

# **Numerical modeling and experimental study of microstamping process for fabricating microchannels using thin sheets of titanium**

Wenze MAO, Yancheng WANG, Deqing MEI,  
Lingfeng XUAN, Caiying ZHOU

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# Constitutive Modeling

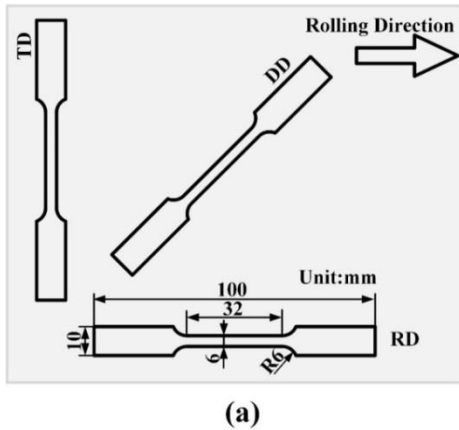


Fig. 1 The tensile testing specimens

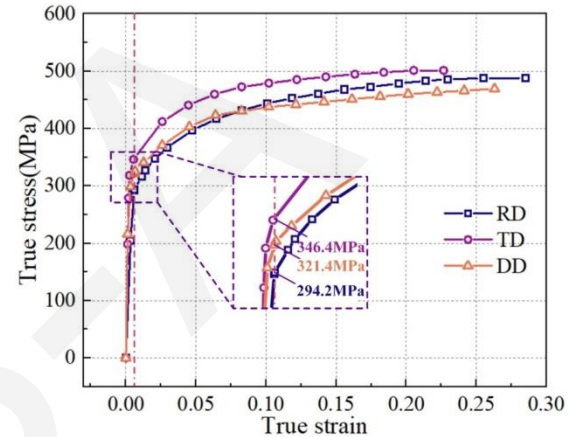
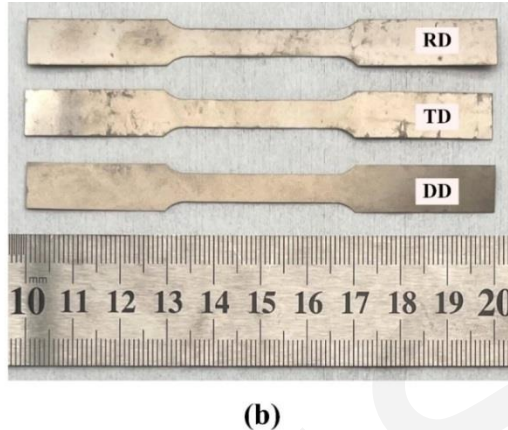


Fig. 2 The true stress-true strain curves

## Off-axis elastic modulus

$$E_x(\theta) = \frac{1}{S_{11}} = \left[ \frac{1}{E_1} m^4 + \left( \frac{1}{G_{12}} - \frac{2\nu_1}{E_1} \right) m^2 n^2 + \frac{1}{E_2} n^4 \right]^{-1}$$

## Voce hardening law

$$\sigma = s + A(1 - e^{-m\varepsilon^p})$$

## Hill's yield criterion

$$\bar{\sigma} = \sqrt{(G + H)\sigma_1^2 + (F + H)\sigma_2^2 - 2H\sigma_1\sigma_2 + 2N\tau_{12}^2}$$

least squares method

	F	G	H	N
LS method	0.2035	0.3542	0.5306	1.4096

## stress-strain relationships

$$\sigma(\theta) = \begin{cases} \varepsilon \cdot E_x(\theta), & \varepsilon < \frac{\sigma_s(\theta)}{E_x(\theta)} \\ \sigma_s(\theta) + 169.94 \left[ 1 - e^{-23.44 \left( \varepsilon - \frac{\sigma_s(\theta)}{E_x(\theta)} \right)} \right], & \varepsilon \geq \frac{\sigma_s(\theta)}{E_x(\theta)} \end{cases}$$

# Constitutive Modeling

- For the Hill's criterion using the least-squares method, the maximum error in the prediction of the yield stress occurs in the RD specimen with 6.3%.
- In the hardening stage, the RD and DD specimen curves are close to each other, and the maximum error occurs in the DD specimen with 8.3%.

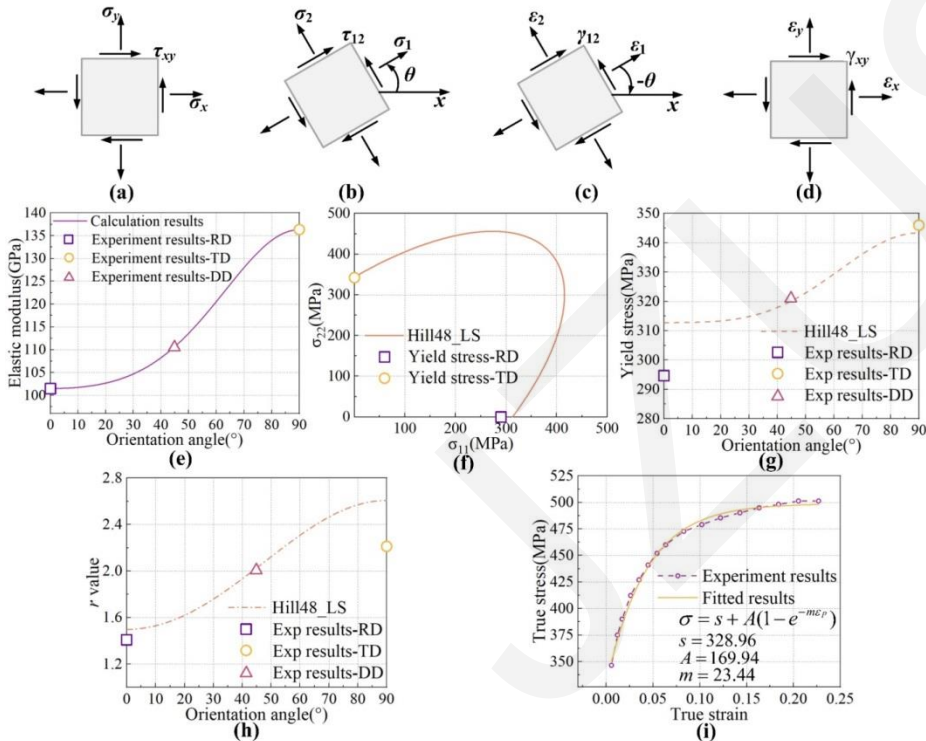


Fig. 3 Establishment of constitutive model

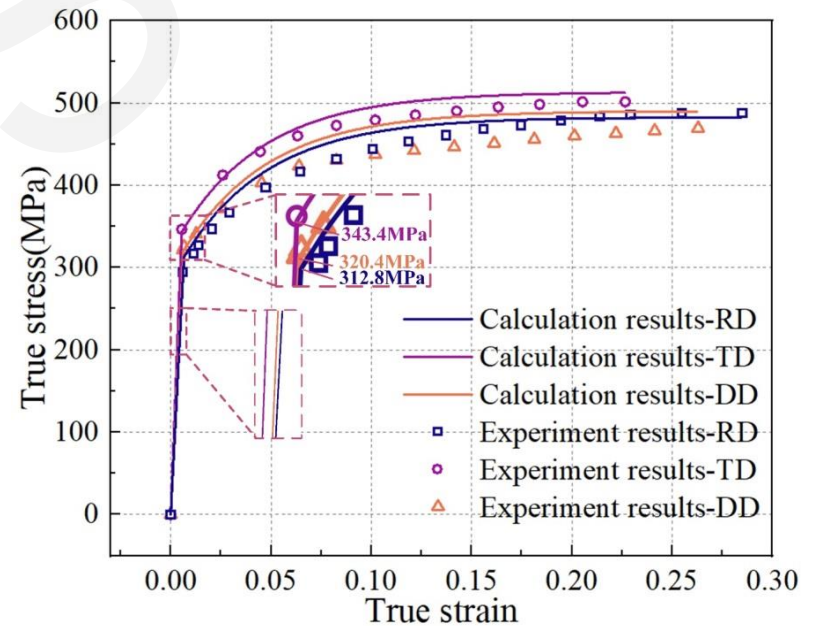


Fig. 4 The comparison of experimental and calculated true stress-true strain curves

# Experimental Setup and Procedure

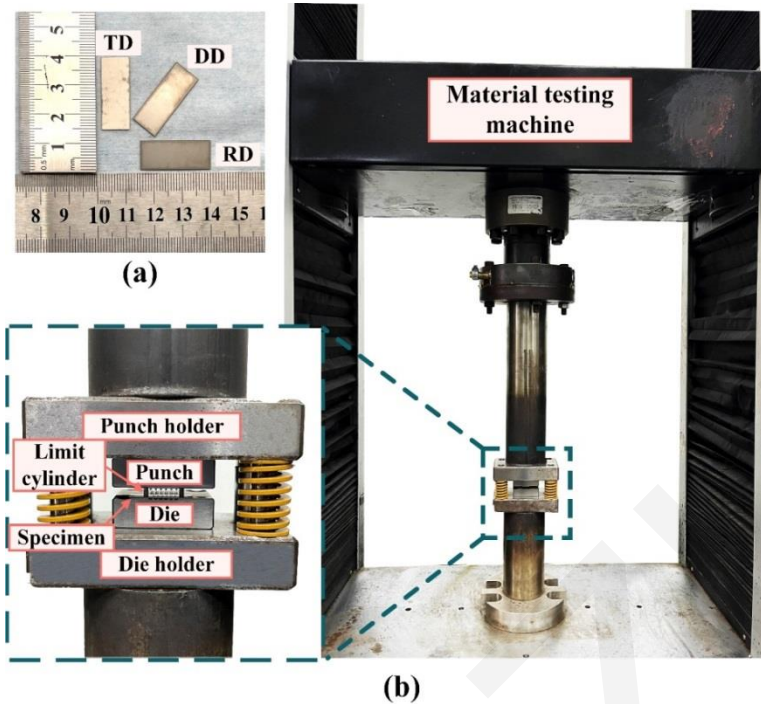


Fig. 6 Experiment of microstamping process

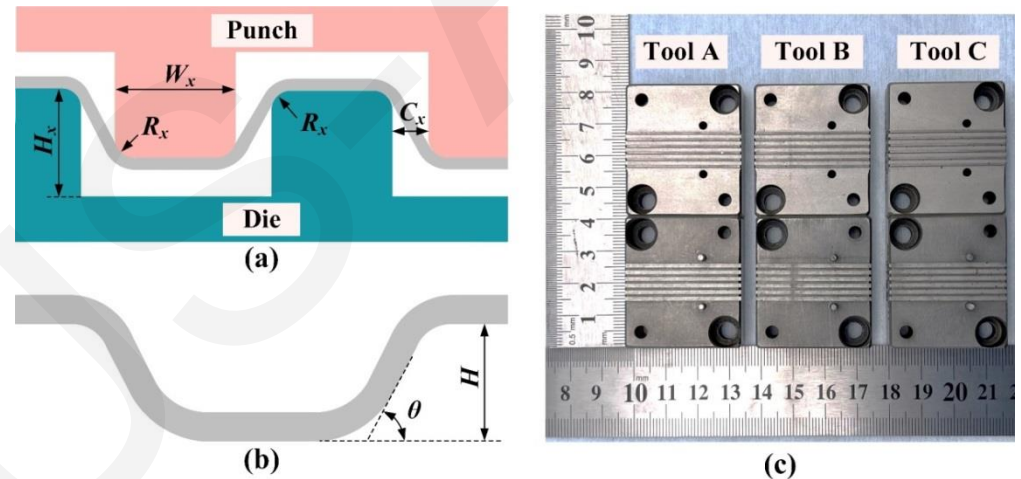
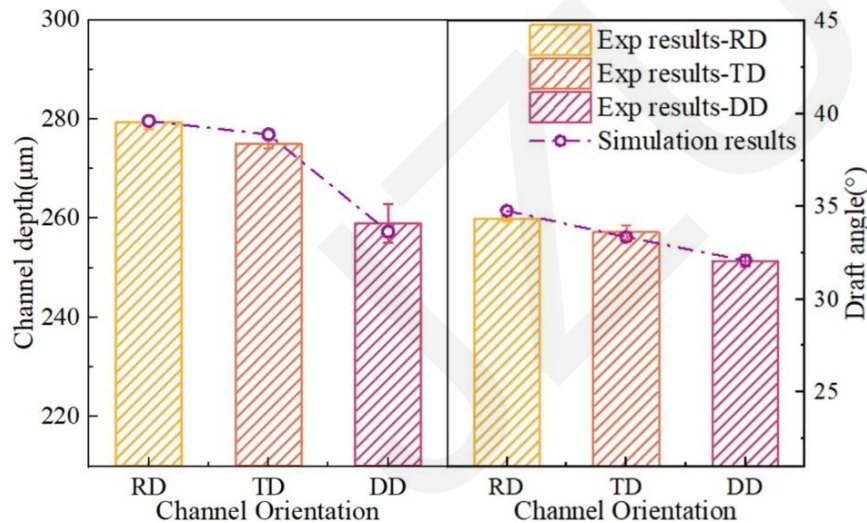
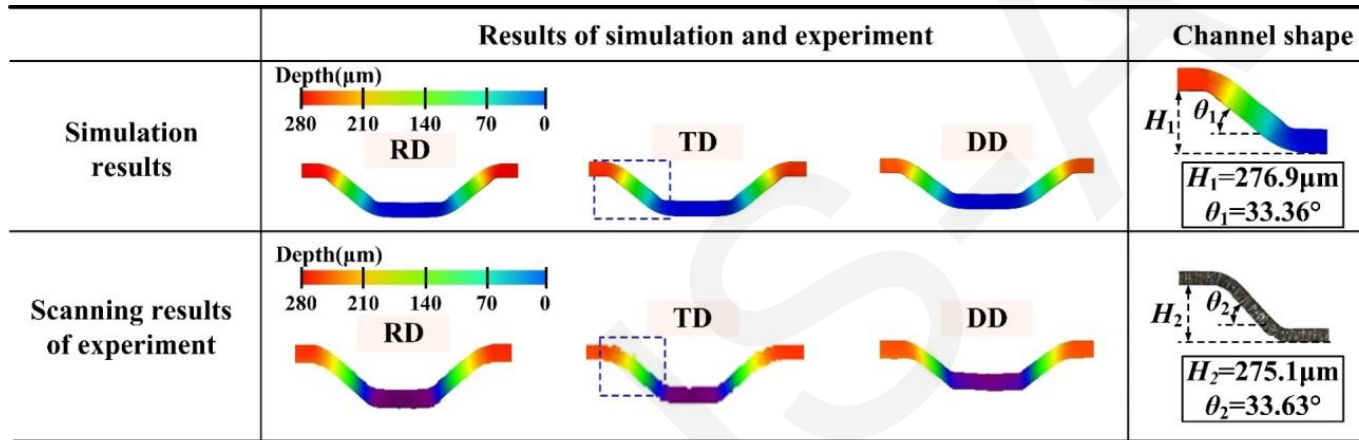


Fig. 7 Schematic diagram of process parameters and tool dimensions

Microstamping experiments were conducted on the **INSTRON 5966 material testing machine**. Three sets of tools were selected for **model verification** and **manufacturing forming** experiments.

# Results and Discussion

## ■ Verification of Model



The micro-stamping model was validated using Tool A. For the channel depth, the maximum error occurred in the TD specimen with 0.7%, while the maximum error in the draft angle occurred in the RD specimen with 1.2%.

Fig. 12 Simulation and experiment results of microstamping

# Results and Discussion

## Simulation Results of Microstructures Stamping

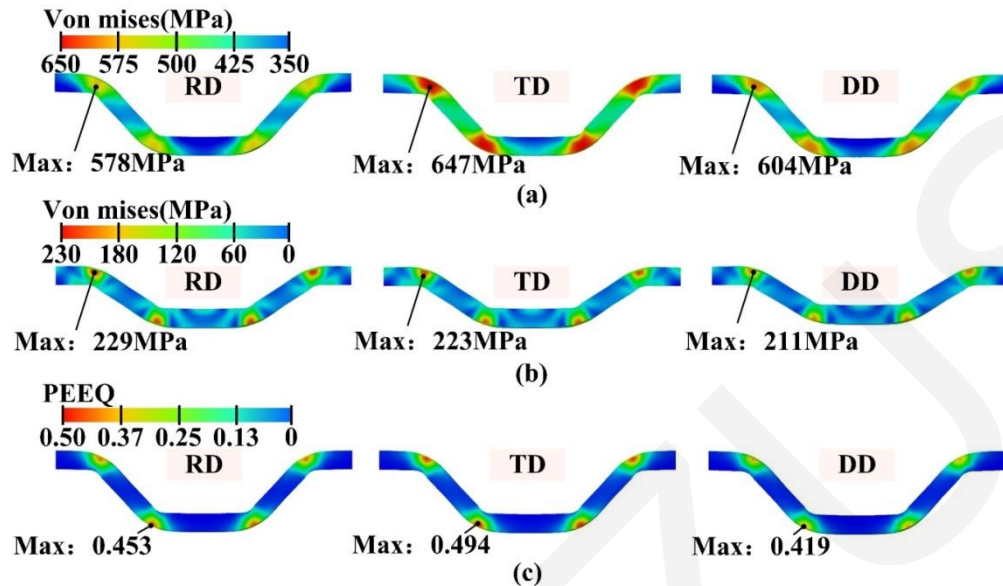


Fig. 8 The distribution of stress and plastic strain with different orientations under different microstamping stages

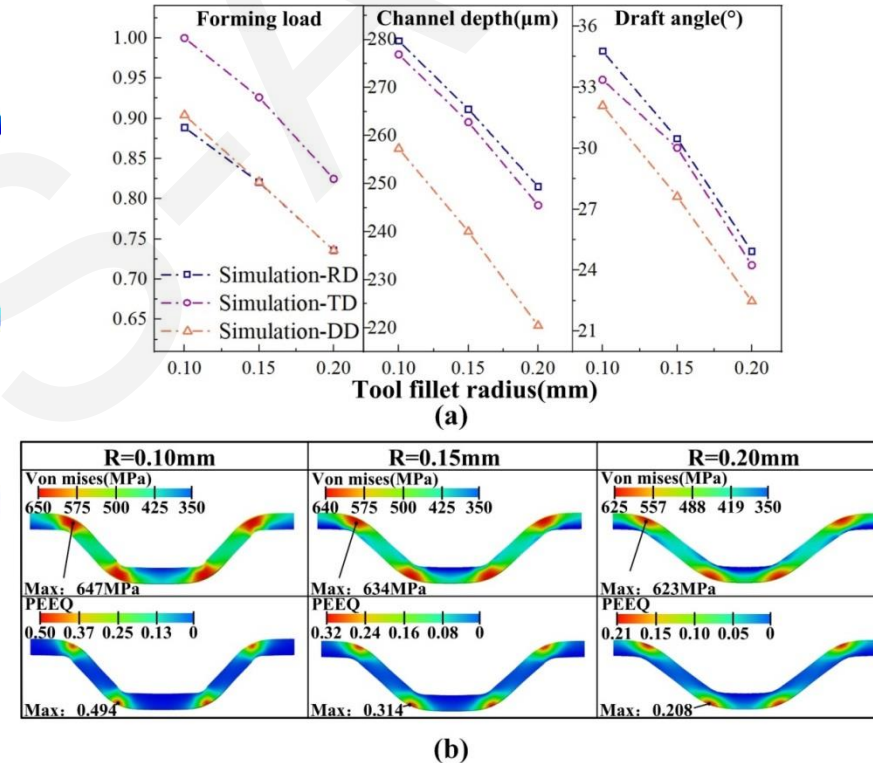


Fig. 9 Effects of tool fillet radius

- We explain the **springback anisotropy** of titanium sheet during microstamping from the **stress** and **strain** analysis.
- Compared to **tool clearance** and **punch width**, the decrease in **tool fillet** causes a **greater depth increase** and a **milder stress concentration**.

# Results and Discussion

## ■ Microstructures Manufacturing Result

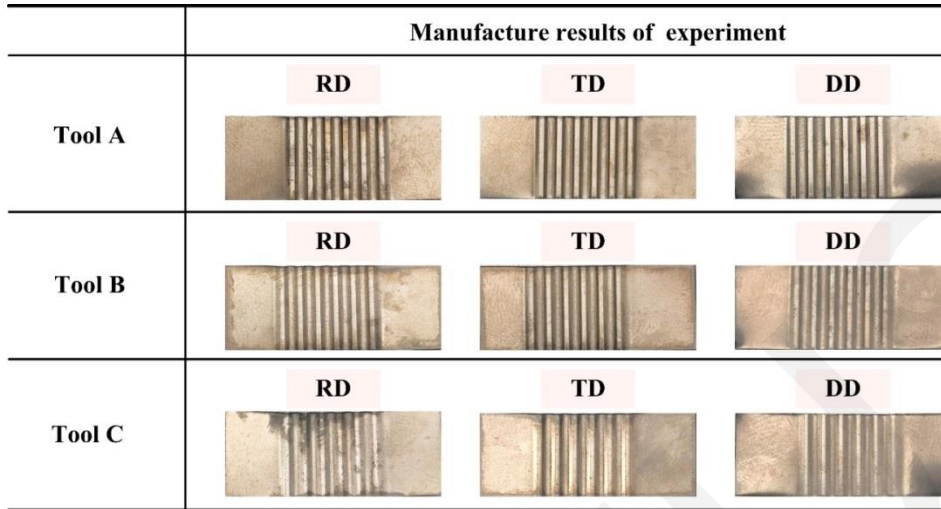


Fig. 13 Microchannels fabrication results

Central channels' depth and draft angle are less than edge channels'. Due to the anisotropy, the RD channel has minimal springback. We chose RD channel with 0.1mm fillet radius to fabricate channels with 279.3  $\mu\text{m}$  depth and 34.34° draft angle.

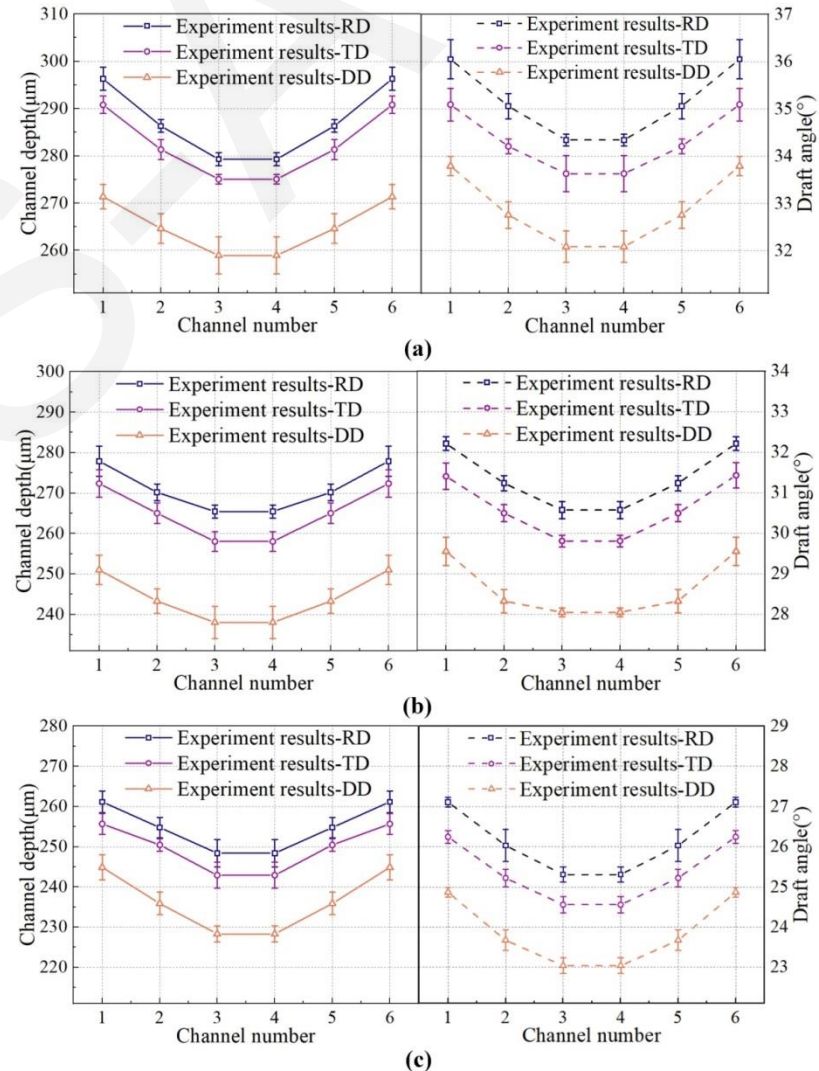


Fig. 14 The measured evaluation indicators

# Conclusions

- The orthogonal constitutive model can accurately predict the elastic-plastic behavior of titanium sheet and the microstamping simulation model can accurately predict springback.
- The anisotropy of titanium sheet in microstamping processing leads to different degrees of forming load and springback for specimens with different orientations
- Channels with a depth of 279.3  $\mu\text{m}$  and a draft angle of  $34.34^\circ$  was fabricated by selecting RD specimens and a tool with a fillet radius of 0.10 mm.