

# Effective length factor of a non-symmetrical cross-bracing system with a discontinuous diagonal

***Key words:*** Non-symmetrical cross-bracing system, Discontinuous diagonal, Out-of-plane buckling analysis, Effective length factor

***Cite this as:*** Yong Chen, Yong Guo, Hai-wei Xu, 2019. Effective length factor of a non-symmetrical cross-bracing system with a discontinuous diagonal. *Journal of Zhejiang University-SCIENCE A (Applied Physics & Engineering)*, 20(8):590-600.  
<https://doi.org/10.1631/jzus.A1900169>

# Backgrounds

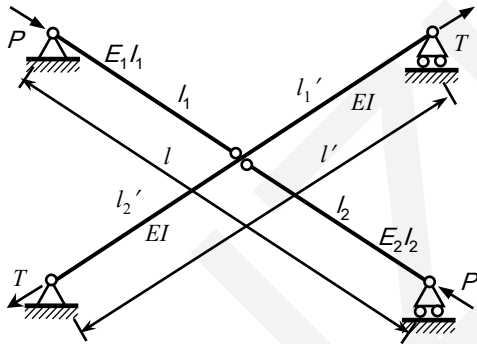
- ❑ Cross-bracing systems are widely adopted in offshore structures, transmission towers, to resist lateral loadings such as wind and earthquake.
- ❑ non-rectangular frame panels might result in geometrical asymmetry of a cross-bracing system, e.g. cross-bracing systems in transmission tower structures.
- ❑ Wind-induced out-of-plane buckling of cross-bracing system may lead to failure or even collapse of a transmission tower.



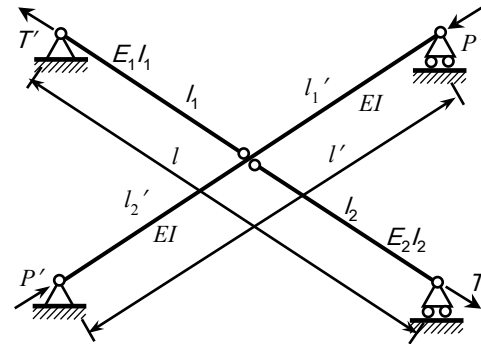
Out-of-plane buckling collapse of transmission tower

# Objectives

- Elastic out-of-plane buckling of a completely non-symmetrical X-bracing system with a discontinuous diagonal under a general case, i.e. continuous and discontinuous diagonals with different lengths and cross-sections, and intersection points not fixed at their mid-spans



(a) Discontinuous compression diagonal

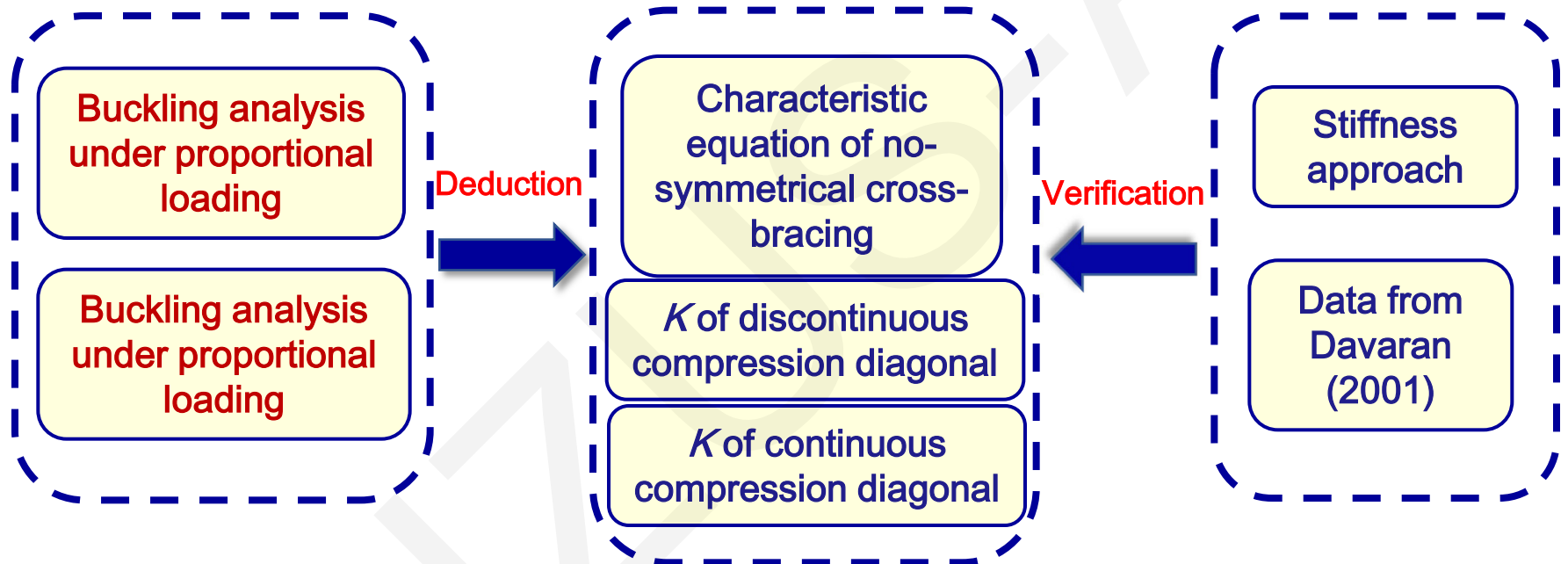


(b) Discontinuous tension diagonal

A general non-symmetrical X-bracing system with a discontinuous diagonal

# Methods

- Cross-bracing system with a discontinuous diagonal -- Effective length factor  $K$



# Results

- The characteristic equation of a general non-symmetrical cross bracing system

$$1 = \alpha'(1-\alpha')\beta_0\sqrt{\beta_0\hat{\gamma}_0} \sinh(\sqrt{\beta_0\hat{\gamma}_0}) / [(1-\alpha')\alpha'\sqrt{\beta_0\hat{\gamma}_0} \sinh(\sqrt{\beta_0\hat{\gamma}_0}) - \sinh(\sqrt{\beta_0\hat{\gamma}_0}) - \sqrt{\beta_0\hat{\gamma}_0}\alpha' \sinh(\sqrt{\beta_0\hat{\gamma}_0}\alpha')]$$

- Effective length factor of a non-symmetrical cross-brace with a discontinuous compressive diagonal,  $K$

$$K = \begin{cases} \sqrt{v}\psi(\xi_1\xi_2 + 0.5), & \beta_0 < \beta_{0cr} \\ 1, & \beta_0 \geq \beta_{0cr} \end{cases}, \quad \xi_1 = \frac{\mu_\xi(\alpha') - 0.5}{\mu_\xi(0.5) - 0.5}, \quad \xi_2 = \begin{cases} -0.07586\bar{\beta}^4 + 0.31064\bar{\beta}^3 - & \beta_0 \geq -1 \\ 0.54441\bar{\beta}^2 + 0.91557\bar{\beta}, & \beta_0 \geq -1 \\ -0.0007\bar{\beta}^4 + 0.0153\bar{\beta}^3 - & \beta_0 < -1 \\ 0.1279\bar{\beta}^2 + 0.6999\bar{\beta}, & \beta_0 < -1 \end{cases}$$

$$\begin{aligned} \mu_\xi(\alpha') &= 0.897\alpha'^4 - 1.821\alpha'^3 + 0.617\alpha'^2 + 0.300\alpha' + 2.836, \\ \bar{\beta} &= 8.593 - \frac{8.593}{\mu_\beta(\alpha') + 8}(\beta_0 + 8), \\ \mu_\beta(\alpha') &= -7.29\alpha'^4 + 12.94\alpha'^3 - 9.89\alpha'^2 + 3.79\alpha' + 0.01. \end{aligned}$$

- Effective length factor of a non-symmetrical cross-brace with a continuous compressive diagonal,  $K'$

$$K' = \begin{cases} \frac{1}{1+\kappa(v\beta'-1)^\chi} \left( \alpha' - \frac{\pi}{\sqrt{\gamma'_\infty}} \right) + \frac{\pi}{\sqrt{\gamma'_\infty}}, & v\beta' > 1 \\ 1 - v\beta' + v\beta'\alpha', & v\beta' \leq 1 \end{cases}, \quad \begin{aligned} \kappa &= (-8.1004 + 37.6598\alpha' - 59.7324\alpha'^2 + 33.4999\alpha'^3)^{-1}, \\ \chi &= 0.8472 + 0.4438\alpha'. \end{aligned}$$

# Conclusions

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- ❑ The characteristic equation of a completely non-symmetrical cross bracing system is similar to the expression of characteristic equation of a geometrically mono-symmetrical system.
- ❑ When under compression, the discontinuous diagonal may buckle before the continuous diagonal and is thereby the control case in determining critical loading of a cross bracing system.
- ❑ The out-of-plane buckling of the discontinuous compression diagonal will show a pure sway mode on condition that 1) the non-dimensional stiffness is less than a critical value, or 2) the ratio of tension to compression, is less than a critical value.
- ❑ For design purposes, Direct closed-form equations of the effective length factor were formulated for a general cross-bracing system and their validity was verified through case studies.