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Design of a wideband symmetric large back-off range Doherty power amplifier based on impedance and phase hybrid optimization

Key words: Back-off power range; Doherty power amplifier; Fragment-type structure; Impedance–phase hybrid function

Corresponding author: Jing XIA

E-mail: jingxia@ujes.edu.cn

 ORCID: <https://orcid.org/0000-0001-6255-9297>

Motivation

1. Conventional symmetrical Doherty power amplifiers (DPAs) achieve efficiency enhancement only at a 6-dB back-off power (BOP), which is insufficient to meet the increasing demands of modern communication systems.
2. The DPA based on integrated enhancing reactance (IER) does not consider the effect of phase dispersion in the output matching network (OMN) on the IER across a wide frequency band, resulting in significant efficiency variations between high and low frequencies at the BOP and limiting its ability to achieve a wider band.
3. Conventional power amplifier designs commonly use regular microstrip circuit structures, which limits the feasibility of circuit optimization.

Main idea

1. An impedance–phase hybrid objective function was employed to reduce efficiency inconsistencies caused by phase dispersion across the wideband range.
2. To enhance design flexibility, a fragment-type matching circuit is employed in the OMN design.
3. Compared to conventional regular structure designs, the optimized fragment-type structure DPA achieves an expanded relative operating bandwidth while maintaining high BOP efficiency.

Method (Cont'd)

2. For high frequencies, the optimal load impedance at 2.5 GHz under saturation is determined to be $(14+j1) \Omega$ through load-pull simulation. Based on Eq. (2), when R_L is 28Ω , jX_{IER} is calculated as $-j30 \Omega$. Using the two-impedance matching method, the corresponding phase of OMN_A at 2.5 GHz is determined to be -215° . Therefore, the optimization objective function for OMN_A at the high frequency is given as in Eq. (3).

$$jX_{IER} = \frac{-2R_L(1 + \Gamma_1)}{1 + 3\Gamma_1} \quad (2)$$

$$F_{Z_\theta_{2.5\text{GHz}}}(Z_L, \theta) = \max(|R_L - 14| + |X_L - 1|, |\theta + 215|) \quad (3)$$

Method (Cont'd)

3. For the center and low frequencies, an impedance constraint circle is employed as the impedance target, and a phase balancing strategy is applied to minimize the phase difference.

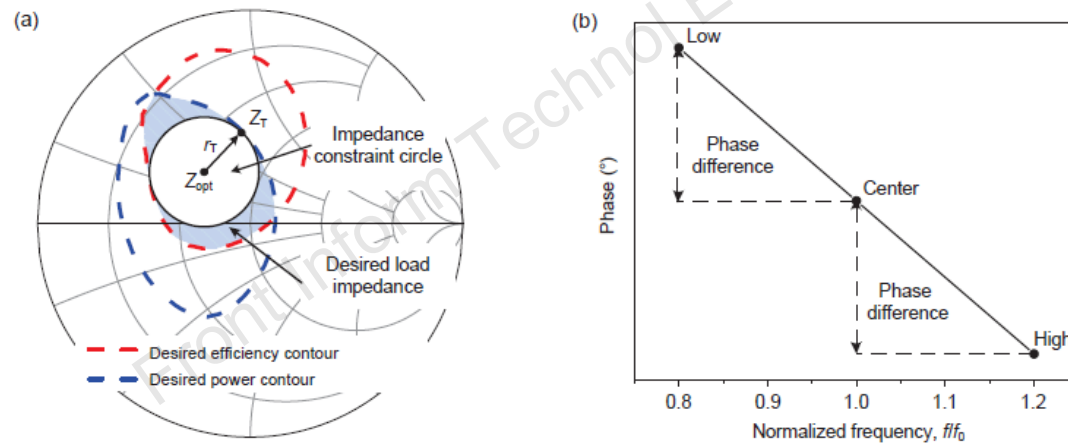


Fig. 2 Illustration of the objective functions for center- and low-frequency optimization: (a) impedance; (b) phase

$$\begin{aligned}
 & F_{Z_ \theta_ 2.1\text{GHz}}(Z_L, \theta) & F_{Z_ \theta_ 1.7\text{GHz}}(Z_L, \theta) \\
 = \max(F_{Z_ 2.1\text{GHz}}(Z_L), F_{\theta_ 2.1\text{GHz}}(\theta)) & = \max(F_{Z_ 1.7\text{GHz}}(Z_L), F_{\theta_ 1.7\text{GHz}}(\theta)) & (4)
 \end{aligned}$$

Method (Cont'd)

4. Based on the previously mentioned optimization strategy, a fragment-type structure is selected for the OMN_A design to reduce phase dispersion.

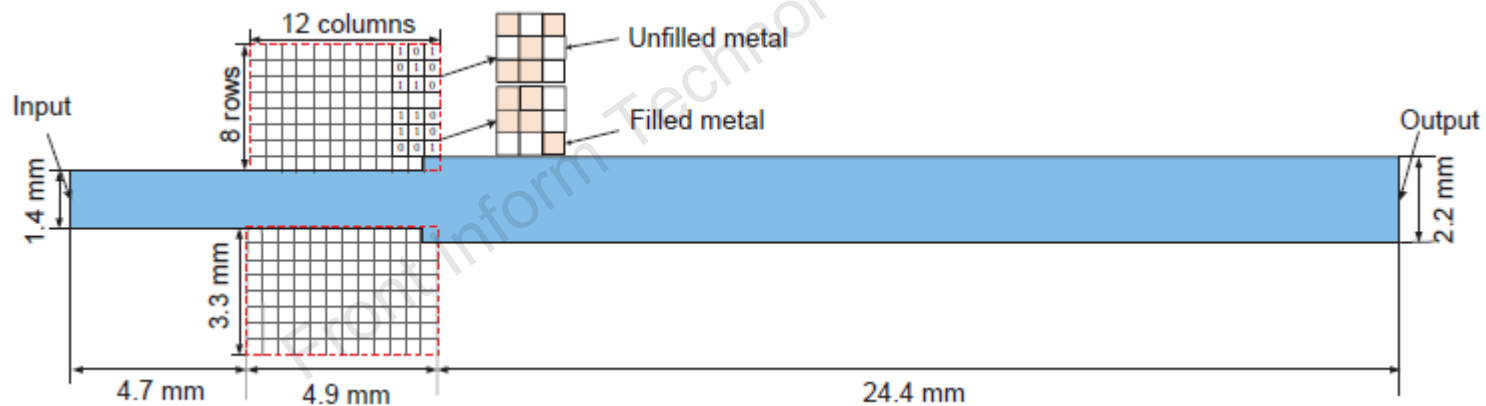
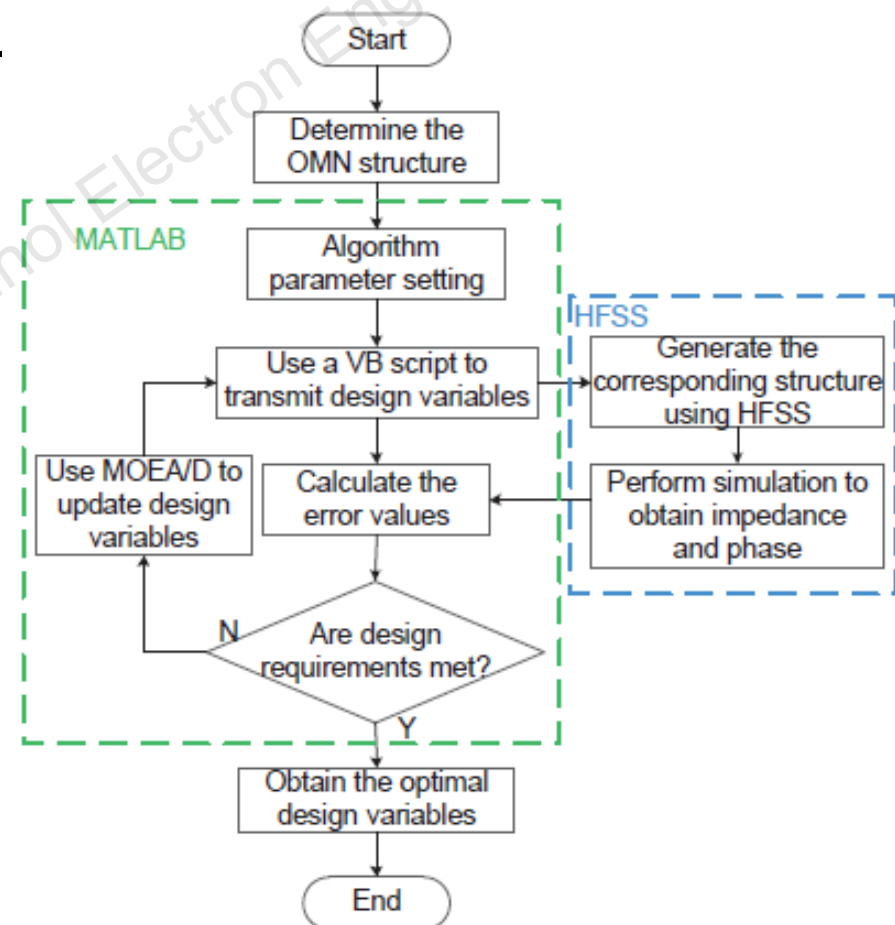


Fig. 3 Structure of the fragment-type auxiliary output matching network (OMN_A)

Method (Cont'd)

5. A multi-objective evolutionary algorithm based on decomposition (MOEA/D) is used to generate the design parameters of the fragment-type structure for OMN_A .

Fig. 4 Design flowchart of the proposed method (OMN: output matching network; MOEA/D: multi-objective evolutionary algorithm based on decomposition; HFSS: High Frequency Structure Simulator)



Major results

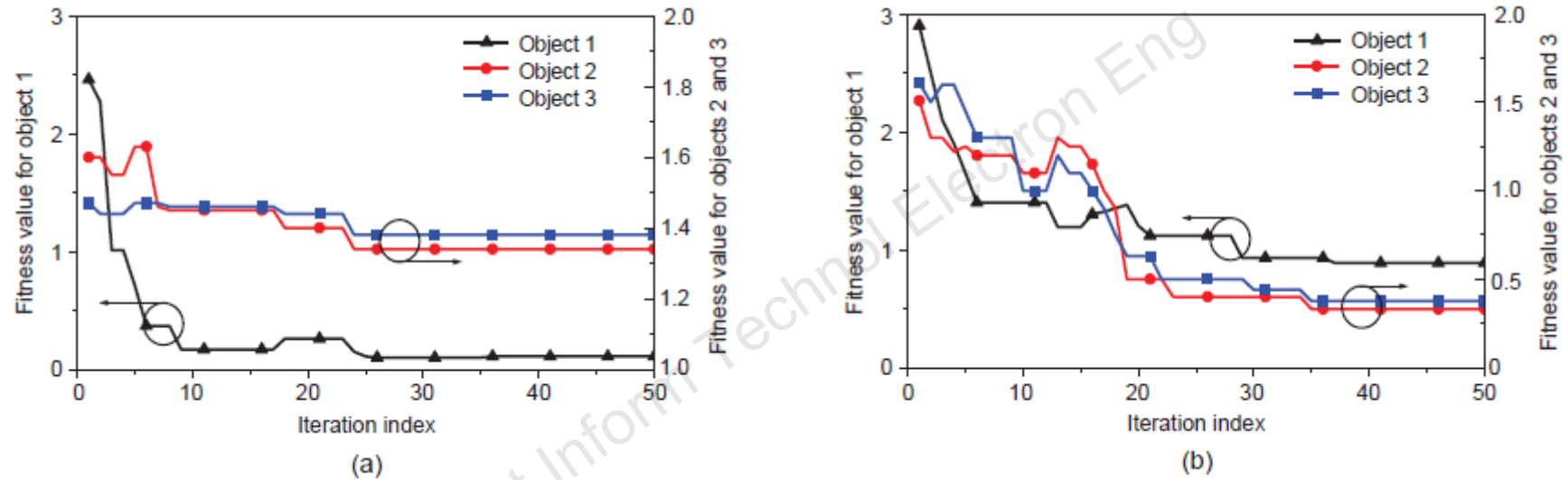


Fig. 5 Fitness value of the objective functions in the optimization process: (a) regular structure; (b) fragment-type structure

Major results (Cont'd)

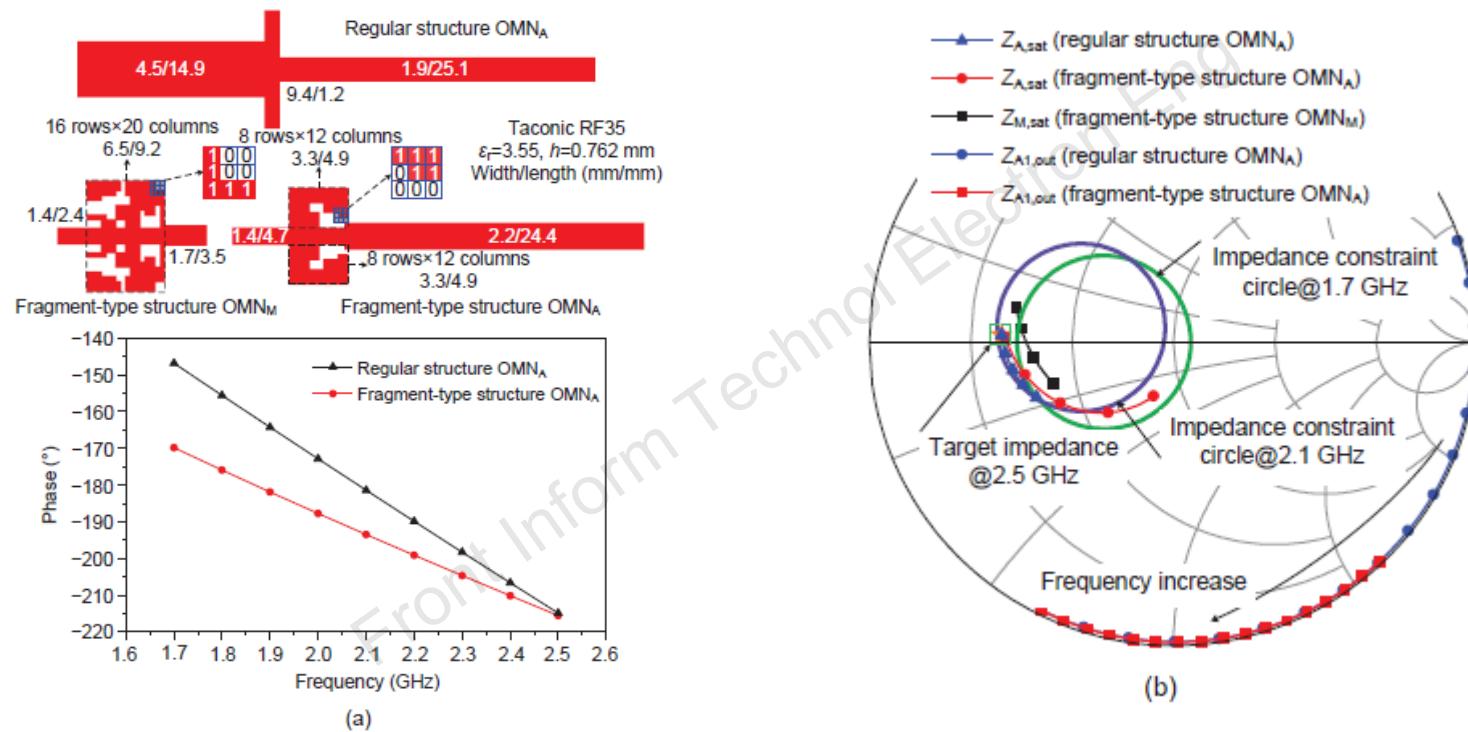


Fig. 6 The optimized output matching network (OMN) and simulation results in the 1.7–2.5 GHz frequency band: (a) phase; (b) impedance

Major results (Cont'd)

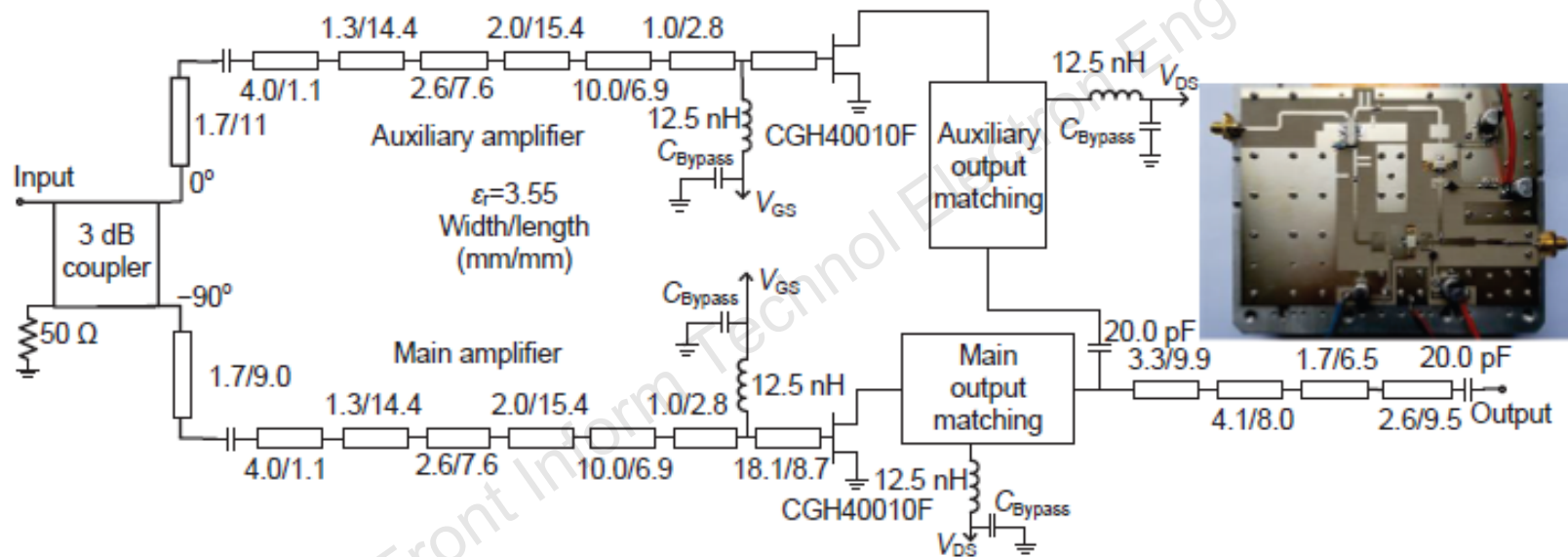


Fig. 7 Complete schematic of the proposed Doherty power amplifier (DPA) (Inset shows the fabricated DPA)

Major results (Cont'd)

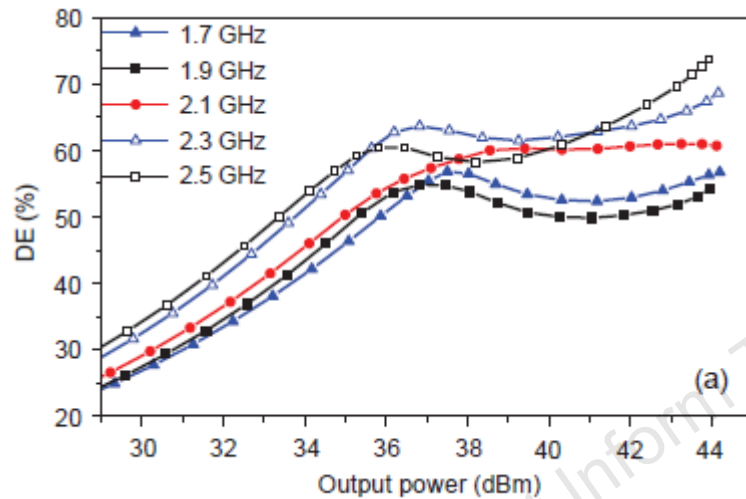


Fig. 8a Doherty power amplifier (DPA) simulation results

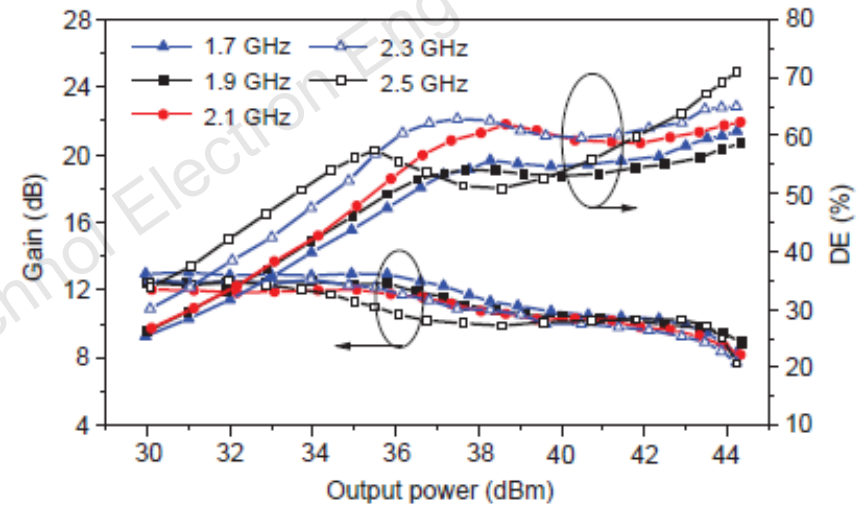


Fig. 9 Measurement results of the gain and drain efficiency (DE) for the proposed Doherty power amplifier (DPA)

Major results (Cont'd)

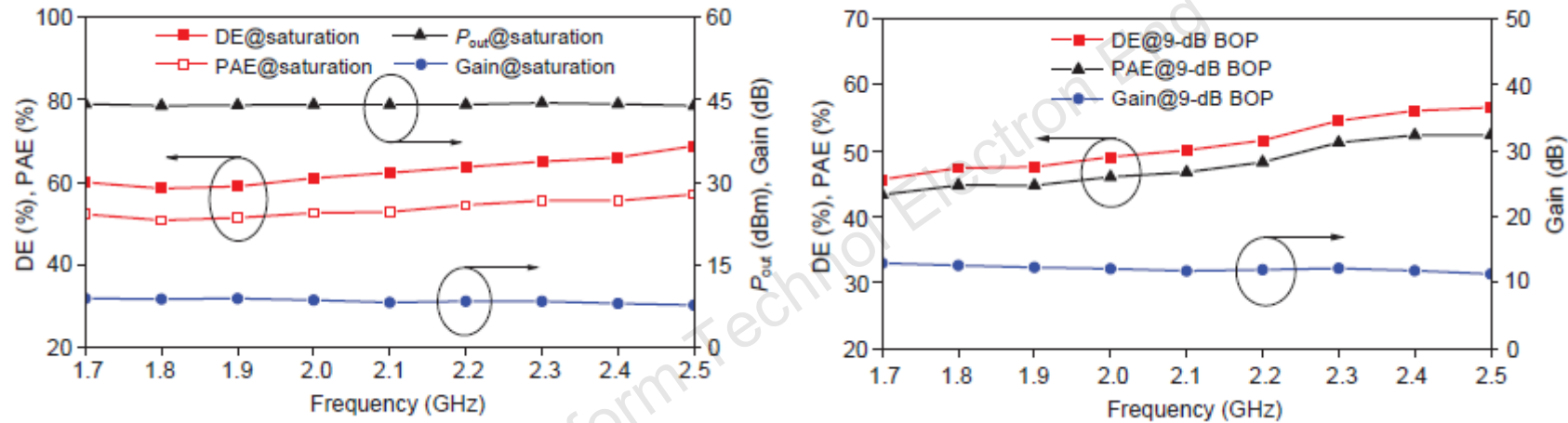


Fig. 10 Measurement results vs. frequency (DE: drain efficiency; PAE: power added efficiency)

Major results (Cont'd)

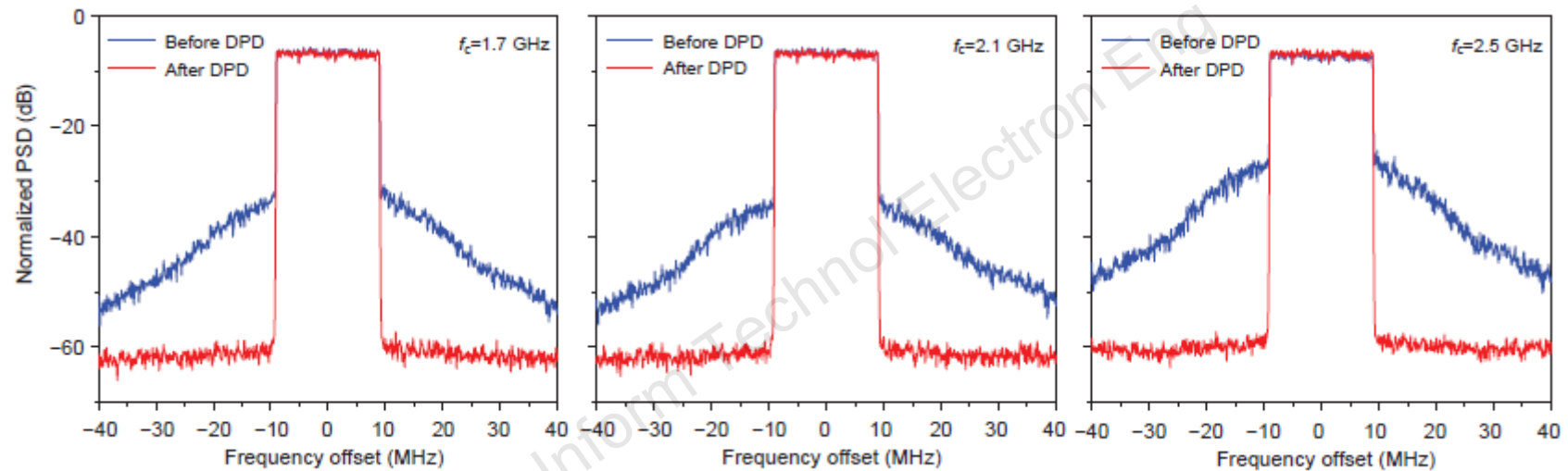


Fig. 11 Measured spectra before and after linearization for 20-MHz LTE modulation signal (LTE: long-term evolution; DPD: digital pre-distortion; PSD: power spectral density)

Conclusions

1. A fragment-type structure OMN optimization method using an impedance–phase hybrid objective function has been proposed.
2. To validate the effectiveness of the method, a 1.7–2.5 GHz DPA was fabricated and measured.
3. The fabricated DPA achieved a saturated output power exceeding 44 dBm within the operating bandwidth, with a DE ranging from 58.5% to 68% at saturation and from 45% to 55% at a 9-dB BOP.



Zhongpeng NI received the B.E. degree in electronic engineering from Changshu Institute of Technology in 2021. Since September 2021, he has been pursuing the M.S. degree in electronic information at Jiangsu University, Zhenjiang, China. He is currently working toward the Ph.D. degree. His research interests include the design of high-efficiency power amplifiers.



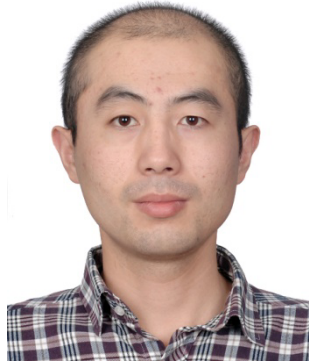
Jing XIA received the M.E. degree in computer science and technology from Jiangsu University, Zhenjiang, China, in 2007, and the Ph.D. degree in electromagnetic field and microwave technology from the State Key Laboratory of Millimeter Waves, Southeast University, China, in 2014. From 2015 to 2016, he was a Postdoctoral Research Fellow with the RF and Microwave Research Group, University College Dublin, Ireland. He is currently a Professor with the School of Computer Science and Communication Engineering, Jiangsu University. His research interests include high back-off efficiency power amplifier (PA) design, wideband efficient PA design, and digital pre-distortion techniques.



Xinyu ZHOU received the M.S. and Ph.D. degrees in electronic engineering from the City University of Hong Kong, Kowloon, Hong Kong, China, in 2014 and 2018, respectively. He is currently an Assistant Professor (Research) with the Department of Electrical and Electronic Engineering, The Hong Kong Polytechnic University (PolyU), and a member of the Research Institute for Artificial Intelligence of Things (RIAIoT), PolyU. He is also a Principal Investigator of the Laboratory of Radio Frequency Microelectronics Circuits (RFMC), PolyU. His current research interests include broadband high-efficiency and high-linearity GaN power amplifiers in RF and millimeter-wave, microelectronic circuits, and microwave passive circuits.



Wa KONG received the M.E. degree in communication and information system and the Ph.D. degree in computer application technology from Jiangsu University, Zhenjiang, China, in 2006 and 2020, respectively. She is currently an Associate Professor with the School of Computer Science and Communication Engineering, Jiangsu University. Her research interests include microwave circuit design and wideband efficient power amplifier circuit optimization design.



Wence ZHANG received the B.S. and Ph.D. degrees at Southeast University, China, in 2009 and 2015, respectively. From Sept. 2013 to Sept. 2014, he was a visiting student in Department of Electronics, University of York, UK. From Sept. 2015 to Sept. 2016, he was a postdoc researcher in CETUC, PUC-Rio, Brazil. Since Sept. 2016, he has been an associate professor in Jiangsu University, China. He serves as an associate editor for *IEEE Access* and has served as a TPC member for many conferences including IEEE ICC and IEEE GLOBECOM. His research interests include channel knowledge map, mmWave massive MIMO, and integrated sensing and communications.



Xiaowei ZHU received the M.E. and Ph.D. degrees in electronic and information engineering from Southeast University, Nanjing, China, in 1996 and 2000, respectively. Since 1984, he has been with Southeast University, where he is currently a Professor with the School of Information Science and Engineering. He has authored or coauthored more than 100 technical publications. He holds over 25 patents. He was a recipient of IEEE Microwave Theory and Techniques Society 2021 Microwave Prize and the 2003 Second-Class Science and Technology Progress Prize of Jiangsu Province, China. His current research interests include radio frequency and antenna technologies for wireless communications, microwave and mmWave theory and technology, and also PA nonlinear characteristics and its linearization research with a particular emphasis on wideband and high-efficiency GaN PAs.