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Miniaturized bandpass filter with wide upper stopband using isomeric resonators in a cavity

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Key words: Compact filter; Wide upper stopband; Waveguide resonator; Half-wavelength resonant slot; Tuning post; Transmission zero

We propose a compact three-pole bandpass filter (BPF) using isomeric resonators in a cavity, consisting of two ridge waveguide (WG) resonators and a half-wavelength resonant slot (HWRS) in between. Based on the E-field distributions of the first two modes (TE_{101} and TE_{102} modes) of the ridge WG resonator, a tuning post (Tup) is embedded at the center of the ridge, where the E-field of the TE_{101} mode is concentrated, whereas that of the TE_{102} mode is minimal. As a result, the resonant frequency of the fundamental TE_{101} mode is significantly shifted, while the first harmonic TE_{102} mode remains almost unchanged, indicating that both miniaturization and a wide spurious-free range can be achieved. In addition, the introduction of an HWRS resonator between the two ridge WG resonators enables the realization of a three-pole filter, thereby reducing the length of the BPF and introducing cross-coupling to generate a transmission zero (TZ) in the upper stopband. Moreover, the thickness of the HWRS resonator provides an additional path to control the cross-coupling, enabling precise TZ positioning within a certain range. Based on this approach, an inline filter with a compact structure and high performance is designed, achieving a size reduction of approximately 90% and wider upper stopband rejection compared with a filter based on a traditional ridge WG.

1 Introduction

Recently, the increasing demand for advanced telecommunication systems has spurred extensive research into bandpass filters (BPFs), with particular emphasis on miniaturization, reduction of insertion loss (IL), and enhancement of upper stopband rejection (Huang et al., 2021; Snyder et al., 2021; Lin et al., 2023; Zeng et al., 2023).

The metal waveguide (WG) filter has been the subject of extensive research due to its high-power capacity and low loss (Wong et al., 2021; Xiang et al., 2023). However, the substantial size of filter circuitry poses significant challenges to the miniaturization required in modern communication systems (Fang et al., 2022). Dielectric resonator (DR)-loaded cavities (Chen et al., 2016; Tomassoni et al., 2016; Widaa and Höft, 2023) and dielectric WGs (Xie et al., 2023; Qin et al., 2024; Tang et al., 2024; Xu et al., 2024) are widely employed to reduce dimensions. Nevertheless, spurious responses associated with either DR-loaded cavities or dielectric WGs persist, leading to insufficient suppression of the upper stopband and limiting their application in multi-standard wireless communication systems (Zhao et al., 2022).

Relatively speaking, ridge WG technology has attracted increasing attention because of its potential for size reduction and improved upper stopband performance (Fahmi et al., 2009; di Crestvolant and de Paolis, 2018; Chen et al., 2024; Zhang et al., 2025). Recently, a U-shaped ridge resonator is proposed to generate a transmission zero (TZ) either above or below the passband (Chaudhary et al., 2023). However, the upper stopband performance and overall size of the cavity BPF ave not addressed. To reduce the filter length, the coupling structure between ridge WG resonators is modified to width-reduced rectangular WGs (Chen et al., 2025). This modification shortens the distance between ridge WG resonators and introduces TZs. Nevertheless, the filter length remains relatively large due to cascade coupling of the ridge WG resonators, and the improvement in upper stopband performance is limited. Moreover, the TZ in the upper stopband cannot be independently controlled because the coupling between the first and third resonators, K_{13}, is determined once the coupling between the first and second resonators, K_{12}, is established in traditional inline cavity BPFs.

In this paper, based on the E-field distributions of the first two modes in ridge WG resonators (TE_{101} and TE_{102} modes), a tuning post (Tup) is embedded in the central region of the ridge. By adjusting

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the Tup depth, the resonant frequency of the fundamental TE_{101} mode (f_{101}) is significantly reduced, whereas the first harmonic TE_{102} mode remains almost unchanged, indicating that both miniaturization and a wide upper stopband can be achieved. Furthermore, a half-wavelength resonant slot (HWRS) resonator is introduced between two ridge WG resonators to construct a three-pole BPF. This configuration reduces the BPF length and introduces cross-coupling, thereby generating a TZ in the upper stopband. In addition, the thickness of the HWRS resonator provides an extra path to control the cross-coupling, enabling precise TZ positioning within a certain range. Measurement results indicate that the proposed filter achieves a size reduction of approximately 90% and wider upper stopband rejection compared with a filter based on a traditional ridge WG (Chen et al., 2025).

2 Guidelines for manuscript preparation

The proposed BPF is a three-pole filter using isomeric resonators in a cavity, consisting of two ridge WG resonators and an HWRS in between. As illustrated in Fig. 1, the ridges are designed to be re-entrant to allow the embedding of the Tup.

2.1 Working principle of the ridge WG resonator with Tup

As illustrated in Fig. 2(a), a metal ridge (a_r×b_r=10 mm×11.8 mm) is inserted into an evanescent-mode rectangular WG (a×b=25.2 mm×12.6 mm) to form a ridge WG resonator. The first two modes of the ridge WG resonator are the TE_{101} and TE_{102} modes, as shown in Fig. 2. The E-field of the TE_{101} mode is predominantly concentrated in the central region above the ridge, whereas that of the TE_{102} mode is distributed in the longitudinal regions above the ridge. Therefore, the Tup can be strategically embedded in the central region of the ridge, as shown in Fig. 3(a), to modulate f_{101}.

As shown in Fig. 3(b), the modulation range of f_{101} is approximately 0%–45%, which can be combined with the analysis of ridged WG modes to predict f_{101} (Utsumi, 1985). Meanwhile, f_{102} remains almost constant as the height of the Tup (h_c) increases, whereas f_{101} exhibits a decreasing trend with increasing h_c or w_1, as shown in Figs. 3(b) and (c). In addition, the unloaded quality factor Q_u of the TE_{101} mode decreases, as shown in Fig. 3(d). These results indicate that the introduction of the Tup can reduce f_{101} while forming a wide spurious-free range between the two modes. As illustrated in Fig. 4(a), the first higher-order resonant frequency f_1 of the ridge WG resonator with Tup decreases as h_c increases or w_1 decreases. Concurrently, f_{101} also varies with changes in h_c or w_1, resulting in an expanded single-mode operating bandwidth n (n=f_1/f_{101}), which increases as h_c or w_1 increases, as shown in Fig. 4(b).

According to Fig. 3(d) and Fig. 4, a compromise is required among Q_u, size reduction, and spurious range. To maintain a Q_u value exceeding 1300, the parameters h_c and w_1 are set to 7.5 mm and 5 mm, respectively.

2.2 Resonant coupling structure

As shown in Fig. 5(a), the proposed resonant coupling structure is formed by an HWRS resonator. As shown in Fig. 5(b), the resonant frequency of the proposed resonant coupling structure (f_{s0}) is primarily determined by the total slot length (d_0=2d_1+2d_2+2d_3+2d_4+d_5), following the approximate relation f_{s0}≈c/2d_0, where c is the speed of light in vacuum.

Although f_{s0} slightly decreases as the thickness (l_5) increases, it can be decoupled by slightly adjusting d_0. The E-field direction of the resonant coupling structure is shown in Fig. 6. It can be observed that the input and output couplings of the proposed structure have the same E-field direction, implying that the structure can provide the required characteristics to achieve a controllable TZ in the upper stopband.

2.3 Design of the compact BPF

Due to the characteristics of the resonant coupling structure, its resonant frequency depends on both l_5 and d_0, implying that, under the condition of meeting the required coupling coefficient, the resonant coupling structure can be designed to be extremely thin.

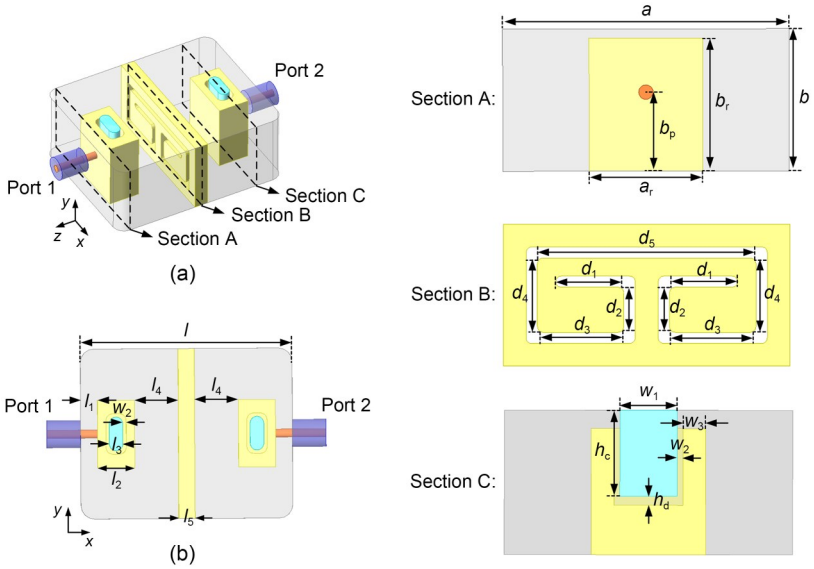

Fig. 1 3D view (a) and top view (b) of the Configuration of the proposed filter. Parameters are a=25.2, b=12.6, a_r=10, b_r=11.8, b_p=7, d_1=6, d_2=4, d_3=7.6, d_4=6.6, d_5=19.2, h_c=7.5, w_1=5, w_2=0.5, w_3=0.5, h_d=0.8, l=32.8, l_1=2.5, l_2=5.5, l_3=2, l_4=7.1, and l_5=2.6. Unit: mm)

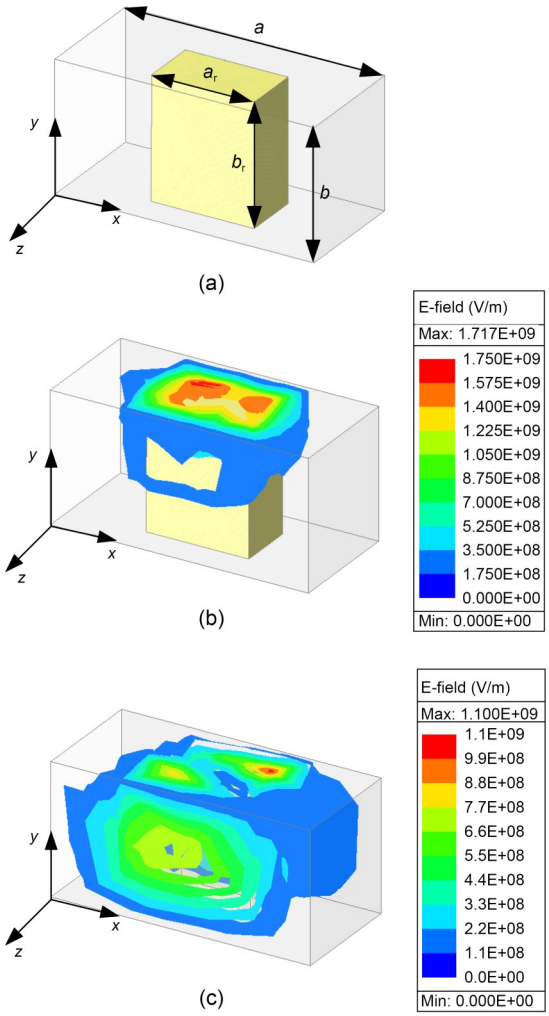

Fig. 2 Ridge waveguide resonator (a) and the E-field distributions of TE_{101} (b) and TE_{102} modes

Consequently, the ridge WG resonators are closely arranged in the BPF design, and the topology structure of the BPF is shown in Fig. 7.

In addition, the ridge WG resonator exhibits a wide single-mode operating bandwidth, within which only the fundamental mode is supported and no higher-order modes are excited. As a result, a broad attenuation region is formed prior to the onset of the first higher-order resonance. As shown in Fig. 8, this attenuation region fully covers the first higher-order mode of the half-mode resonator, indicating that filters employing the isomeric ridge WG and HWRS resonators can realize a wide upper stopband.

The proposed BPF has a center frequency (f_0) of 2.2 GHz with a 0.3 dB ripple fractional bandwidth of 13%. According to the specifications, the lumped-element values of the low-pass prototype filter are g_0=1, g_1=1.04, and g_2=1.15.

Accordingly, the required external quality factor and coupling coefficients of the BPF are obtained (Hong et al., 2001): Q_e=7.5 and K_{12}=K_{23}=0.12. The coupling matrix is as follows:

$$\begin{bmatrix} 0 & 1.001 & 0 & 0 & 0 \\ 1.001 & 0.093 & 0.867 & 0.405 & 0 \\ 0 & 0.867 & -0.418 & 0.867 & 0 \\ 0 & 0.405 & 0.867 & 0.093 & 1.001 \\ 0 & 0 & 0 & 1.001 & 0 \end{bmatrix}$$

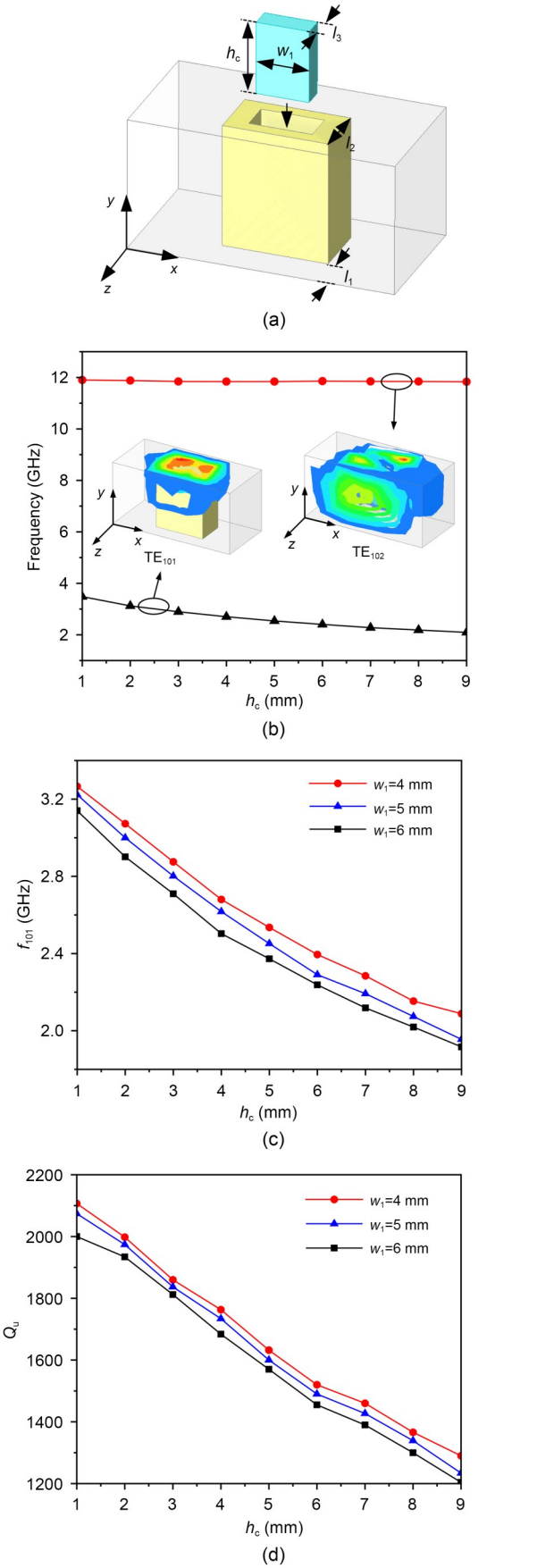

Fig. 3 Ridge waveguide (WG) resonator with Tup (a) (w_1=5, l_1=2.5, l_2=5.5, and l_3=2. Unit: mm), simulated resonant frequency of the ridge WG resonator versus h_c with different modes (TE_{101} and TE_{102} modes) (b), and simulated f_{101} (c) and Q_u (d) versus h_c with different w_1

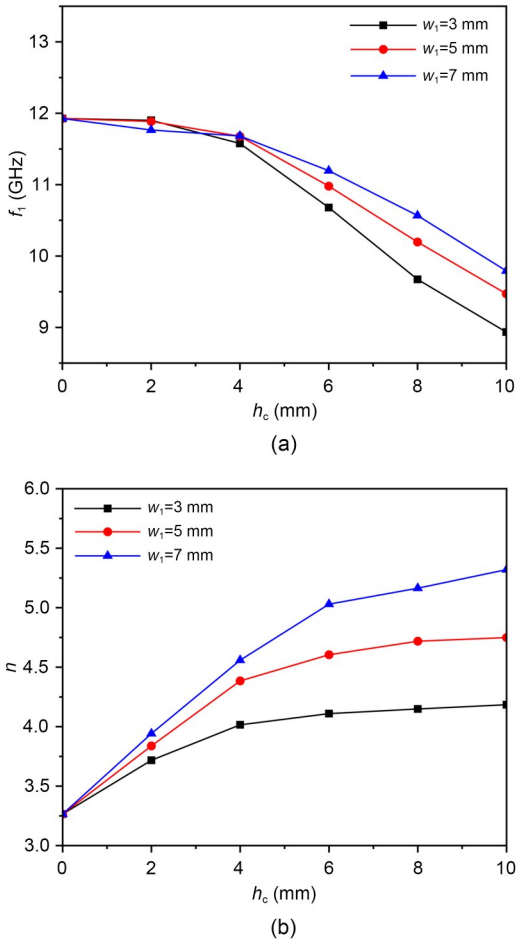

Fig. 4 Simulated f_1 (a) and n (b) versus h_c with different w_1 (n=f_1/f_{101}) (l_1=2.5, l_2=5.5, and l_3=2. Unit: mm)

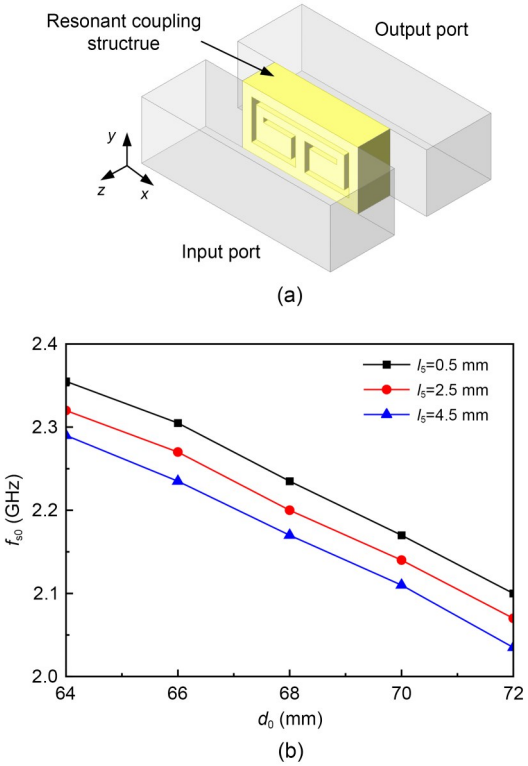

Fig. 5 Proposed resonant coupling structure (a) and f_{s0} versus d_0 with different l_5 (b)

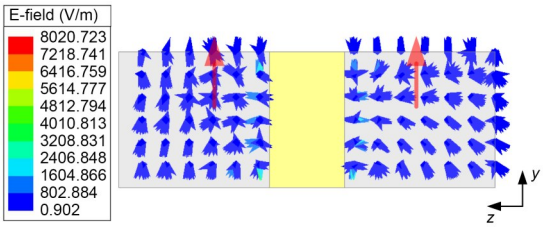

Fig. 6 E-field distribution of the resonant coupling structure

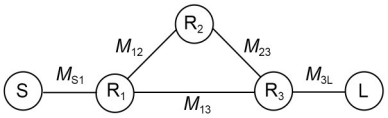

Fig. 7 Coupling topology structure of the proposed bandpass filter

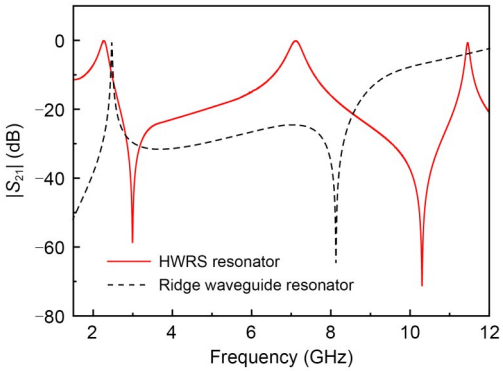

Fig. 8 Simulated $|S_{21}|$ of the HWRS and ridge waveguide resonators

The extracted Q_e depends on the length l_1 and the height b_p of the feeding probe. As shown in Fig. 9, Q_e increases as b_p increases or l_1 decreases. A parametric investigation of coupling coefficient control is conducted to validate the TZ tuning capability. As illustrated in Fig. 10(a) and (b), K_{12} and K_{13} are governed by the distance l_4 between the ridge WG and HWRS resonators. Notably, the thickness l_5 of the HWRS resonator provides an additional control mechanism for K_{13}. From Fig. 10(a) and (b), it is evident that K_{13} can be effectively adjusted by varying l_5, whereas K_{12} remains largely unaffected, demonstrating decoupled control capability. Fig. 10(c) presents the simulation results of BPFs with different l_5. The demonstrated TZ tuning capability enables strategic enhancement of the

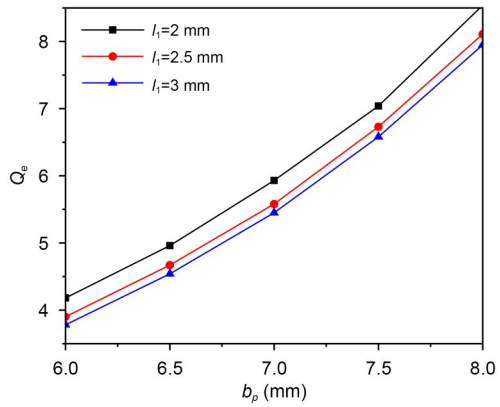

Fig. 9 Extracted Q_e versus b_p with different l_1

filter upper stopband rejection. After the optimization process, the dimensions of the proposed BPF are provided in the caption of Fig. 1, achieving a size reduction of approximately 90% compared with a filter based on a traditional ridge WG.

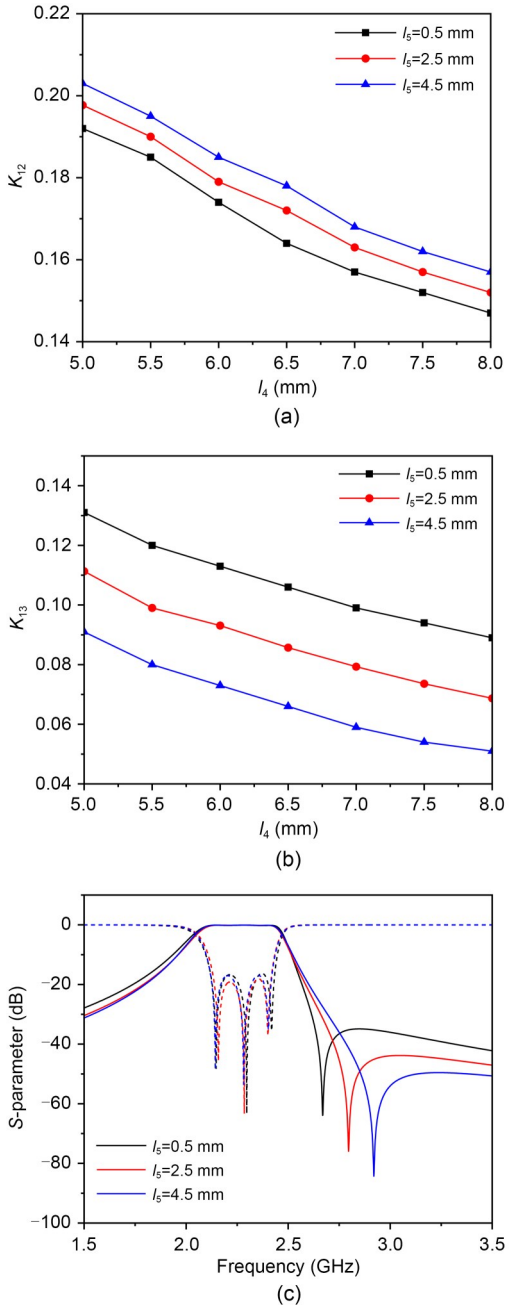

Fig. 10 Extracted K_{12} (a) and K_{13} (b) versus l_4 with different l_5 and simulation result of the proposed bandpass filter with different l_5 (c) ((solid lines: $|S_{21}|$, dashed lines: $|S_{11}|$)

3 Simulation and experimental results

Fig. 11 shows a photograph of the fabricated BPF, and the experimental results are measured using an Agilent N5230A PNA-L network analyzer. The measurement and simulation results are presented in Fig. 12 and show good agreement. The BPF has f_0=2.2 GHz and a passband ranging from 2.04 to 2.48 GHz, achieving a predefined 3-dB fractional bandwidth of approximately 19%. The measured return loss ($|S_{11}|$) is better than 17 dB, while the minimum IL is 0.45 dB. The proposed design exhibits a wide upper stopband, with a suppression level higher than 30 dB from 2.65 to 10.6 GHz, corresponding to a defined ζ value of 3.63, as listed in Table 1.

Table 1 summarizes the performance of BPFs using various technologies. As expected, the proposed BPF has the smallest volume ($0.23\lambda_0\times0.18\lambda_0\times0.09\lambda_0$) owing to the use of isomeric resonators in a cavity. It achieves a size reduction of approximately 90% compared with the BPF based on cascade coupling of ridge WG

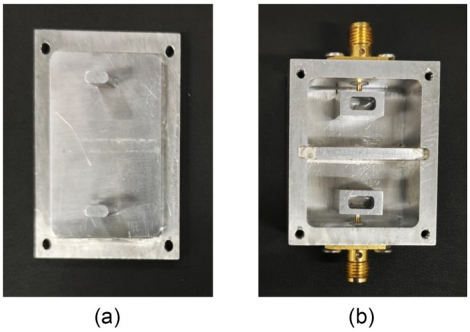

Fig. 11 Top part (a) and Bottom part (b) of the prototype

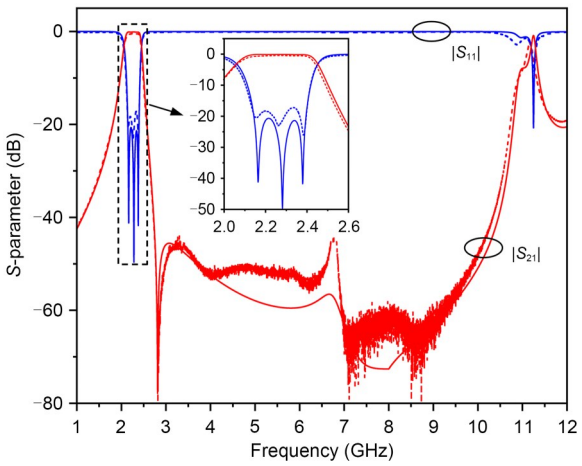

Fig. 12 Simulation(solid lines) and measurement (dashed lines) results

Table 1 Comparison with other bandpass filters

Reference	Technology	f_0 (GHz)	3-dB fractional bandwidth (%)	Order	Insertion loss (dB)	ζ	3D size (λ_0^3)
Zhu et al. (2024)	Waveguide	3.72	4.5	3	0.24	0.18	0.72×0.62×0.54
Widaa et al. (2023)	Dielectric resonator-loaded WG	3.967	0.5	2	1.3	N.A.	0.82×0.26×0.164
Qin et al. (2024)	Dielectric WG	3.45	2.8	3	0.8	1.47	0.34×0.34×0.07
Ruiz-Cruz et al. (2005)	Ridge WG	4	14.6	3	0.3	0.2	0.82× 0.33×0.33
Chen et al. (2024)	Ridge WG	3.5	20	3	0.25	1.94	0.44×0.29×0.15
Proposed	Ridge WG and resonant slot	2.2	19	3	0.45	3.63	0.23×0.18×0.09

Note: $\zeta=(f_{max}-f_{min})/f_0$, where f_{max} and f_{min} are the maximum and the minimum frequencies when $|S_{21}|$=−30 dB in the upper stopband, respectively. λ_0 represents the free space wavelength at f_0

resonators (Chen et al., 2025). Meanwhile, the upper stopband is much wider than those of the designs listed in Table 1 and is comparable to that of a microstrip design with harmonic suppression (Chen et al., 2018), indicating that the proposed design effectively addresses the long-standing issue of harmonic interference in traditional WG filters. In fact, this improved performance is obtained at the expense of passband loss, which is slightly higher than that of WG or ridge WG designs but lower than that of designs based on DRs and dielectric WGs, as listed in Table 1.

4 Conclusions

In this paper, a miniaturized cavity BPF using isomeric resonators is presented, achieving a size reduction of approximately 90% and wider upper stopband rejection compared with a filter based on a traditional ridge WG. The proposed design offers three key advantages: a compact footprint, an extended upper stopband, and a controllable TZ. These features collectively address long-standing challenges in conventional WG filters, including excessive size and harmonic interference, while providing a systematic approach for positioning the TZ within the upper stopband to enhance selectivity. The high performance verified by simulation and experiment makes the proposed filter attractive for practical applications, such as satellite communication.

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Author contributions

Chengyang ZHANG designed the research, processed the data, and drafted the paper. Jianxin CHEN, Ying XUE, and Qingyuan LU helped organize the paper. Chengyang ZHANG and Jianxin CHEN revised and finalized the paper.

Conflict of interest

Chengyang ZHANG, Ying XUE, Qingyuan LU, and Jianxin CHEN declare that they have no conflict of interest.

Data availability

The data that support the findings of this study are available from the corresponding author upon reasonable request.

Declaration of generative AI and AI-assisted technologies in the writing process

During the preparation of this work the authors used ChatGPT in order to improve language. After using this tool, the authors reviewed and edited the content as needed and take full responsibility for the content of the published article.

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