The obtained results show that the cooling performance of an array of closely spaced micro-jets is much better than that of a corresponding single jet over nearly all the whole surface, and a heavier injection gas gives a better cooling performance. This phenomenon is the same as the effect of molecular weight on the mixing improvement in transverse injection flow fields (Huang *et al.*, 2014a). Venukumar and Reddy (2007) have conducted experiments on the effect of the injection species on aerodynamic drag reduction; however, the overall drag force reduction performance has not been compared. That is to say that the influence of injection species on the drag force reduction has not been evaluated quantitatively and a maximum of 29% reduction in the drag coefficient has been obtained with a supersonic counterflowing jet.

The drag force reductions on the blunt cone flare and large blunt cone flare bodies with a counterflowing jet have been studied numerically by Aruna and Anjalidevi (2012); the counterflowing jet is found to be very effective for the reduction of pressure drag, skin friction drag, and total drag force. Meyer *et al.* (2001), Tian and Yan (2008), and Wang X. *et al.* (2010) have also validated the drag force reduction mechanism of the counterflowing jet numerically. At the same time, the minimum counterflowing jet ejection has been successfully employed in an Apollo command module (Zheng *et al.*, 2012). Lu and Liu (2012a) have investigated numerically the influence of the angle of attack on a hemisphere nose-tip with a counterflowing jet and they found that the cruise angle of attack has a great impact on the flow field parameters (Huang and Wang, 2009),

aerodynamic force, and surface heat flux distribution, and that the parameter distributions were asymmetric. A new parameter R_{PA} was proposed by Rong and Liu (2010) and Rong (2013) to analyze the influence of a counterflowing jet on flow field properties as well as on the aerodynamic force of the blunt body, and it has been shown to depend on the intensity of the counterflowing jet. Its definition is as follows:

$$R_{PA} = \frac{P_{0j}}{P_{0\infty}} \frac{A_j}{A_{base}} = \frac{P_{0j}}{P_{0\infty}} \frac{R_j^2}{R^2}, \quad (2)$$

where R_j is the radius of the jet exit, and R is the radius of the blunt body. A_j and A_{base} are the areas of the jet orifice exit and the base plane of the blunt body, respectively.

Zhou and Ji (2014) have investigated numerically the influences of the jet pressure, the nozzle size of the jet, and the angle of attack on the drag force reduction of a spherical body with a sonic counterflowing jet from its stagnation point. The freestream Mach number was set to be 2.5. In their research, a critical jet pressure ratio (P_{crit}) was obtained as well, and it varies approximately linearly with the jet nozzle exit size (Fig. 4). In Fig. 4, D is the diameter of the jet nozzle exit in millimeters. The jet pressure ratio is as defined by Venukumar *et al.* (2006). A flow mode transition occurs at this critical point, from an unsteady oscillatory motion mode to a nearly steady motion mode (Fig. 5). The maximum overall drag reduction usually happens at the unsteady oscillatory motion mode. This conclusion is consistent with that obtained with plasma injection by Fomin *et al.* (2002), but the flow field properties induced by the plasma injection and the hot-gas injection are different (Ganiev *et al.*, 2000). This may imply that the variation tendency of the drag reduction is not consistent with that of the heat release reduction, and that there must be a tradeoff in the design of the thermal protection system. The multi-objective design optimization (MDO) approach, as well as the data mining method (Huang *et al.*, 2010; 2012a), is suitable to solve this problem, and it has already been applied successfully to the blunt body with aerospike (Ahmed and Qin, 2010; 2012), as well as to the transverse injection flow field (Huang, 2014; Huang *et al.*, 2014b), supersonic nozzle (Huang *et al.*, 2013a), and cavity flameholder

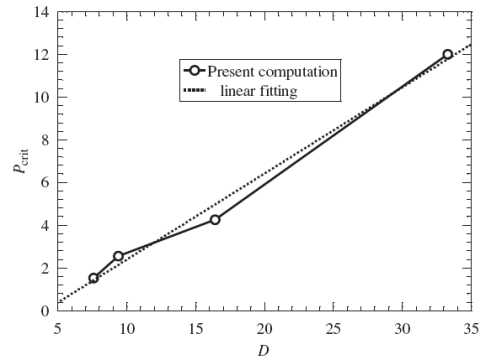


Fig. 4 Variation of critical jet pressure ratio with the jet nozzle exit size. D is in millimeter. Reprinted from (Zhou and Ji, 2014), Copyright 2014, with permission from SAGE Publications

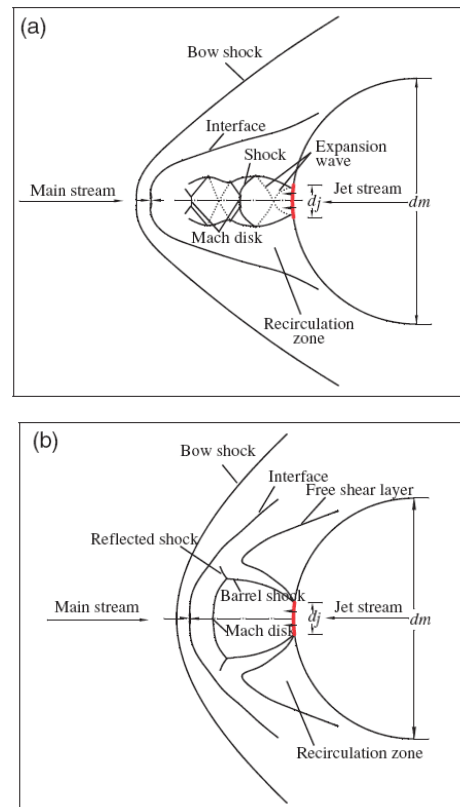


Fig. 5 Flow field properties around the spherical body with counterflowing jet: (a) unsteady state mode with regular reflection; (b) steady-state mode with Mach reflection. Reprinted from (Zhou and Ji, 2014), Copyright 2014, with permission from SAGE Publications

(Huang *et al.*, 2013b). In plasma injection, the drag force reduction is mostly induced by the viscous-inviscid interaction of the counterflowing jet and thermal energy deposition (Shang, 2002; Shang *et al.*,

2002). The flow mode transition is similar to that described by He *et al.* (2006), Gerdroodbary *et al.* (2012), and Zhou *et al.* (2012), namely the unsteady oscillatory and nearly steady motion modes are the long and short penetration modes, respectively (Fig. 6). In the long penetration mode, the bow shock becomes diffused or dispersed, and it is no longer visible. The short penetration mode is shown to be beneficial to heat release reduction (Daso *et al.*, 2009). The short penetration mode jet provides a greater than 15% reduction in drag force in a Mach 2.0 freestream (Daso *et al.*, 2002). At the same time, a sharp variation in the drag coefficient ratio near the critical point appears (Fig. 7) (Zhou and Ji, 2014), and the sharp variation phenomenon disappears with the increase of the angle of attack (Zhou *et al.*, 2013). In Fig. 7, D is the ratio of the diameter of the jet orifice to that of the blunt body, and P is the jet pressure ratio as PR mentioned above. Chen *et al.* (2011) have analyzed the detailed flow field structures at the unstable and stable conditions systematically by using a large eddy simulation, and the fundamental mechanisms including shock-wave/jet interaction, shock-wave/shear-layer interaction, turbulent shear-layer evolution, and coherent structures have been studied.

3 Combination of counterflowing jet and other techniques

Recently, several novel combinatorial strategies between the counterflowing jet and other techniques have been proposed, and research on the combinatorial strategies for the drag and heat release reductions is described in this section, including the combination of a counterflowing jet and forward-facing cavity, the combination of a counterflowing jet and energy deposition, and the combination of a counterflowing jet and an aerospike.

3.1 Combination of counterflowing jet and forward-facing cavity

The influence of a forward-facing cavity on heat transfer and aerodynamic coefficients has been investigated by Saravanan *et al.* (2009), and the deepest cavity shows better heat flux reduction (Silton and Goldstein, 2005; Lu and Liu, 2012b; Yadav and Guven, 2014). The mechanism of heat reduction induced by a forward-facing cavity has been

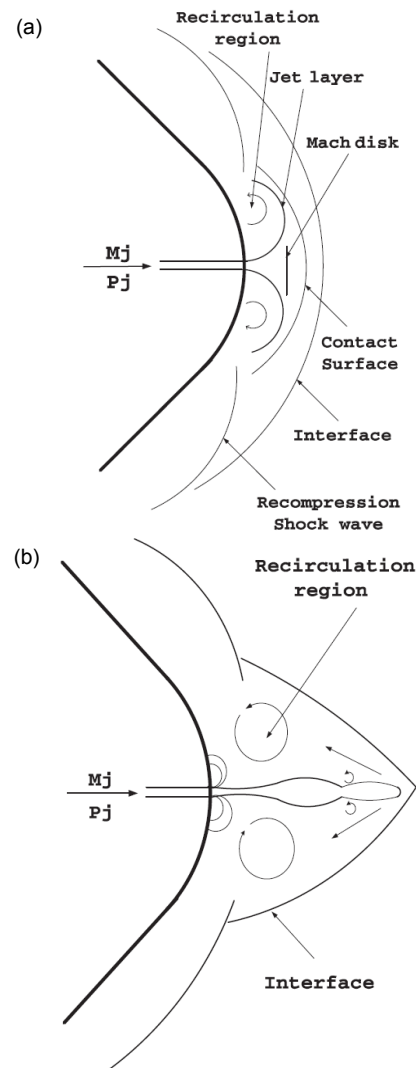


Fig. 6 Comparison of flow field properties around the blunt body with a counterflowing jet: (a) short penetration mode (SPM) jet; (b) long penetration mode (LPM) jet. Reprinted from (Gerdroodbary *et al.*, 2012), Copyright 2012, with permission from Elsevier Masson SAS

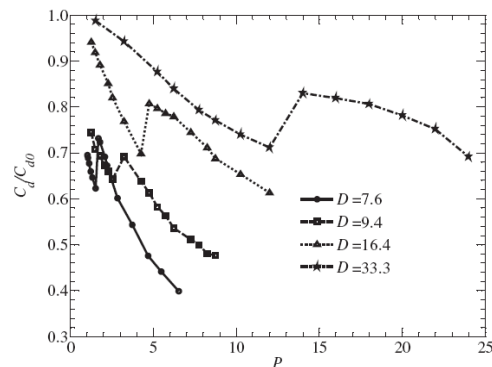


Fig. 7 Variation of drag coefficient ratio with jet pressure ratio under different jet nozzle exit sizes. Reprinted from (Zhou and Ji, 2014), Copyright 2014, with permission from SAGE Publications

explained by many researchers (Huebner and Utreja, 1993; Engblom *et al.*, 1997), and the cooling effect is produced by the oscillation of the bow shock wave (Ladoon *et al.*, 1998). Thus, the combinatorial configuration with counterflowing jet and forward-facing cavity (Fig. 8, from (Lu and Liu, 2014)) may be a promising drag and heat release reduction strategy, and it is attracting increasing attention. In Fig. 8, L and D stand for the length and depth of the forward-facing cavity, respectively, and D_n is the diameter of the base surface for the reentry body.

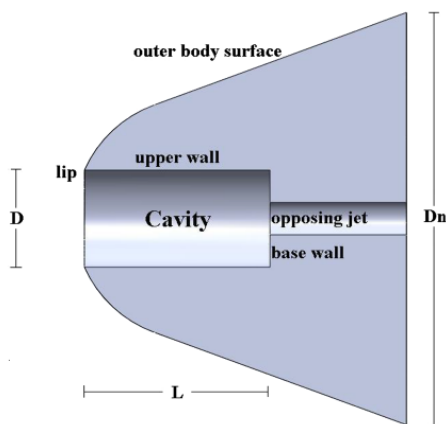


Fig. 8 Schematic diagram of the combination of counterflowing jet and forward-facing cavity. Reprinted from (Lu and Liu, 2014), Copyright 2014, with permission from Springer Science+Business Media

The combinatorial configuration of a counterflowing jet and a forward-facing cavity is more advantageous than that with the counterflowing jet alone when the stagnation pressure of the counterflowing jet is high enough (Huang *et al.*, 2015); its physical mechanism has been provided by Lu and Liu (2014). When the total pressure ratio is high, namely 0.4 in (Lu and Liu, 2014), the cavity acts just like a speed-up nozzle for the counterflowing jet. The high total pressure ratio is beneficial for performance improvement of the drag and heat release reduction, and the recirculation zone plays an important role in heat release reduction (Lu and Liu, 2012c; 2013). However, when the total pressure ratio is low, namely 0.2 in (Lu and Liu, 2014), the cavity will waste the energy of the counterflowing jet, and this condition may be unstable (Hayashi *et al.*, 2006). The combinatorial configuration with a low total pressure ratio can avoid the disadvantage induced by

the unsteady oscillation in the supersonic cavity flow (Lu and Liu, 2012d), and the heat release reduction is more sensitive to the variation of the cavity diameter than to the cavity length (Lu and Liu, 2012e). Further information needs to be obtained using unsteady numerical approaches.

3.2 Combination of counterflowing jet and energy deposition

Due to the difficulty encountered in the engineering implementation of energy deposition and the instability problem encountered in the counterflowing jet, Khamooshi *et al.* (2007) have combined the counterflowing jet and the upstream energy deposition at the nose of the blunt body (Fig. 9), and this combinatorial configuration shows larger decreases in overall drag and heat release than the single strategies of a counterflowing jet and energy deposition (Table 1). In Table 1, Δ stands for the shock standoff distance. RD is the drag reduction factor, defined as the modified drag value divided by the baseline. RQ is the heat transfer reduction factor, defined as the flowfield modified heat transfer over the baseline. At the same time, the instability problem of the counterflowing jet is significantly reduced by the combinatorial configuration.

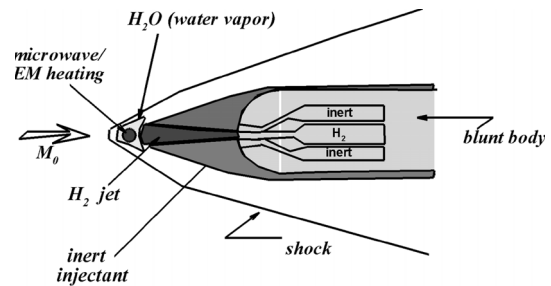


Fig. 9 Schematic diagram of the combination between counterflowing jet and energy deposition. Reprinted from (Khamooshi *et al.*, 2007), Copyright 2007, with permission from AIAA

Table 1 Performance summary of counterflowing jet and energy deposition. Reprinted from (Khamooshi *et al.*, 2007), Copyright 2007, with permission from AIAA

Item	Δ	RD	RQ
Baseline	0.16	1.00	1.00
Counterflowing jet	0.23	0.92	0.95
Energy deposition	0.48	0.60	1.10
Combinatorial configuration	1.10	0.34	0.37

Marley and Riggins (2011) have extended the above work numerically by analyzing the influence of an axisymmetric annular ring injector as well as imposing swirl on the jet stability. The upstream energy deposition is shown to significantly enhance stability and penetration of the counterflowing jet. The annular ring injection exhibits a stabilizing effect on the jet; centered forward injection without upstream energy deposition would encounter high instability.

3.3 Combination of counterflowing jet and aerospike

The aerospike is a relatively mature strategy for drag and heat release reductions, and it has already been utilized successfully in some actual vehicles. However, it also has some inherent disadvantages. Firstly, the nose of the aerospike encounters serious local high temperature due to its small radius of curvature (Mehta, 2000). Secondly, the surface heat flux at the shoulder of the blunt body rises abruptly due to the strong shock-wave/shock-wave and shock-wave/boundary-layer interactions. Thirdly, the aerospike induced conical shock wave may hit the body nose or aerospike at relative high angle of attack, and this could result in a local high heat flux area (Lawrence *et al.*, 1995; Gnemmi *et al.*, 2003). Therefore, the combination of aerospike and counterflowing jet has been proposed to solve these problems.

A new adaptive drag reduction and non-ablative thermal protection approach named telescopic self-aligning jet-spike (TSAJS) has been proposed by Geng *et al.* (2012) (Fig. 10). The influences of the L/D ratio (the ratio of spike length to the cylinder diameter), the freestream and jet Mach numbers, the angle of attack on the flow field structures, and the pressure and heat flux distributions on nose surface have been analyzed. The results obtained show that the TSAJS approach is suitable even for conditions with large angles of attack, and the drag force coefficient and maximum surface heat flux decrease by 65% when the L/D ratio is 1.0. At the same time, its drag and heat release reduction efficiencies are both better than those of the case with only counterflowing jets (Geng and Yan, 2010).

Liu and Jiang (2013) have proposed and validated a combinatorial strategy using both aerospike and lateral jets (Fig. 11). In Fig.11, M stands for the

freestream Mach number. The lateral jets are used to push the conical leading shock wave away from the blunt body (Jiang *et al.*, 2009), as shown in Fig. 12 (Liu and Jiang, 2013). This can achieve efficient cooling of the aerospike tip, as well as high temperature reduction at the shoulder of the blunt body. The results obtained show that the peak pressure at the reattachment region can be decreased by 65% even under a 4° angle of attack by the lateral jet, as shown in Fig. 13 (Liu and Jiang, 2013), and its engineering application appears to be quite promising. In Fig. 13, the symbol α stands for the angle of attack, and P is the wall static pressure. s/D stands for the ratio of the arc length along the blunt body surface measured from the geometric stagnation point to the blunt body diameter.

Gerdroodbary *et al.* (2014) have proposed a novel strategy to reduce further the aerodynamic drag and the heating rates in the vicinity of the nose tip region of a hypersonic vehicle. A coolant is

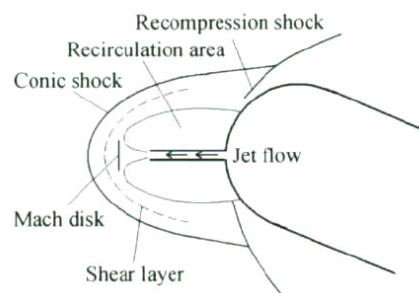


Fig. 10 Schematic diagram of the telescopic self-aligning jet-spike (TSAJS) flow field structure. Reprinted from (Geng *et al.*, 2012), Copyright 2012, with permission from CNKI

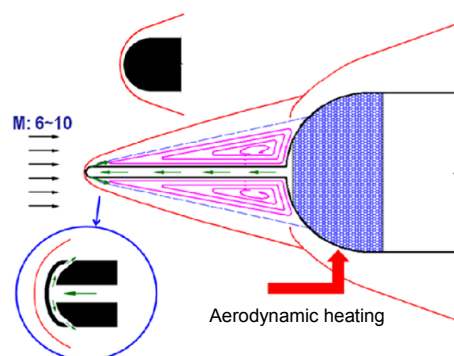


Fig. 11 Operating principles of non-ablative thermal protection system for aerodynamic force and heat load reduction. Reprinted from (Liu and Jiang, 2013), Copyright 2013, with permission from AIAA

injected from the nose cone behind the aerodisk (Fig. 14, from (Gerdroodbary *et al.*, 2014)). In their study, two different jets, namely helium and carbon dioxide, as well as variations of the jet pressure ratio and spike length have been considered. The results obtained show that the combination of the counterflowing jet and aerospike has a great impact on the heating rate reduction (Fig. 15, from (Gerdroodbary *et al.*, 2014)), and the discrepancy between the performance of the coolant jet with aerospike and that without aerospike decreases with the increase of the pressure ratio.

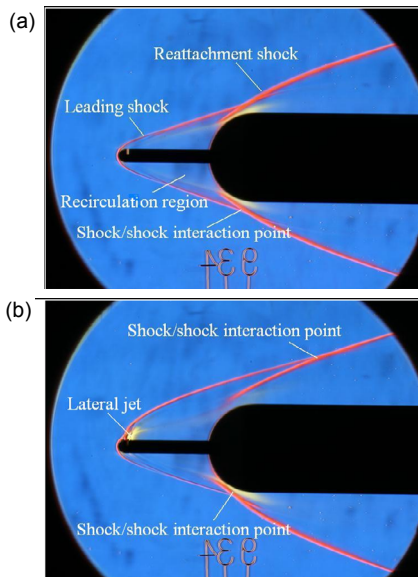


Fig. 12 Comparison of flow field properties around a non-ablative thermal protection system test model with angle of attack being 0° without lateral jet (a) and with lateral jet (b). Reprinted from (Liu and Jiang, 2013), Copyright 2013, with permission from AIAA

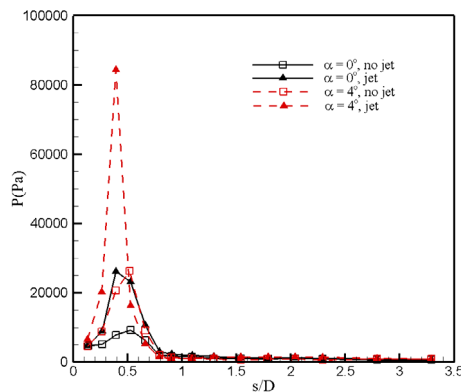


Fig. 13 Wall pressure comparison along the generatrix of non-ablative thermal protection system test model. Reprinted from (Liu and Jiang, 2013), Copyright 2013, with permission from AIAA

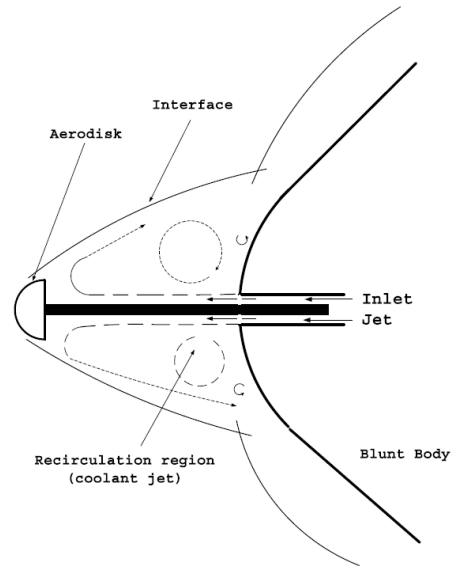


Fig. 14 Schematic diagram of the flow field properties around the aerodisked blunt cone with counterflowing jets. Reprinted from (Gerdroodbary *et al.*, 2014), Copyright 2014, with permission from Elsevier Masson SAS

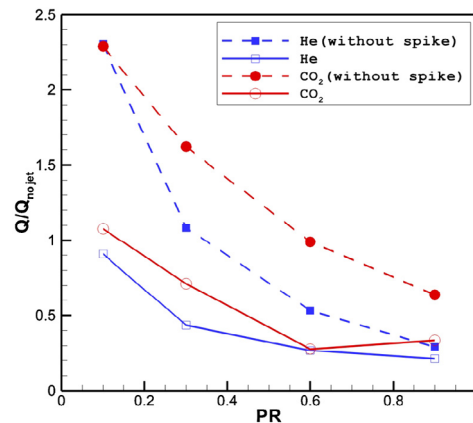


Fig. 15 Comparison of influences of various jet pressure ratios on the heat load reduction of the counterflowing jet with $L/D=1.0$. Reprinted from (Gerdroodbary *et al.*, 2014), Copyright 2014, with permission from Elsevier Masson SAS

4 Remarks and recommendations

In this survey, research on the drag and heat release reduction induced by a counterflowing jet and its combinations has been reviewed. Three combinatorial configurations have been considered in the current survey, namely the combination of the counterflowing jet and a forward-facing cavity, the combination of the counterflowing jet and an aerospike, and

the combination of the counterflowing jet and energy deposition. We came to the following conclusions:

1. The jet instability encountered in a counterflowing jet and its combinations is a critical problem for the variation of drag force, and it needs to be further investigated by using an unsteady numerical approach, especially for the combination of the counterflowing jet and a forward-facing cavity. This would provide a valid supplement for the phenomena observed in the ground experimental test.

2. Drag and heat release reductions on hypersonic vehicles are often conflicting, and they should be solved by using a multi-objective design optimization approach. At the same time, the influences of the operational and geometric parameters on the drag and heat release reductions should be investigated comprehensively, and the critical points for more parameters during the flow mode transition could be obtained. This information would be very useful for the design of a thermal protection system.

3. The combinatorial configurations show better drag and heat release reduction performance than for a single counterflowing jet, and more attention should be paid to combinations of the counterflowing jet and other techniques. In the flow field around the combinatorial configurations, the local high heat flux at the shoulder of the blunt body disappears, and the recirculation zone increases. Further, the flow rate of the counterflow jet for a real vehicle should be estimated, and it is a crucial step towards an engineering implementation.

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中文概要

题目: 逆向喷流及其组合体在超声速气流中减阻防热功效研究进展

概要: 总结归纳国内外逆向喷流及其组合体在超声速气流中减阻防热功效的研究进展, 并给出逆向喷流在某些应用领域的建议, 特别是喷流的不稳定性保护、减阻与热防护之间的权衡以及流动模态转换的工作参数和结构参数临界点选取等。

关键词: 高超声速飞行器; 减阻; 热防护; 逆向喷流; 前向凹腔; 能量沉积