



Bone implants with triply periodic minimal surface architectures: design, fabrication, and biological performance

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Abstract

Triply periodic minimal surface (TPMS)-based bone implants are an innovative approach in orthopedic implantology, offering customized solutions for bone defect repair and regeneration. This review comprehensively examines the current research landscape of TPMS-based bone implants, addressing key challenges and proposing future directions. It explores design strategies aimed at optimizing mechanical strength and enhancing biological integration, with a particular emphasis on TPMS structures. These design strategies include graded, hierarchical, and hybrid designs, each contributing to the overall functionality and performance of the implants. This review also highlights state-of-the-art fabrication technologies, particularly advancements in additive manufacturing (AM) techniques for creating metal-based, polymer-based, and ceramic-based bone implants. The ability to precisely control the architecture of TPMS structures using AM techniques is crucial for tailoring the mechanical and biological properties of such implants. Furthermore, this review critically evaluates the biological performance of TPMS implants, focusing on their potential to promote bone ingrowth and regeneration. Key factors, such as mechanical properties, permeability, and biocompatibility, are examined to determine the effectiveness of these implants in clinical applications. By synthesizing existing knowledge and proposing innovative research directions, this review underscores the transformative potential of TPMS-based bone implants in orthopedic surgery. The objective is to improve clinical outcomes and enhance patient care through advanced implant designs and manufacturing techniques.

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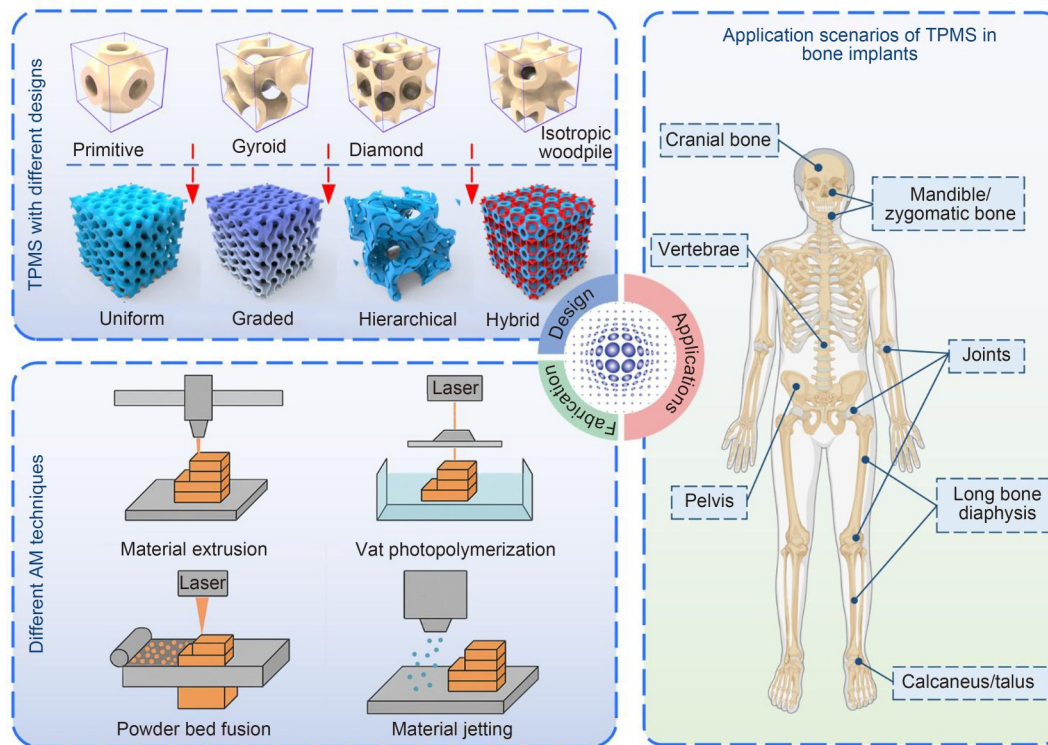
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Graphical abstract



Keywords Triply periodic minimal surface · Bone implants · Design method · Additive manufacturing · Biological performance

1 Introduction

Bone implants play a crucial role in orthopedic and dental surgeries, significantly enhancing the quality of life of patients with bone defects or bone degeneration [1]. These implants replace or support damaged bones, thereby helping restore function and alleviate pain. The design and material properties of these implants are crucial for their success, as they must seamlessly integrate with host tissue while enduring mechanical loads [2]. Traditionally, bone implants have been made from dense, nonporous materials like titanium and its alloys, which are known for their excellent mechanical strength and biocompatibility [3]. However, these dense materials often fail to mimic the intricate, hierarchical structure of natural bone, which is essential for effective osseointegration [4]. This limitation has spurred the development of new approaches that incorporate porous structures to better replicate natural bone environments [5].

One of the most promising advancements in porous bone implants is the use of triply periodic minimal surfaces (TPMSs) [6]. TPMSs are a unique class of mathematical

surfaces characterized by their periodicity in three dimensions and their minimal surface area for a given volume. These structures provide high interconnectivity and porosity, which can be precisely controlled through computational design. Examples of TPMS structures include gyroid, Schwarz D, and diamond surfaces, each offering complex geometries that can be tailored to meet specific mechanical and biological requirements [7]. The use of TPMS in bone implants offers several significant advantages. These intricate geometries can be engineered to achieve high strength-to-weight ratios, closely mimicking the mechanical properties of natural bone [8]. This is particularly beneficial for load-bearing applications, where the implant must support physiological loads without failing. Additionally, the interconnected porosity of TPMS structures promotes vascularization and bone ingrowth, which are crucial for the successful integration of the implant with the host bone. This network of interconnected pores facilitates nutrient exchange and waste removal, thus promoting healthy bone tissue development around the implant [9, 10].

The design process is a critical first step in developing effective TPMS-based bone implants, as it directly influences their mechanical and biological performance [11]. This process involves various innovative methods for optimizing the functional properties of implants. Graded design techniques enable the creation of implants with spatially varying properties, mimicking the natural gradation of bone tissue and enhancing the integration between the implant and host bone [12]. Hierarchical design approaches incorporate multiple levels of porosity, from macro to micro scales, to replicate the complex structure of natural bone, thereby improving mechanical stability and biological compatibility [13]. Furthermore, hybrid designs combine different TPMS geometries or integrate TPMS structures with other elements, leveraging the strengths of various configurations to achieve implants with tailored mechanical properties and enhanced functionality [14]. These diverse design methodologies have collectively contributed to the development of advanced TPMS-based bone implants that closely mimic natural bone and meet specific clinical requirements [15].

TPMS-based bone implants are primarily produced using various additive manufacturing (AM) techniques that enable the precise construction of complex geometries inherent to TPMS designs [16]. Laser powder bed fusion (LPBF) is a prominent technique for fabricating metallic implants, particularly with materials such as titanium and its alloys, because of their excellent mechanical properties and biocompatibility [17, 18]. For polymer-based implants, techniques, such as fused deposition modeling (FDM) [19, 20] and stereolithography (SLA) [21, 22] are commonly used. These methods are advantageous for creating lightweight, flexible structures that can be tailored to specific biological and mechanical requirements. Ceramics, which are also known for their outstanding wear resistance and biocompatibility, are often fabricated using extrusion-based AM [23] and digital light processing (DLP) [24, 25]. These techniques enable the creation of intricate TPMS structures that support bone ingrowth and ensure long-term stability in orthopedic applications. The choice of material and manufacturing method is carefully selected based on the specific properties required for the final implant, ensuring that it meets the stringent demands of biomedical applications.

As the field of orthopedic and dental implantology continues to advance, the integration of AM techniques with innovative design principles is crucial for the development of TPMS-based bone implants [26]. The unique geometric properties of TPMS structures, combined with recent progress in computational design and AM, hold significant potential for improving patient outcomes. Despite the rapid growth of research on TPMS structures over the past decade, encompassing numerous studies on design, fabrication, and performance, a comprehensive review specifically focused on TPMS-based bone implants has yet to be published. This

review aims to bridge this gap by thoroughly examining the design, fabrication processes, and biological performance of TPMS-based bone implants. Building on this foundation, this review aims to consolidate existing knowledge, identify key challenges, and propose future research directions. The structure of this review, as outlined in Fig. 1, is as follows. Section 2 discusses design strategies. Section 3 summarizes the

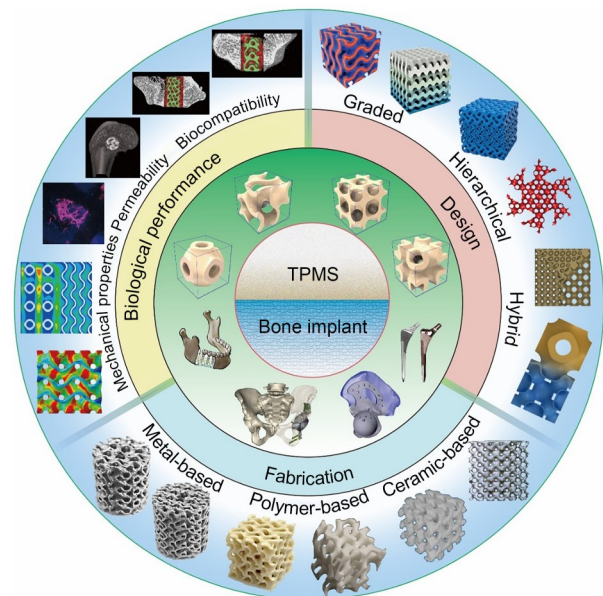


Fig. 1 Overview of TPMS-based bone implants: design, fabrication, and biological performance. Images for “Bone implant” were reproduced from [27] (Copyright 2023, with permission from the authors, licensed under CC BY), [28] (Copyright 2022, with permission from the authors, licensed under CC BY), and [29] (Copyright 2022, with permission from the authors, licensed under CC BY). Images for “Graded” were reproduced from [30] (Copyright 2020, with permission from the authors, licensed under CC BY) and [31] (Copyright 2022, with permission from the authors, licensed under CC BY). Images for “Hierarchical” were reproduced from [32] (Copyright 2020, with permission from the authors, licensed under CC BY) and [33] (Copyright 2021, with permission from the authors, licensed under CC BY-NC-ND). Images for “Hybrid” were reproduced from [34] (Copyright 2020, with permission from John Wiley & Sons, Ltd.) and [35] (Copyright 2022, with permission from the authors, licensed under CC BY-NC-ND). Images for “Ceramic-based” were reproduced from [36] (Copyright 2023, with permission from Elsevier) and [37] (Copyright 2023, with permission from Elsevier). Images for “Polymer-based” were reproduced from [38] (Copyright 2022, with permission from the authors, licensed under CC BY) and [39] (Copyright 2023, with permission from the authors, licensed under CC BY-NC-ND). Images for “Metal-based” were reproduced from [40] (Copyright 2021, with permission from ASM International). Image for “Mechanical properties” was reproduced from [41] (Copyright 2020, with permission from the authors, licensed under CC BY-NC-ND). Image for “Permeability” was reproduced from [42] (Copyright 2024, with permission from Elsevier). Images for “Biocompatibility” were reproduced from [43] (Copyright 2022, with permission from Elsevier), [44] (Copyright 2023, with permission from Wiley-VCH GmbH), and [45] (Copyright 2022, with permission from the authors, licensed under CC BY)

fabrication methodologies. Section 4 presents the biological performance analysis. Finally, Section 5 presents the conclusions and future prospects.

2 Design of TPMS-based bone implants

The development of TPMS-based bone implants relies heavily on the design process and their biological performance, which are critical for successful clinical applications. Effective design ensures that these implants not only mimic the mechanical properties of natural bone—providing necessary strength and flexibility to withstand physiological loads without causing stress shielding—but also promote optimal biological integration [43]. The key aspects of biological performance include mechanical strength, permeability, and biocompatibility [46–48]. The intricate TPMS structures achieve high permeability, which is essential for nutrient transport, waste removal, and vascularization, facilitating integration with host bone tissue [49, 50]. Biocompatibility is crucial because the materials and surface properties must support cell attachment, proliferation, and differentiation without triggering adverse immune responses [51]. Furthermore, the interconnected porous architecture inherent in TPMS designs promotes bone ingrowth and osseointegration, enhancing long-term stability and functionality [52, 53]. By carefully considering factors such as porosity, pore size, and interconnectivity during the design process, TPMS structures can replicate the hierarchical structure of natural bone, ultimately leading to improved patient outcomes.

2.1 TPMS-based structures

The smooth and continuous surfaces of TPMS minimize stress concentration, thereby improving the mechanical performance and durability under physiological loads. The ability to precisely control the pore size and distribution within TPMS structures allows for the customization of mechanical properties to closely match those of natural bone, thereby

reducing the risk of implant failure. Additionally, the inherent geometrical complexity of TPMS can be easily manipulated to facilitate the creation of patient-specific implants with tailored properties to optimize clinical outcomes [54].

Several types of TPMSs, including gyroid, primitive, isotropic woodpile (IWP), and diamond (Fig. 2a), have been used to design bone implants, each characterized by distinct equations and morphologies, as illustrated in Table 1 [55]. These varied morphologies and mathematical formulations allow for the customization of bone implants to meet specific clinical requirements, thereby optimizing mechanical performance and biological compatibility [56].

Moreover, two types of bone scaffolds (Fig. 2c) based on TPMS have been proposed: skeletal and sheet [57]. Skeletal scaffolds are characterized by their framework-like structure, which provides high mechanical strength and rigidity, making them suitable for load-bearing applications. Their open framework facilitates excellent nutrient flow and waste removal, promoting efficient cell migration and bone ingrowth [58]. In contrast, sheet scaffolds feature thin, continuous surfaces that offer a high surface area-to-volume ratio, which is beneficial for cell adhesion and proliferation. The sheet structure can be designed to have varying degrees of flexibility and porosity, allowing for customization based on the specific requirements of the implant site [59]. It has been verified that sheet topologies, particularly sheet diamond, demonstrate 1.3–2.0 times higher peak and plateau stress values than skeletal topologies, while also demonstrating superior toughness [60].

The pore size of TPMS-based bone implants (Fig. 2b) significantly influences their biological and mechanical performance [7]. Optimal pore sizes facilitate cell migration, proliferation, and differentiation, which are crucial for effective osseointegration and bone regeneration [61, 62]. Larger pores enhance nutrient and waste exchange, supporting healthier tissue growth, whereas smaller pores contribute to a higher surface area and mechanical interlocking between the implant and surrounding bone. By adjusting the pore size, TPMS-based implants can be engineered to balance

Table 1 Mathematical equations for different TPMSs

TPMS type	Equation $F(x,y,z)$
Primitive	$\cos\left(\frac{2\pi}{a}x\right) + \cos\left(\frac{2\pi}{b}y\right) + \cos\left(\frac{2\pi}{c}z\right) = n$
Gyroid	$\cos\left(\frac{2\pi}{a}x\right)\sin\left(\frac{2\pi}{b}y\right) + \cos\left(\frac{2\pi}{b}y\right)\sin\left(\frac{2\pi}{c}z\right) + \cos\left(\frac{2\pi}{c}z\right)\sin\left(\frac{2\pi}{a}x\right) = n$
Diamond	$\cos\left(\frac{2\pi}{a}x\right)\cos\left(\frac{2\pi}{b}y\right)\cos\left(\frac{2\pi}{c}z\right) - \sin\left(\frac{2\pi}{a}x\right)\sin\left(\frac{2\pi}{b}y\right)\sin\left(\frac{2\pi}{c}z\right) = n$
IWP	$2 \times \left(\cos\left(\frac{2\pi}{a}x\right)\cos\left(\frac{2\pi}{b}y\right) + \cos\left(\frac{2\pi}{b}y\right)\cos\left(\frac{2\pi}{c}z\right) + \cos\left(\frac{2\pi}{c}z\right)\cos\left(\frac{2\pi}{a}x\right) \right) - \cos\left(2 \times \frac{2\pi}{a}x\right)\cos\left(2 \times \frac{2\pi}{b}y\right)\cos\left(2 \times \frac{2\pi}{c}z\right) = n$

F denotes the isosurface determined by the isosurface value n ; a , b , and c denote the constants that control the TPMS unit dimensions in x , y , and z directions, respectively

strength and permeability, ensuring that they can withstand physiological loads while promoting rapid and robust bone healing [63]. This design flexibility makes TPMS-based implants highly versatile and effective for various clinical applications, offering a tailored approach to meet the diverse needs of patients with different bone defects and conditions. Parametric design methods for TPMS scaffolds with programmable pore size distributions have been proposed to effectively govern the pore size for practical application in bone implants [30].

The surface curvature of TPMS-based bone implants also plays a crucial role in their performance [64, 65]. The continuous and smooth curvature of TPMS structures (Fig. 2d) helps distribute stress more evenly across the implant, thereby reducing the likelihood of stress concentrations that could lead to mechanical failure [66]. This curvature enhances the mechanical compatibility of the implant with the natural bone, resulting in a more stable and durable integration. The surface curvature also influences cell behavior, with certain curvatures promoting better cell adhesion, proliferation, and differentiation. Surfaces that not only mimic the mechanical environment of natural bone but also support and enhance the biological processes necessary for successful bone regeneration and integration can be created by fine-tuning the curvature of TPMS-based implants [45].

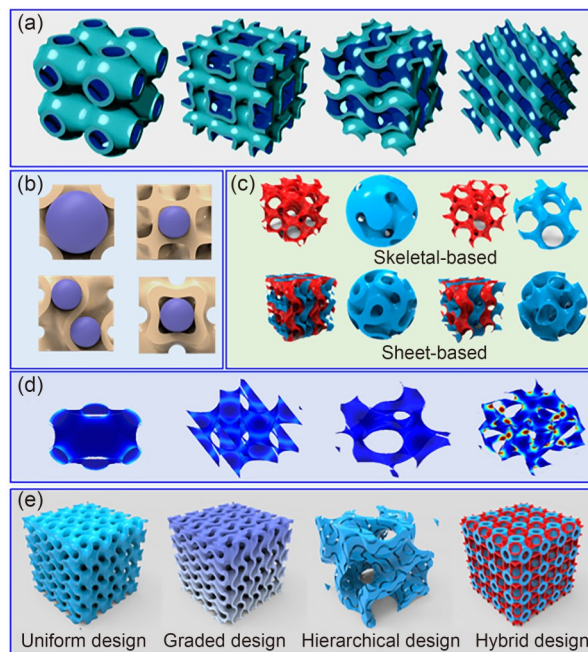


Fig. 2 TPMS-based structures. (a) Four types of TPMSs (reproduced from [67], Copyright 2017, with permission from Acta Materialia Inc.). (b) Pore size of TPMS-based structures (reproduced from [43], Copyright 2022, with permission from Elsevier). (c) Skeletal and sheet structures (reproduced from [30], Copyright 2020, with permission from the authors, licensed under CC BY). (d) Surface curvature of different TPMSs (reproduced from [66], Copyright 2017, with permission from IOP Publishing). (e) Four design strategies of TPMSs

This multifaceted approach makes TPMS-based implants a promising solution for advanced bone repair and replacement therapies.

Based on the flexibility and vast design space of TPMS structures, TPMS-based bone implants can be categorized into uniform, graded, hierarchical, and hybrid designs (Fig. 2e). The key difference among these designs lies in the strategies employed to vary the parameters during the design process, which aim to improve the performance of TPMS-based porous bone implants. The characteristics of these designs are discussed as follows.

2.2 Graded design

The graded design of TPMS-based bone implants involves the creation of structures with spatially varying properties that closely mimic the natural gradation observed in bone tissue (Fig. 3a). Unlike traditional uniform designs, graded designs allow continuous variation of the pore size, porosity, and structural properties of a single implant [68]. This approach enhances the implant's functionality and integration with the host bone. For TPMS-based bone implants, varying the porosity involves designing regions with different pore sizes and densities to optimize mechanical strength and biological integration, promoting better load distribution and enhanced tissue ingrowth. This can be achieved by spatially varying the design parameters in Cartesian space based on specific functions or tabulated data [69]. The graded design for bionic TPMS scaffolds can be achieved by analyzing computed tomography (CT) scans of human bones to determine the pore size and distribution [70].

The design of TPMS-based gradient structures involves several variables, including pore size, porosity, unit cell size, and wall thickness (Fig. 3b). By systematically varying these variables, it is possible to achieve the desired gradient design [71]. The most common gradient involves the uniform variation of these variables along a particular direction; however, they can vary exponentially to create more natural transitions. Typical gradient directions include linear and radial gradients [40]. Linear gradients exhibit consistent changes in variables along a straight line, whereas radial gradients exhibit changes radiating outward from central points. Radial gradients are particularly effective in mimicking the morphological variations of cylindrical bones [72].

Recent advances in the design of TPMS-based gradient structures have led to innovative approaches for mimicking the complex morphologies and mechanical properties of natural bone. Liu et al. [73] designed three distinct linear grading patterns for precise control over surface area and pore size and demonstrated their potential for mimicking host bone morphologies and mechanical properties. Wang et al. [74] proposed a centrosymmetric gradient structure in which the pore size and porosity are varied along an

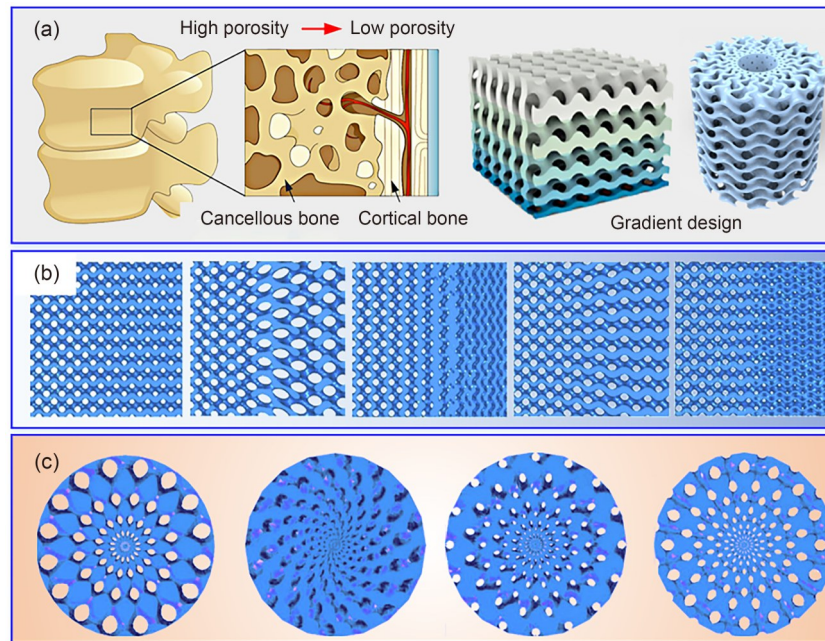


Fig. 3 Graded design of TPMS-based bone implants. (a) Gradient in human bone (reproduced from [31] (Copyright 2022, with permission from the authors, licensed under CC BY) and [76] (Copyright 2023, with permission from Elsevier)). (b) Linear gradient (reproduced from [71], Copyright 2019, with permission from Elsevier). (c) Radial gradient (reproduced from [81], Copyright 2020, with permission from Elsevier)

axisymmetric gradient. For radial gradients (Fig. 3c), Bora et al. [75] employed the gyroid TPMS lattice to parametrically design a functionally graded scaffold with radial grading to replicate the topology of human bone. Numerical investigations have shown that the designed scaffolds closely resemble human cortical bone and satisfy the essential structural requirements. Song et al. [76] proposed a radial-graded porosity design for low-modulus gyroid porous tantalum structures. They found that the radial-graded design exhibited a larger surface area with higher wall shear stress, which can activate cell growth factors and induce stress fiber formation.

For bone implants, the core of the implant should be designed with lower porosity to provide higher mechanical strength, whereas the outer regions may have higher porosity to facilitate bone ingrowth and vascularization [77]. Another approach involves varying the material composition within the implant, such as integrating metal alloys with density gradients or combining metals with bioactive hydrogels to create regions with distinct mechanical and biological properties [78]. Given the various gradient distributions present in actual bones, the design of TPMS-based bone implants can be guided by the real morphological and mechanical performance requirements of human bones [79]. This approach allows for the creation of implants that not only mimic the morphology and mechanical properties of natural bone but also ensure biocompatibility. Moreover, the performance of the implant and its integration with host tissue can be enhanced by tailoring the gradient design to

match the specific structural and functional characteristics of the bone [80].

Some studies on biomimetic scaffold design have integrated TPMS structures and functionally graded porosity to enhance implant mechanical compatibility and biological integration with human bone tissue. For example, Zhang et al. [77] designed and optimized biomimetic scaffold architectures using TPMS structures to achieve mechanical matches with human bone tissues, particularly in load-bearing scenarios. Davoodi et al. [78] developed a functionally graded porosity hip implant by adjusting the local porosity at the implant/tissue interface to enhance the biological response. The gradual decrease in porosity from the surface to the center of the porous construct ensures both biological integration at the interface and mechanical integrity of the implant, providing a robust and biocompatible solution for bone tissue engineering.

2.3 Hierarchical design

Hierarchical design refers to the systematic organization of structural features at multiple scales, from macroscopic to microscopic levels [82]. In the context of bone implants, this approach involves creating a multilevel framework that closely replicates the complex architecture of natural bone (Fig. 4a). By integrating features at various scales, hierarchical design can better emulate the mechanical and biological properties of the bone, ensuring that the implant functions harmoniously within the body [32]. This design methodology

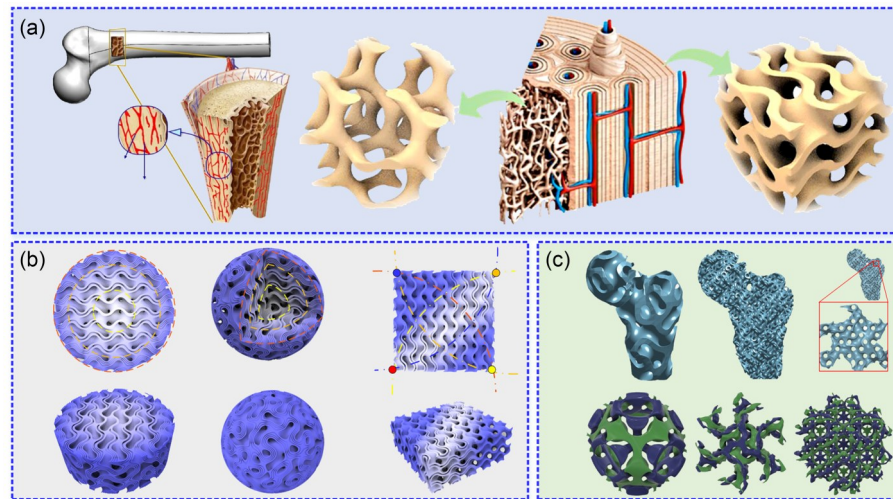


Fig. 4 Hierarchical design of TPMS-based bone implants. (a) Hierarchical pores in human bone (reproduced from [68] (Copyright 2022, with permission from the authors, licensed under CC BY) and [88] (Copyright 2022, with permission from Elsevier)). (b) Multisheet hierarchical design (reproduced from [32], Copyright 2020, with permission from the authors, licensed under CC BY). (c) Hierarchical sheet TPMS lattices (reproduced from [82] (Copyright 2021, with permission from CIRP) and [85] (Copyright 2019, with permission from Elsevier))

(Fig. 4b) is particularly advantageous in enhancing the performance and longevity of bone implants, as it allows for the optimization of strength and biocompatibility. The hierarchical design method based on TPMS offers significant potential benefits by accurately controlling the porosity and pore architecture gradients while preserving the inherent advantages of TPMS geometries [83].

A critical aspect of hierarchical design is the incorporation of multiple scales of porosity. In TPMS-based bone implants, varying the pore size across different scales can significantly impact mechanical stability and biological integration [33]. Larger pores at the macroscopic level facilitate the vascularization and nutrient flow necessary for tissue growth, whereas smaller pores at the microscopic level enhance the surface area required for cell attachment and proliferation. By carefully controlling the distribution and size of these pores, a scaffold that supports robust bone regeneration can be created while maintaining the necessary mechanical strength to withstand physiological loads. Zou et al. [84] proposed a hierarchical porous scaffold based on TPMS by adding small pores on the original TPMS structures to increase their versatility and controllability. Feng et al. [85] constructed hierarchical architectures using fractal-sheet TPMS and external freeform shapes through T-spline surfaces (Fig. 4c). The porosity features can be conveniently controlled in two-dimensional (2D) space according to actual CT images of human bones.

Natural bone exhibits a complex, multiscale architecture with varying degrees of porosity and density. By replicating this intricate structure, TPMS-based implants can achieve a closer resemblance to natural bone, both in form and function. Li et al. [86] proposed a Haversian system-like hierarchical structure with a pore size varying from the edge

to the center. This biomimetic approach improves the mechanical compatibility of the implant and promotes bone regeneration. Luo et al. [87] introduced TPMS to metallic screws to address stress shielding and postoperative loosening in orthopedic fixation. They found that a stiffer integration between the screw and bone tissue could be achieved with more bone tissue regrowing on the inner surface of the hierarchical screw. Rezapourian et al. [88] designed anatomically matched implants composed of cortical bone mimicking Haversian and Volkmann canals combined with the trabecular-bone-mimicking parts with uniform internal TPMS structures. The optimal design could be achieved by combining pores with different scales to obtain a more successful integration and long-term functionality.

2.4 Hybrid design

Hybrid design refers to an innovative approach for integrating multiple TPMS geometries or combining TPMS structures with other types of structural elements [89, 90]. This approach leverages the strengths of various geometric configurations to create implants that are optimized for specific functional and mechanical requirements [91]. By blending different design elements, hybrid TPMS implants can achieve a superior balance of properties, thereby improving their overall performance and adaptability to medical applications. The TPMS-based hybrid design can be primarily categorized into two approaches. The first approach involves transitioning from one TPMS configuration to another, which is sometimes referred to as a heterostructure gradient in the literature [73]. By gradually changing the TPMS configuration, these implants can provide tailored mechanical properties and biological interactions across different regions

of the implant. The second approach involves fusing multiple TPMS units to adjust the performance of individual unit cells, such as enhancing the anisotropy [92]. This method enables precise control over the mechanical and biological properties of the implant at a microscale level, allowing for the customization of characteristics, such as stiffness, strength, and directional properties. Regions with distinct mechanical behaviors can be created by integrating different TPMS geometries within a single scaffold, thereby improving the overall versatility and functionality of the implant.

Several studies on heterostructure hybridizations have provided a foundation for the advancement of hybrid TPMS metamaterials. For example, Khaleghi et al. [90] proposed the idea of designing hybrid TPMS structures consisting of Schwarz-P/Neovius and each of the other five structures in laminated or matrix-spherical inclusion form to obtain structures with a more uniform directional elastic modulus. The mathematical functions of the hybrid structures were carefully parameterized to ensure a smooth transition between the two structures. They found that hybrid structures have a more uniform directional elastic modulus than their parent structures. They also demonstrated that an appropriate selection of the combination ratio of parent structures leads to the least universal anisotropy. Zhang et al. [93] used a similar approach to construct 1D, 2D, and 3D hybridizations using a Sigmoid function based on the P, IWP, and Forstner random dots (FRD) structures. Gao et al. [35, 94] proposed

a periodic hybrid method for TPMS structures (Fig. 5a) while maintaining the original surface connectivity and structural strength. They used a representative volume element (RVE)-based homogenization method to demonstrate how hybridization expands the designable range of the elastic modulus. Li et al. [95] investigated the impact resistance of several hybrid structures when subjected to high strain-rate loading.

For the unit fusion method, Feng et al. [96] combined different TPMS units to acquire the appropriate elastic modulus and ideal isotropic properties using numerical homogenization theory and finite element analysis methods to build the relationship between the TPMS parameters and elastic modulus or anisotropy properties (Fig. 5b). A curvature-wall thickness adjustment method was proposed to achieve sheet TPMS structures with similar performances to the isotropic properties. Zhao et al. [89] used body-centered cubic and IWP lattice structures as internal and external structures, respectively, to construct interpenetrating lattice structures. They also developed a multiscale optimization framework to simultaneously optimize the distribution of the volume fractions and interpenetrating parameters.

Both hybrid design approaches significantly enhance the diversity and functionality of TPMS-based bone implants. The structural gradient method allows for the creation of implants with varying properties tailored to specific regions, ensuring optimal performance under physiological conditions. The fusion of multiple TPMS units enables detailed

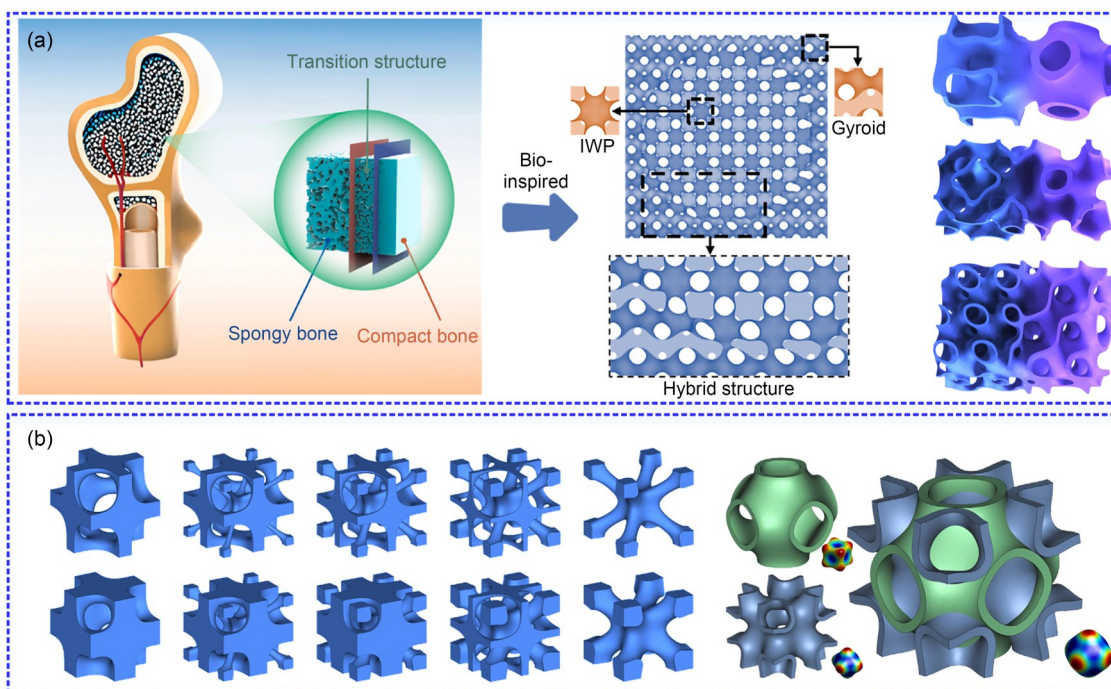


Fig. 5 Hybrid design of TPMS-based bone implants. (a) Transition hybrid design (reproduced from [94] (Copyright 2024, with permission from Elsevier) and [95] (Copyright 2023, with permission from Elsevier)). (b) Unit fusion hybrid design (reproduced from [89] (Copyright 2022, with permission from Elsevier) and [96] (Copyright 2021, with permission from the authors, licensed under CC BY))

customization of the mechanical properties, thereby promoting better integration with natural bone and improving the implant's ability to support tissue regeneration and load-bearing requirements. Overall, these hybrid design strategies represent a promising advancement in the development of next-generation bone implants, offering improved patient outcomes and broader clinical applications.

3 Fabrication of TPMS-based bone implants

The fabrication of TPMS-based bone implants that are characterized by complex and intricate internal structures, primarily relies on AM techniques. The application of AM in bone implants offers several advantages over traditional manufacturing approaches, including increased design flexibility for implant customization, reduced lead time for emergency cases, and the ability to create complex geometries for patient-specific implants. Given the versatility of AM techniques, this review categorizes the fabrication methods into three main types based on the materials used: metal-based, polymer-based, and ceramic-based TPMS implants. Metal-based TPMS implants typically employ techniques like LPBF to produce highly detailed and mechanically robust structures suitable for load-bearing applications. The resulting implants exhibit excellent strength and durability, closely matching the mechanical properties required for bone substitution. There is no fundamental difference in the processes used for different metals, and the different properties of the materials themselves are the key influencing factors for the design and surface modification strategies of bone implants. Therefore, this study focuses on introducing the material characteristics. Polymer-based TPMS implants often employ methods like FDM or SLA to create complex geometries at relatively low costs. Ceramic-based TPMS implants are fabricated using various AM techniques to create implants with excellent bioactivity and osteoconductivity, which are essential for bone regeneration. Ceramic implants offer a balance between mechanical strength and biological functionality, making them ideal for orthopedic and dental applications. Due to the relatively diversified preparation processes of ceramics, we will incorporate the preparation processes of different ceramic bone implants from research-development perspectives.

3.1 Metal-based bone implants

Metal-based AMs have attracted significant attention in the field of bone implants over the past decade. Materials that can be used for the metal-based AM of bone implants include titanium alloys, stainless steel 316L, magnesium (Mg) alloys, nickel–titanium alloys, and tantalum alloys.

These materials are widely used in bone implants for different purposes. This review provides a comprehensive overview of these materials and their preparations for TPMS-based bone implants.

3.1.1 Titanium alloys

Titanium and its alloys, particularly Ti-6Al-4V, are highly favored for orthopedic joint replacements and dental implants because of their high strength-to-weight ratio and good biocompatibility [97, 98]. These materials are particularly chosen for their inertness toward tissues and body fluids, thereby ensuring a secure osseointegration [3]. The bio-inertness of titanium is ensured by a protective film of titanium oxides that form spontaneously on its surface, which prevents the penetration of metal compounds and adheres well to the calcium and phosphate ions necessary for the formation of the mineralized bone structure [99, 100]. The ability of the alloy to be precisely fabricated into complex geometries using AM techniques (Fig. 6a) also enhances its suitability for customized implants [101]. This customization is crucial for patient-specific treatments to ensure better integration with existing bone structures and improve overall patient outcomes. Furthermore, the ongoing advancements in surface modification techniques for Ti-6Al-4V aim to enhance its osseointegration, which is the direct structural and functional connection between the living bone and the surface of a load-bearing implant, thereby promoting faster and more secure healing processes [102, 103].

Yan et al. [104] used selective laser melting (SLM) to manufacture Ti-6Al-4V gyroid and diamond TPMS lattices with interconnected high porosity (80%–95%) and pore sizes ranging from 560 to 1600 μm and from 480 to 1450 μm , respectively, for bone implants. The manufacturability, microstructure, and mechanical properties of these lattices were thoroughly evaluated. The mechanical properties of the fabricated TPMS structures matched the moduli of human bones, and this modification of the modulus and porosity helped reduce stress shielding and increase implant longevity. Ataei et al. [105] employed electron beam melting (EBM) to fabricate Ti-6Al-4V gyroid scaffolds (Fig. 6b) with anisotropic ratios comparable to those of trabecular bone, exhibiting a mixed mode of ductile and brittle behavior under compression. Tilton et al. [106] found that for a similar porosity and applied stress-amplitude, Schoen-IWP scaffolds exhibit significantly higher fatigue life when compared to the primitive (Fig. 6c). Wang et al. [74] created bone scaffolds with excellent mechanical properties, permeability, and cell adhesion capabilities using TPMS and Ti-6Al-4V. The results demonstrated the promising potential of the designed structures for use in artificial bone scaffolds. Therefore, the Ti-6Al-4V TPMS structures fabricated using AM techniques exhibited high porosity and tailored

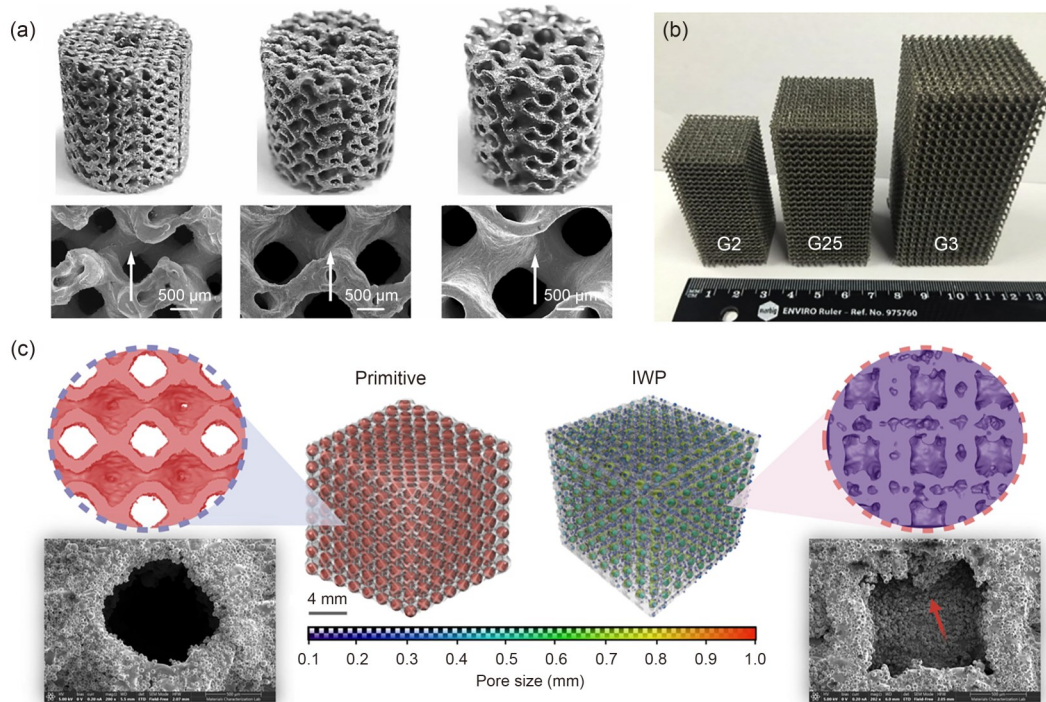


Fig. 6 Fabrication of Ti-6Al-4V TPMS structures for bone implants. (a) Microstructure of 3D-printed graded TPMS scaffolds (reproduced from [40], Copyright 2021, with permission from ASM International). (b) Gyroid scaffolds with different unit cell sizes manufactured by EBM (reproduced from [105], Copyright 2017, with permission from Elsevier). (c) Structural and morphological evaluation of the additively manufactured TPMS scaffolds (reproduced from [106], Copyright 2023, with permission from the Society of Manufacturing Engineers)

mechanical properties resembling human bone. This design flexibility helps mitigate stress shielding and improves implant durability, making these implants promising candidates for advanced bone implants.

Several researchers have proposed process improvements and enhancements to better utilize the fabricated Ti-6Al-4V TPMS structures for bone implants, focusing on their mechanical properties, biocompatibility, stress-shielding mitigation, and fatigue performance. For example, Rezapourian et al. [107] explored Ti-6Al-4V split-P TPMS structures manufactured using SLM and evaluated two cell morphologies with varying densities. They found that the elastic modulus, yield strength, and strength of the fabricated parts approached the mechanical properties of the trabecular and cortical bone. Liao et al. [40] fabricated Ti-6Al-4V scaffolds with radial gradient porosity distributions using SLM to mimic natural bone structures. The scaffolds exhibited varying porosities (55%–71%) and pore sizes (333–674 µm), with mechanical properties (Young's modulus: 2.7–7.4 GPa; yield strength: 233–520 MPa) suitable for orthopedic applications. Biocompatibility was demonstrated by performing cell viability assays. Song et al. [11] proposed porous root analog implants of Ti-6Al-4V using TPMS structures to mitigate stress shielding and promote osteoblast growth. Compression experiments and finite element analysis demonstrated that implants with 30% and 40% porosity

effectively prevented stress shielding, enhanced bone tissue integration, and optimized clinical implantation outcomes. Tilton et al. [106] investigated the fatigue performance of Ti-6Al-4V scaffolds designed using TPMS, highlighting the impact of structural design and manufacturing variability on metabiomaterials. They found that the Schoen-IWP scaffold exhibited a 97% higher fatigue life than the primitive scaffold. The primitive scaffolds closely replicated the compressive mechanical properties of the trabecular bone.

3.1.2 Stainless steel 316L

Stainless steel is another prominent material used in AM for TPMS-based bone implants because of its favorable mechanical properties, biocompatibility, and cost-effectiveness [108]. Known for its excellent corrosion resistance and strength, stainless steel 316L is particularly suited for medical applications where durability and reliability are critical [109]. The application of stainless steel 316L in AM allows for the creation of intricate TPMS structures (Fig. 7a) that closely mimic the porosity and mechanical properties of natural bone, thereby promoting better osseointegration and tissue ingrowth. Despite its advantages, one of the challenges with stainless steel 316L is its relatively high elastic modulus compared to natural bone, which can lead to stress shielding. However, advancements in AM techniques have enabled the production of optimized porous structures that can

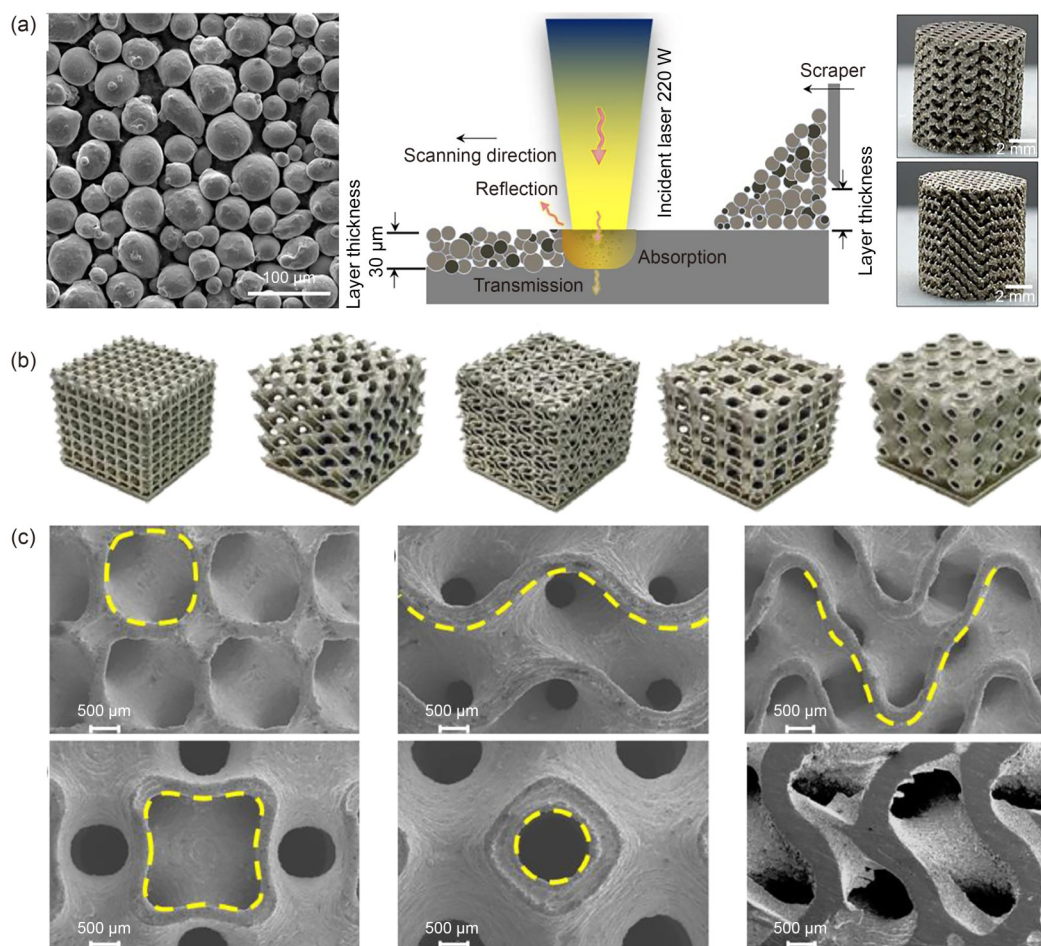


Fig. 7 Fabrication of stainless steel TPMS structures for bone implants. (a) SLM process for the fabrication of stainless steel lattice structures, including the powder and fabricated TPMS structures (reproduced from [114] (Copyright 2023, with permission from the authors, licensed under CC BY) and [115] (Copyright 2024, with permission from Elsevier)). (b) Fabricated TPMS lattice structures using stainless steel 316L (reproduced from [109], Copyright 2023, with permission from Elsevier). (c) SEM images of fabricated surfaces (reproduced from [109], Copyright 2023, with permission from Elsevier). SEM: scanning electron microscope

mitigate this issue, making stainless steel 316L a viable option for producing effective and long-lasting TPMS-based bone implants [110].

Wang et al. [111] compared the mechanical properties and cytotoxicity of TPMS gyroid and other porous structures fabricated from stainless steel 316L using SLM at various relative densities. They found that TPMS structures exhibit favorable Young's modulus and excellent biocompatibility, highlighting their potential for biomedical applications. Szatkiewicz et al. [112] investigated the mechanical properties and energy absorption capabilities of cylindrical TPMS structures with shell gyroid unit cells fabricated from stainless steel 316L under compression loading. Ravichander et al. [109] evaluated the mechanical and electrochemical properties of sheet-based TPMS lattices (Figs. 7b and 7c) fabricated from stainless steel 316L, revealing enhanced corrosion resistance compared to solid samples and offering valuable insights for biomedical applications. Ma

et al. [113] examined the suitability of stainless steel 316L gyroid structures for bone scaffolds by analyzing their mechanical properties and fluid dynamics. They found that increasing the volume fraction improved the elastic moduli and yield stresses and that the fluidity of the structures enhanced nutrient transport. These studies confirmed that stainless steel 316L TPMS structures exhibit excellent mechanical properties, corrosion resistance, and biocompatibility, making them promising for various biomedical applications.

Foroughi et al. [116] fabricated TPMS scaffolds for bone tissue engineering using stainless steel 316L to ensure that these scaffolds possess essential mechanical strength and biocompatibility, thereby highlighting the suitability of the material for optimizing bone scaffold architectures. Cui et al. [115] created four TPMS structures using stainless steel 316L by incorporating TiB₂ nanoparticles to enhance their mechanical properties. This nanocomposite exhibited improved nano-hardness, ultimate compressive stress, and

Young's modulus compared to plain stainless steel, closely matching the human cortical bone strength. Zhu et al. [117] employed Schwarz primitive TPMS to design novel porous scaffolds, optimizing the scaffold thickness to enhance its mechanical and biological properties. The experimental and numerical results confirmed the enhanced mechanical performance and controlled permeability of the scaffold, demonstrating the effectiveness of the method in tailored scaffold design for biomedical applications. Yang et al. [118] studied the compression–compression fatigue behavior of gyroid cellular structures and revealed enhanced fatigue resistance after sandblasting treatment, which was characterized by reduced cyclic ratcheting and improved high-cycle fatigue performance. These studies underscore the versatility of stainless steel 316L for fabricating TPMS scaffolds with enhanced mechanical properties and biocompatibility, highlighting its potential for advancing bone implant applications.

3.1.3 Mg alloys

Mg and its alloys are emerging as prime candidates for AM of TPMS-based bone implants because of their exceptional physical properties and biocompatibility [119, 120]. Known for their low density, high specific strength, and stiffness,

Mg alloys (Fig. 8a) have been widely used in aerospace and automotive industries as structural metals [121]. Their application in the biomedical field is particularly promising because of their excellent biocompatibility, good osseointegration properties, biodegradability, and elasticity that closely match human bone, thereby reducing the risk of stress shielding [122]. This makes Mg alloys ideal for orthopedic implants. Moreover, Mg-based implants must feature specific geometries that match critical-sized bone defects and highly porous, interconnected structures to facilitate the delivery of nutrients, cells, proteins, and growth factors, thereby promoting bone ingrowth [123].

Temiz et al. [124] employed a casting technology based on infiltration to fabricate controllable porous Mg alloy gyroid structures that were subjected to mechanical testing. They found that Young's modulus of these gyroid structures fell within the range of human trabecular bone but was lower than that of sheep bone, as determined through compression tests and finite element analysis. Ren et al. [125] developed a novel vat photopolymerization-assisted template replacement method for creating intricate TPMS structures with various pore sizes in biodegradable Zn-based porous scaffolds. The resulting Zn–1Mg scaffolds exhibited precise pore structures with a deviation of less than 2% from

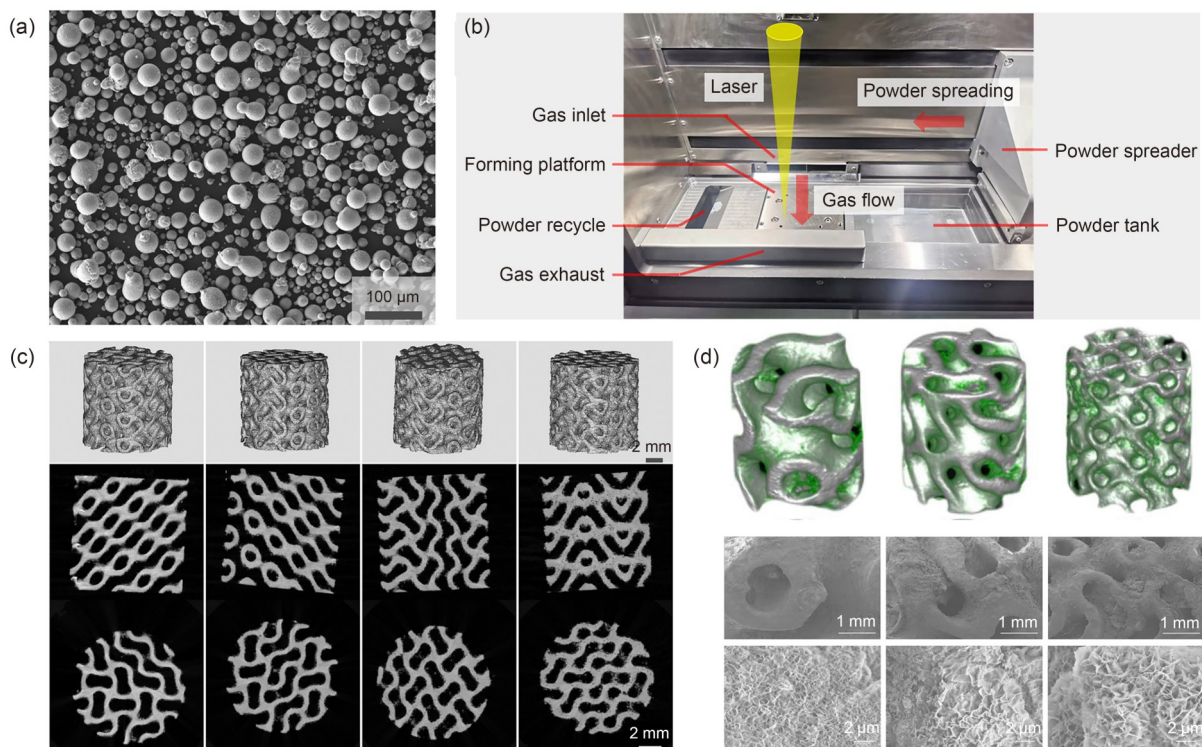


Fig. 8 Fabrication of Mg TPMS structures for bone implants. (a) SEM image of WE43 Mg alloy powder (reproduced from [126], Copyright 2022, with permission from the authors, licensed under CC BY-NC-ND). (b) Setup of the AM processing chamber (reproduced from [126], Copyright 2022, with permission from the authors, licensed under CC BY-NC-ND). (c, d) Formation quality of TPMS-based porous scaffolds by macroscopic and cross-sectional images using μ -CT (reproduced from [126] (Copyright 2022, with permission from the authors, licensed under CC BY-NC-ND) and [127] (Copyright 2023, with permission from the authors, licensed under CC BY-NC-ND)). SEM: scanning electron microscope

the designed porosity, demonstrating excellent mechanical properties, cytocompatibility, and antibacterial activity. These non-AM techniques exemplify effective methods for fabricating precise and functional porous Mg structures.

AM has significantly facilitated the preparation of porous Mg alloy structures, offering great potential for advanced biomedical applications (Figs. 8b and 8c). For example, Wang et al. [127] investigated the effects of pore size in additively manufactured biodegradable porous Mg scaffolds (Fig. 8d) on mechanical properties, biodegradation, and new bone formation. They found that scaffolds with smaller pore sizes exhibited superior mechanical properties, enhanced osteogenic differentiation, and promoted new bone formation, particularly when high-temperature oxidation was applied to improve corrosion resistance. They also examined the influence of the layer thickness on the formation quality, microstructure, mechanical properties, and corrosion resistance of the WE43 Mg alloy and found that increased layer thickness led to enhanced tensile strength and elongation but higher corrosion rates due to more precipitation phases [126]. They also investigated the optimization of LPBF parameters for WE43 Mg alloy porous scaffolds, achieving high structural fidelity and mechanical strength comparable to cancellous bone while demonstrating promising biocompatibility and initial osteogenic effects despite challenges in controlling degradation rates [128]. Yue et al. [129] explored AM of high-porosity Mg alloys for

structural and biomedical applications based on TPMS and found that the structures exhibit interconnected architectures and porosity-dependent properties, with elastic moduli akin to cancellous bone.

3.1.4 Nickel–titanium alloys

Nickel–titanium (Ni–Ti) alloys are highly suitable for AM in TPMS-based bone implants because of their shape memory effect, superelasticity, and high damping capacity [130]. These properties enable the Ni–Ti alloys to recover their shape under stress-free conditions, exhibit large nonlinear recoverable strains, and efficiently dissipate energy as heat, thereby enhancing their energy absorption and mechanical resilience. These characteristics improve the durability, adaptability to dynamic body loads, and patient comfort of bone implants by mitigating vibrations [131]. AM techniques allow precise control over the complex porosity and pore architecture of Ni–Ti TPMS structures (Fig. 9) [132, 133], thereby promoting osseointegration and bone tissue growth and making Ni–Ti alloys a promising material for advanced orthopedic implants [134, 135].

Recent advances in AM have greatly enhanced the design and fabrication of Ni–Ti porous scaffolds. For example, Lv et al. [136] designed several porous scaffolds based on TPMS with consistent porosity but varying pore strategies using a novel Ni46.5Ti44.5Nb9 alloy and SLM technique. They systematically investigated the effects of

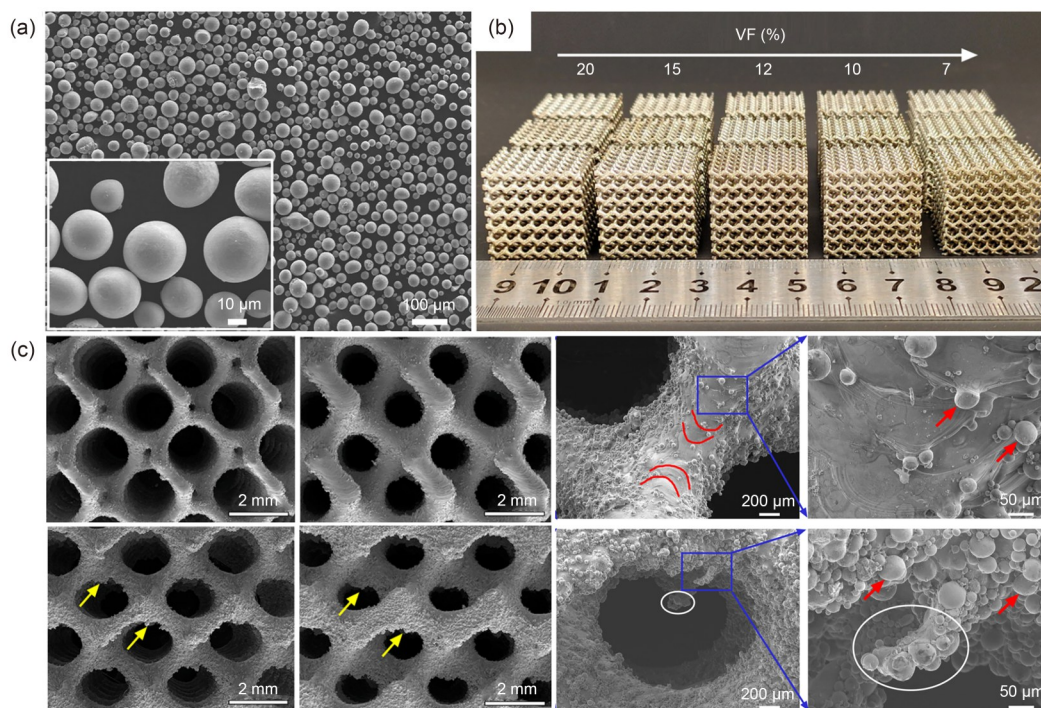


Fig. 9 Fabrication of Ni–Ti TPMS structures for bone implants (reproduced from [132], Copyright 2022, with permission from Elsevier): (a) SEM images of the Ni–Ti powder; (b) additively fabricated Ni–Ti gyroid TPMS lattice structures; (c) SEM images of the Ni–Ti TPMS lattice structures. VF: volume fraction; SEM: scanning electron microscope

these pore strategies on the microstructure, mechanical properties, and permeability of scaffolds. They found that although the pore size had little effect on the mechanical properties, increasing the pore size significantly improved the permeability because of decreased specific surface areas. Sun et al. [137] designed three types of porous Ni–Ti structures based on TPMS and demonstrated that AM is an efficient method for producing highly accurate porous Ni–Ti TPMS structures. They found that porous Ni–Ti TPMS structures offer reversible compressibility, rapid elastic recovery, and controllable shape memory recovery, making them highly efficient energy-absorbing structures. Husain et al. [138–140] addressed the challenges of machining Ni–Ti alloys using conventional methods because of their high ductility and strength, highlighting the advantages of AM in overcoming these limitations. They comprehensively analyzed the geometric properties and process parameters of the microstructural properties and solid-phase distribution within the samples. Their findings revealed significant impacts of the process parameters and structural topology on the microstructural features, including Ni evaporation and the formation of oxide- and Ti-rich phases. These studies underscore the potential of intricate TPMS geometries in Ni–Ti alloys, suggesting their potential for innovative applications and advancements across various fields.

Several attempts have been made to fabricate more complex structures and higher-performance porous scaffolds for bone implants. For example, Zhang et al. [141] explored additively manufactured Ni–Ti lattice structures, highlighting their controllable bio/mechanical properties, large deformation capacity, and damping characteristics akin to natural bone, making them highly suitable for bone implantation applications. Tang et al. [142] highlighted the unique combination of the porous metal characteristics and shape memory properties. They emphasized the significant impact of cyclic loading on the phase transformation and plastic deformation in these materials compared to bulk Ni–Ti alloys. Jin et al. [143] explored Ni–Ti alloys based on TPMS lattice metamaterials, focusing on varying interlacing-cell numbers within gyroid lattice structures. Their findings provide insights into optimizing interlacing configurations to balance manufacturability with mechanical and hyperelastic performance. Zhang et al. [144] designed several TPMS-based gradient porous structures to demonstrate the integration of metallurgical and architectural design principles as a novel approach to tailoring the mechanical properties of gradient porous metals for advanced applications.

3.1.5 Tantalum alloys

Tantalum metal has emerged as a promising biomaterial, exhibiting superior biocompatibility and inherent antibacterial properties [145]. The surface tantalum pentoxide oxide

layer confers exceptional biological inertness, whereas the terminal hydroxyl groups facilitate hydroxyapatite (HA) deposition, thereby promoting osseointegration at the bone–tantalum interface [76, 146]. The elastic modulus of porous tantalum aligns closely with that of human trabecular and cortical bone, mitigating the stress shielding effects and enhancing bone remodeling [147]. The high friction coefficient of the implants compared with those of cancellous and cortical bone bolsters the interfacial bonding with the host bone, thereby augmenting the initial implant stability [5]. Due to the high melting point and high affinity for oxygen of tantalum, traditional processing methods are difficult to process with low production efficiency and material utilization, which increases the preparation cost of tantalum implant devices. Porous tantalum (Figs. 10a and 10c) is commonly processed by vapor deposition or powder metallurgy processes [148, 149]. Clinically, porous tantalum has been widely used in joint arthroplasty, bone defect repair, and spinal fusion procedures [76, 150]. In hip and knee arthroplasties, porous tantalum-constructed integrated acetabular cups and reinforcement pads have exhibited commendable stability both initially and over the long term [150, 151].

Building on these attributes, Balla et al. [5] employed laser-engineered net shaping to fabricate porous tantalum structures with variable porosity for the first time. The mechanical properties of these structures, including a tailored Young's modulus ranging from 1.5 to 20 GPa, can be adjusted by modifying the pore volume fraction. In vitro biocompatibility tests revealed superior cellular adherence, growth, and differentiation in the porous tantalum structures compared with porous Ti control structures, indicating the potential for enhanced and early biological fixation. The improved in vitro cell–material interactions on porous tantalum are attributed to its chemistry, high wettability, and greater surface energy compared to porous titanium.

Expanding their manufacturing capabilities, Soro et al. [147] successfully produced biomimetic Ti–tantalum bone scaffolds using the LPBF process. These scaffolds, designed with TPMS architectures, maintained their morphological characteristics postmanufacturing and exhibited compressive mechanical properties suitable for use as bone implant substitutes. In vitro cell cultures confirmed the high biocompatibility of these novel biomaterials, with the interconnected open-pore designs showing improved biological responses.

To further enhance the functionality of these implants, Song et al. [76] introduced a radial gradient design for the fabrication of low-modulus gyroid porous tantalum structures using LPBF AM (Fig. 10b). This design enhances the mechanical properties and permeability of structures, thereby promoting optimal biological performance. The radial gradient design increased the elastic modulus and yield strength due to edge strengthening, whereas the permeability increased with porosity, which is consistent with the

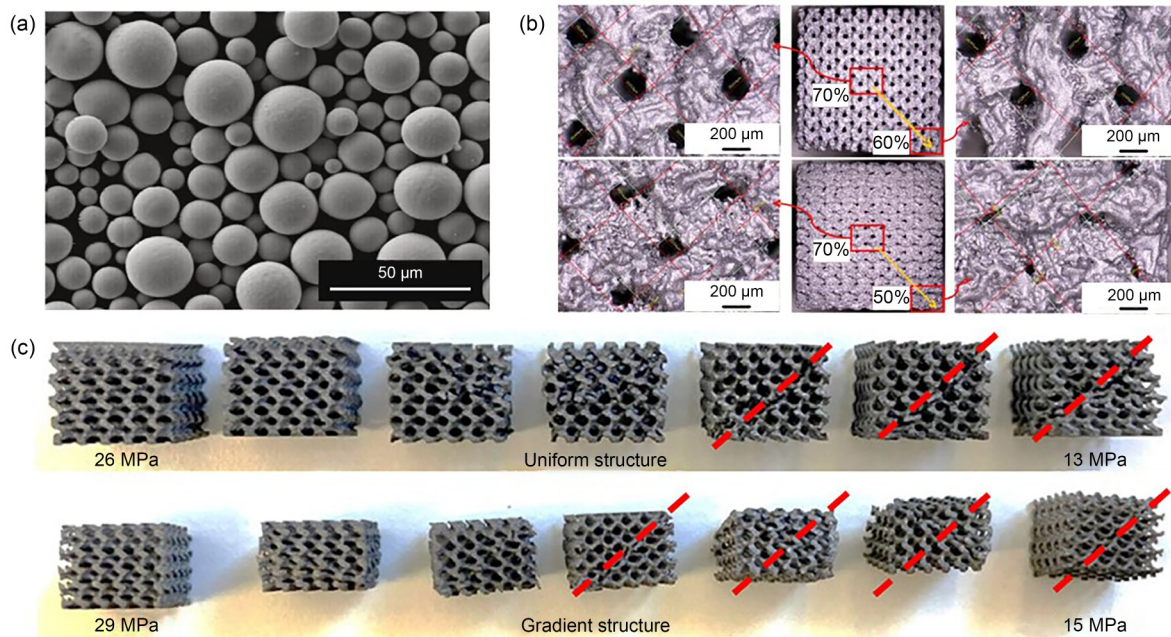


Fig. 10 Fabrication of tantalum TPMS structures for bone implants. (a) SEM image of the tantalum powder (reproduced from [151], Copyright 2014, with permission from Acta Materialia Inc.). (b) Additively fabricated tantalum gyroid TPMS lattice structures (reproduced from [76], Copyright 2023, with permission from Elsevier). (c) Fatigue deformation mode for the uniform and gradient tantalum gyroid TPMS structures (reproduced from [145], Copyright 2021, with permission from Elsevier). SEM: scanning electron microscope

range of cancellous bone permeability. This feature is especially beneficial for nutrient transportation and cell migration, which are crucial for the biological performance of bone implants. The innovative work of Chen et al. [152] further enhances tantalum's role in bone implants by designing and manufacturing gyroid tantalum structures with functional gradients in density and cell size using LPBF. The density gradient structures provide improved impact resistance, whereas the cell-size gradient structures enhance nutrient and gas transport due to lower inlet pressure and increased wall shear stress, underscoring the promise of these designs for superior osseointegration and biological performance in bone implant applications.

To regulate the TPMS structure, Wei et al. [153] employed SLM technology to fabricate gyroid porous tantalum structures, which were then filled with chitosan (CHS) and nano-HA (n-HA) composite sponges prepared by freeze-drying. This innovative approach resulted in a composite scaffold that combines the mechanical strength and corrosion resistance of porous tantalum with the bioactivity and osteoinductivity of the CHS/n-HA composite. These scaffolds offer a comprehensive solution as an ideal substitute for bone defect repair.

3.2 Polymer-based bone implants

Polymer-based biomaterials have been used in the human body since the invention of synthetic polymers. Clinical

practice has adopted these materials because of their robust, inert, and biocompatible nature, which facilitates the management of injured or infected bone, thereby enhancing patient outcomes. Polymer biomaterials can be applied to various tissues, including cardiovascular, neural, musculoskeletal, and dermal tissues [39, 154]. Polymer-based TPMS implants (Fig. 11c) are commonly fabricated using FDM or SLA to achieve precise geometries and intricate structures in a cost-effective manner. These methods enable engineers to create implants with tailored porosity and surface characteristics, which are critical for promoting tissue integration and healing in biomedical applications [155, 156]. The flexibility of polymer materials allows for the fabrication of designs that mimic the natural properties of bone for providing mechanical support.

Material extrusion-based AM, commonly known as FDM, is the predominant technique for fabricating polymer-based structures [157, 158]. This method involves layer-by-layer deposition of thermoplastic polymers to construct complex geometries directly from digital models. Due to its versatility, cost-effectiveness, and ease of use, FDM has been widely used in both prototyping and the production of functional parts [159–161]. Al Hashimi et al. [162] fabricated polymer TPMS sheet lattices with 70% porosity using a pneumatic material extrusion method. The printed scaffolds demonstrated high print accuracy with minimal percentage errors of less than 15% and significant improvements in cell proliferation and attachment. Sabahi et al. [163]

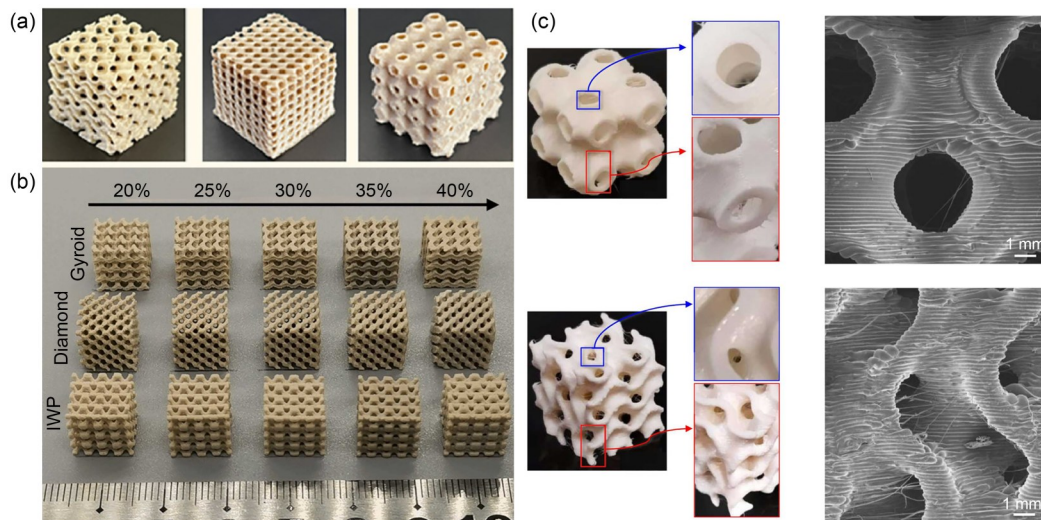


Fig. 11 Fabrication of polymer-based TPMS structures for bone implants. (a) PEEK TPMS structures fabricated by material extrusion-based AM (reproduced from [163], Copyright 2024, with permission from the authors, licensed under CC BY). (b) PEEK TPMS structures fabricated by LPBF (reproduced from [171], Copyright 2022, with permission from Elsevier). (c) SEM images of the TPU-based TPMS lattice structures (reproduced from [172], Copyright 2022, with permission from Elsevier). SEM: scanning electron microscope; TPU: thermoplastic polyurethane

used material extrusion-based AM to fabricate density-graded TPMS polyether ether ketone (PEEK) scaffolds (Fig. 11a), which achieved graded porosity, mirroring the natural bone microstructure, and demonstrated superior mechanical properties with the gradient gyroid scaffold exhibiting elastic modulus and strength of 200 and 5.15 MPa, respectively. Du et al. [164] fabricated 3D-printed PEEK/silicon nitride (PEEK/SiN) scaffolds with a TPMS structure, offering advantages like a large surface area and uniform stress distribution. The 30% porosity scaffold exhibited mechanical properties similar to those of trabecular bone, with a compressive strength of (34.56 ± 1.91) MPa and elastic modulus of (734 ± 64) MPa, demonstrating favorable damping properties. Tripathi et al. [165] fabricated some gyroid scaffolds with varying porosities using FDM with polylactic acid (PLA) filaments, showing compressive strength equivalent to human trabecular bone and expected biocompatibility in vitro. Oladapo et al. [166, 167] developed a PEEK and calcium HA (cHAp) composite with TPMS structures to optimize dental implants. The optimized structures were fabricated using FDM and resulted in increased stiffness and improved fundamental frequency, demonstrating the potential of PEEK composites as lightweight and biocompatible alternatives to metal implants in dental applications. Alkebsi et al. [168] used TPMS and FDM to design and fabricate lightweight orthopedic implants, which were consistent with cancellous bone properties in elastic modulus and porosity ratio. Guo et al. [169] used FDM to develop TPMS structural PLA/graphene oxide (GO) scaffolds, which exhibited improved mechanical properties, with the addition of 0.1% GO increasing the tensile and compression moduli by 35.6% and 35.8%, respectively. The cells showed

better adhesion, proliferation, and osteogenic differentiation in bone marrow stromal cells. Agarwal et al. [170] used TPMS to design biomimetic scaffolds with varying unit cell sizes, which were fabricated using FDM with PLA. These findings suggest that polymer-based TPMS scaffolds fabricated using material extrusion-based AM can be tailored to optimize mechanical strength for bone tissue engineering applications.

In addition to material extrusion-based AM, other AM methods, such as SLA or LPBF, have been used to fabricate polymer-based TPMS structures intended for bone implant applications. Lumba et al. [173] investigated the permeability of a biological implant structure, focusing on a gyroid lattice design that mimics the trabecular bone architecture. The designed TPMS structures were fabricated using DLP to experimentally assess the fluid flow permeability. The experimental results were compared with the numerical predictions to understand the permeability properties, highlighting the discrepancies and suggesting avenues for implant design and fabrication improvement. Abueidda et al. [156] used LPBF to create different polymeric TPMS cellular structures and compared their performances. The results showed that the Neovius and IWP exhibited higher stiffness and strength than primitive, with the mechanical properties affected by the specimen size. Wang et al. [171] designed porous PEEK scaffolds with a highly tunable elastic modulus using TPMS structures (Fig. 11b), which were then fabricated via LPBF. The fabricated gyroid scaffolds exhibited the lowest manufacturing deviation and optimal mechanical properties, with elastic moduli ranging from 42.17 to 512.12 MPa, comparable to human trabecular bones. Gabrieli et al. [174] designed several porous scaffolds with

TPMS geometries, which were then 3D-printed using a stereolithographic technique with dental resin. These scaffolds exhibited mechanical properties and pore interconnectivity comparable to those of cancellous bone.

3.3 Ceramic-based bone implants

Ceramics, comprising inorganic and nonmetallic solids like oxides, nitrides, carbides, and borides, transform into bone-like structures when exposed to high temperatures because of the formation of ionic and covalent bonds [175]. These materials have been widely used in bone scaffolds because of their high tensile strength and ability to form stable bonds with host tissues. Traditional methods for fabricating ceramic scaffolds struggle to produce intricate geometries and interconnecting porous structures due to the rigidity and fragility of ceramics. In contrast, AM offers a promising solution for fabricating complex geometries and shapes that are difficult to achieve with conventional techniques, allowing for the creation of biocompatible, chemically resistant, high-strength, and thermally conductive ceramic scaffolds [176]. Various AM strategies, including material extrusion-based AM, SLA, and DLP, are widely used to fabricate bone scaffolds for tissue engineering and clinical research applications [177]. This review discusses these AM techniques for fabricating ceramic-based TPMS structures for bone implants from a process perspective.

Similar to the preparation of polymer-based TPMS structures, material extrusion-based AM has been widely used to fabricate complex ceramic structures [176]. The main advantage of this method lies in its ability to extrude materials that can be melted or processed into a flowable state and subsequently shaped into the desired structure [178]. It is worth noting that the performance (including quality and mechanical properties) of the structures fabricated using this stepwise extrusion and accumulation process is significantly influenced by various planning parameters, such as path spacing and layer thickness. Moreover, very fine structures like TPMS, which consist of curved surfaces, present additional challenges during fabrication. Consequently, while there is substantial research on using material extrusion-based AM to fabricate ceramic porous scaffolds [179], studies focusing on the preparation of TPMS structures using this method are still relatively limited.

Baumer et al. [180] presented an open-source software algorithm for creating 3D-printable Fischer–Koch S (FKS) and a gyroid scaffold, demonstrating the successful fabrication of HA FKS scaffolds (Fig. 12a) using a low-cost AM method. The results showed promising dimensional accuracy, internal microstructure, and porosity characteristics for TPMS-based ceramic scaffolds for bone regeneration. Restrepo et al. [181] used an FDM printer to create ceramic structures with gyroid, Schwarz primitive, and Schwarz

diamond surfaces (Fig. 12b), which were suitable for bone tissue scaffolds. They compared their mechanical properties to determine the optimal TPMS for constructing ceramic scaffolds for bone repair. All geometries exhibited porosities within the range of the trabecular bone. Among the geometries, the Schwarz primitive exhibited the best mechanical behavior, which was attributed to the orientation of the columns supporting the load. Charbonnier et al. [182] produced custom-made gyroid structure implants (Fig. 12c) with and without cortical-like reinforcement using sintered HA and material extrusion-based AM and characterized their morphological, physicochemical, and mechanical features. The results showed that the implants had improved stiffness and fracture resistance, concentrating new bone formation in the implant core without affecting bone quantity or maturity.

In the vat polymerization process, such as SLA and DLP, a photocurable liquid polymer is selectively solidified by a low-power ultraviolet light source at the surface of a vat. The build progresses as the *z*-axis descends, with each layer of the liquid polymer spreading over the previously solidified surface until the entire object is formed. In recent years, these AM methods have been extensively used to fabricate ceramic bone implants, offering several advantages. These technologies enable the creation of intricate and highly customized structures that are difficult to achieve using traditional manufacturing techniques. These methods also allow for precise control over porosity, which is crucial for promoting bone ingrowth and integration. Moreover, the ability to fabricate complex geometries enhances the functionality and performance of implants, thereby ensuring better patient outcomes.

Kong et al. [183] developed a method for fabricating high-strength and high-toughness TPMS-based ceramic structures by optimizing the SLA process and exploring graded configurations. The results showed significant improvements in toughness and energy absorption compared to pure ceramics. Zhang et al. [184] fabricated gyroid β -tricalcium phosphate (β -TCP) bioceramic scaffolds using SLA to mimic cancellous bone architecture. These scaffolds exhibited adjustable porosity, pore size, wall thickness, and compressive strength and can be tailored to suit various bone sites. The fabricated ceramic gyroid structures enhanced cell proliferation and showed promise for efficient repair of bone defects. Li et al. [36] focused on enhancing bone defect repair using bioactive glass- β -tricalcium phosphate (BG-TCP) scaffolds with TPMS structures fabricated via SLA. The incorporation of BG improved the compressive strength of the β -TCP matrix, facilitating adaptable biodegradability, and promoting the osteogenic differentiation of bone marrow mesenchymal stem cells (BMSCs) and angiogenic ability of endothelial progenitor cells. Based on the above studies, the optimization of the SLA processes

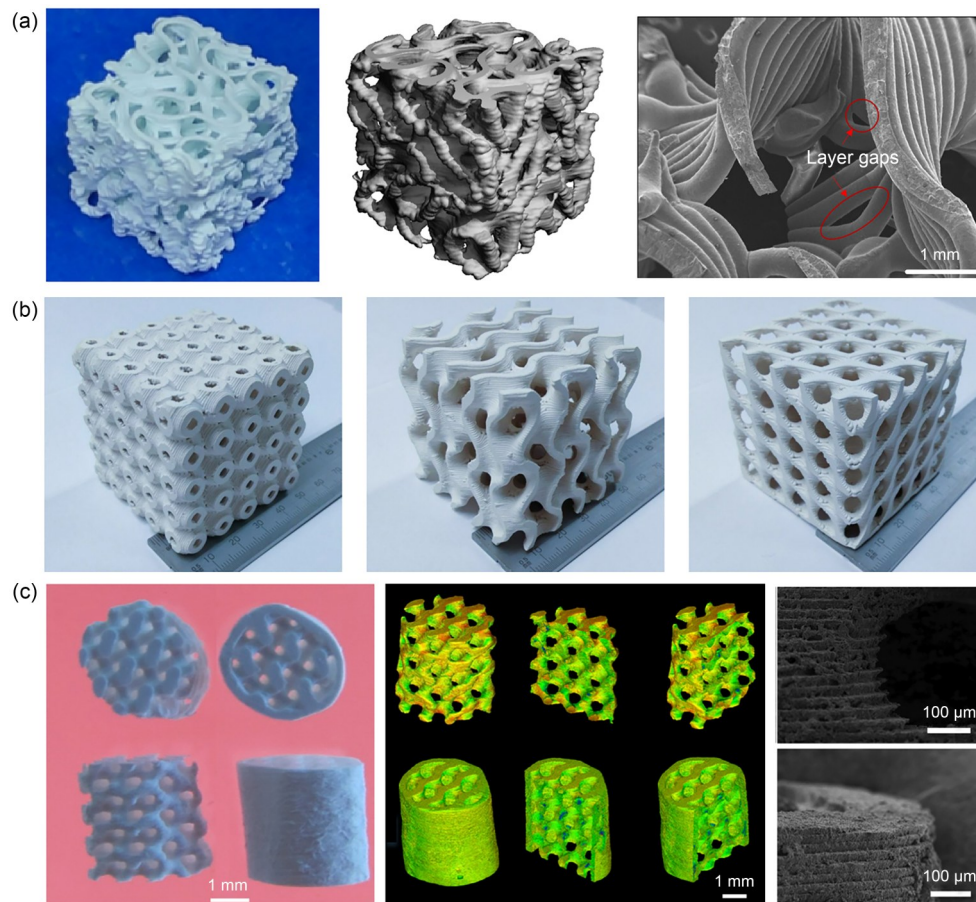


Fig. 12 Fabrication of ceramic-based TPMS structures using material extrusion-based AM. (a) HAp FKS scaffold and its microstructure characterization (reproduced from [180], Copyright 2023, with permission from the authors, licensed under CC BY). (b) Ceramic scaffolds with different TPMS geometries (reproduced from [181], Copyright 2017, with permission from the authors, licensed under CC BY). (c) Gyroid-based macro-porous bioceramic implants (reproduced from [182], Copyright 2020, with permission from Acta Materialia Inc.)

and incorporation of bioactive glass significantly enhanced the mechanical properties and biological performance of the TPMS-based ceramic scaffolds for bone implants.

HA is ideal for bone implants because of its biocompatibility and chemical similarity to natural bone minerals. This enables the fabrication of customized implants (Fig. 13d) with tailored mechanical properties and complex geometries, enhancing osseointegration and long-term implant stability [185]. Bouakaz et al. [186] explored the fabrication and evaluation of HA scaffolds with a gyroid-TPMS porous structure using DLP (Fig. 13c). The scaffolds designed to mimic trabecular bone exhibited high porosity (65%) and excellent HA densification (90.5%). Mechanical testing revealed suitable properties for guided bone regeneration at nonload-bearing sites, such as in maxillofacial contour reconstruction. This pilot study underscores the potential of TPMS-based scaffolds for clinical bone regeneration applications. Maevskaia et al. [187] used TPMS microarchitectures, including diamond, gyroid, and primitive designs, for 3D printing using HA for bone tissue engineering. Mechanical

testing revealed superior strength of the diamond and gyroid structures compared to the primitive. In calvarial defect and bone augmentation models, gyroid demonstrated significantly enhanced osteoconduction and bone ingrowth compared with primitive implants, highlighting its potential as a favorable TPMS-based scaffold for treating bone deficiencies in clinical applications. Liang et al. [188] used DLP to fabricate HA scaffolds with different porous structures, which were then investigated in terms of compressive properties and cell metabolism to analyze their potential in bone tissue engineering applications. Yao et al. [189] investigated the potential of DLP-printed HA ceramics with TPMS geometries, enhanced by wet CO₂ sintering, as promising materials for bone engineering applications. Deng et al. [37] proposed functional gradient lattice structures based on TPMS designs and fabricated them using DLP with a consistent porosity of 65% (Fig. 13b). Four gradient scaffolds were investigated, and the results revealed that the gradient structures significantly enhanced the compressive strength compared to the uniform structures. Hua et al. [190]

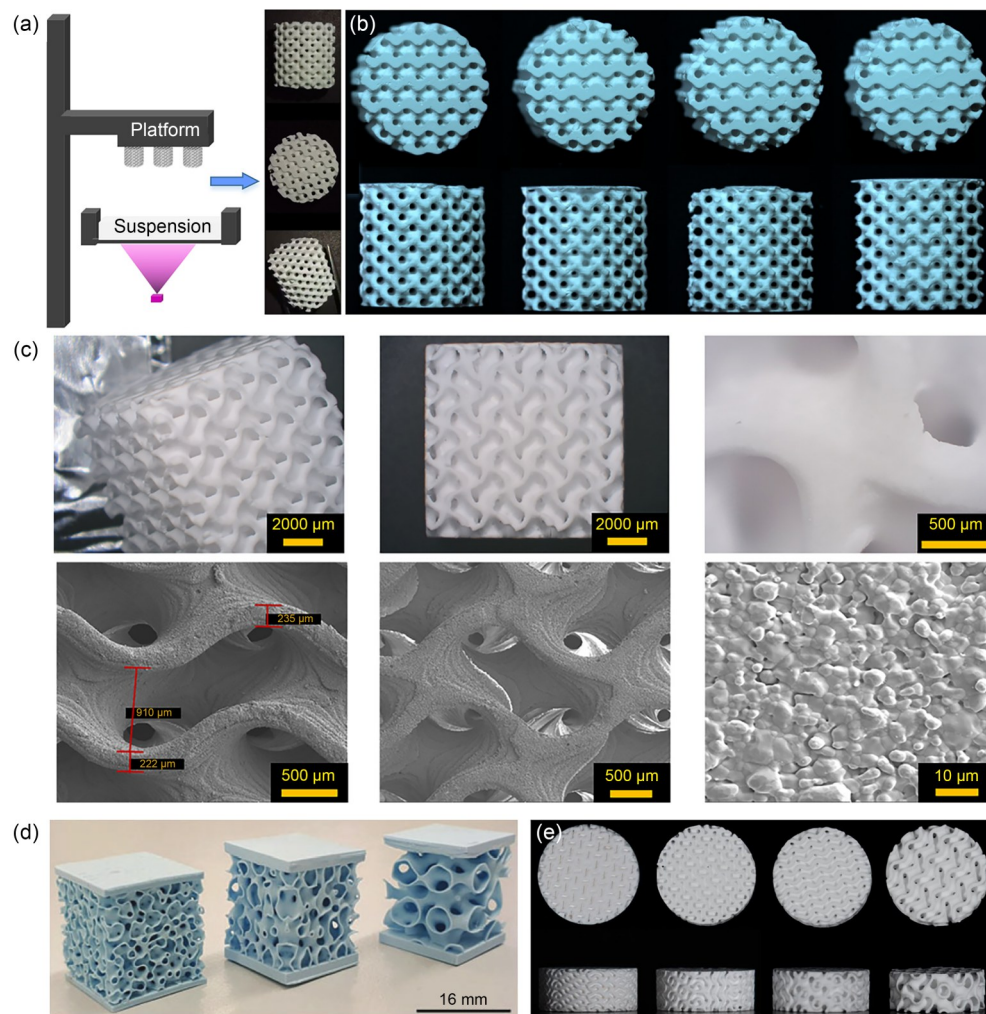


Fig. 13 Fabrication of ceramic-based TPMS structures using DLP. (a) Flow diagram of gyroid structural bioceramic green bodies fabricated using DLP (reproduced from [190], Copyright 2021, with permission from Elsevier). (b) Macrostructure of printed TPMS scaffolds with different gradient structures (reproduced from [37], Copyright 2023, with permission from Elsevier). (c) Gyroid design obtained for the ceramic scaffolds and SEM micrographs of structural details (reproduced from [186], Copyright 2023, with permission from the authors, licensed under CC BY-NC-ND). (d) Fabricated TPMS derivative ceramic structures (reproduced from [185], Copyright 2023, with permission from the authors, licensed under CC BY). (e) Digital photos of TPMS bone scaffold with various porosities (reproduced from [191], Copyright 2024, with permission from the authors, licensed under CC BY-NC). SEM: scanning electron microscope

fabricated HA ceramics with TPMS structures using DLP (Fig. 13a), enhanced by doping akermanite to better tailor the porosity, bioactivity, and mechanical strength.

In addition to HA, other bioceramics are used for DLP of TPMS-based bone implants and extensive research has been conducted to investigate their applications. For example, Lu et al. [192] fabricated ZnO ceramics with gyroid and Schwartz P TPMS structures using DLP. The gyroid-structured ZnO ceramic exhibited a compressive strength of approximately 6.87 MPa with 55% porosity, outperforming the Schwartz P structure, which showed 4.02 MPa. Jiao et al. [193] fabricated bone scaffolds with variable irregularity and porosity using ceramic DLP with 20% (mass fraction) HA-doped zirconia. The scaffolds mimicking the cancellous bone structure demonstrated enhanced mechanical

and biocompatibility properties. Shao et al. [194] investigated $ZrO_2/CSi-Mg_x$ scaffolds fabricated via DLP by combining Mg-doped calcium silicate (CSi-Mg) with ZrO_2 to enhance their biocompatibility and mechanical properties. The incorporation of CSi-Mg significantly strengthened the scaffolds after sintering, with the $ZrO_2/CSi-Mg_{10}$ scaffolds featuring TPMS showing compression strengths exceeding 92 MPa, and a strength of 63 MPa even after prolonged immersion. Shen et al. [195] focused on tailoring the pore architectures of Mg-doped scaffolds using DLP to achieve fully interconnected networks and TPMSs resembling cancellous bone. The sheet-TPMS geometries exhibited higher initial compressive strength and higher Mg-ion release rates than other TPMS structures in vitro. Zhu et al. [191] fabricated four TPMS configurations (Fig. 13e) with β -TCP bioceramic

via DLP and studied the substantial potential of TPMS scaffolds for promoting bone regeneration within mandibular defects. Duque-Urbe et al. [196] fabricated alumina (Al_2O_3) scaffolds using ceramic DLP and a suspension of Al_2O_3 particles in a photopolymerizable resin. Scaffolds with gyroid and Schwartz P geometries were successfully printed and characterized morphologically and mechanically pre- and postsintering. Li et al. [197] fabricated Mg/Sr co-doped wollastonite bioceramic (MS–CSi) scaffolds with gyroid, cylindrical, and cubic pore geometries fabricated using DLP and investigated their impact on osteogenesis and angiogenesis through in vitro and in vivo experiments. Vijayavenkataraman et al. [198] explored porous bone implant designs based on TPMS and fabricated them using Al_2O_3 via DLP. This research demonstrated the feasibility of 3D printing TPMS-based structures in ceramics, highlighting the potential to match the compressive modulus of native bone and mitigate stress shielding effects in bone implant applications.

4 Biological performance of TPMS-based bone implants

The biological performance evaluation of TPMS-based bone implants encompasses several critical aspects. First, their mechanical properties are rigorously assessed through experimental testing and simulation to ensure that they match the structural integrity required for load-bearing applications. Second, permeability studies combining experimental measurements and computational simulations are conducted to investigate how the intricate TPMS structures facilitate nutrient diffusion and waste removal essential for tissue viability. Third, biocompatibility is evaluated through comprehensive in vitro and in vivo experiments to investigate how well these implants interact with biological systems, focusing on aspects like cell adhesion, proliferation, and inflammatory responses. These investigations validate TPMS-based bone implants as robust, biocompatible solutions for enhancing bone regeneration and integration in clinical settings.

4.1 Mechanical properties

The mechanical performance of TPMS-based implants is crucially evaluated using parameters like compressive strength, modulus of elasticity, and fatigue resistance (Fig. 14b) [199, 200]. Compressive strength is a key mechanical property of TPMS-based implants, reflecting their ability to withstand compressive forces in weight-bearing bones [36, 125]. Experimental studies involve subjecting these implants to compression tests to determine the maximum load they can bear before failure. The intricate porous

architecture of TPMS provides structural support while maintaining sufficient porosity for biological integration, resulting in compressive strengths comparable to those of cancellous bone. The modulus of elasticity, also known as Young's modulus, measures the stiffness of TPMS-based implants [93, 115]. This property is critical as it determines how much an implant deforms under applied stress. TPMS structures, with their open-cell design and variable pore sizes, can be tailored to achieve moduli that closely match those of natural bone, thereby minimizing stress shielding effects and promoting load transfer between the implant and surrounding bone tissue. In addition to efficiently adjusting the porosity to tailor the mechanical properties of TPMS structures, various gradient structures have been used to create porous bone implants that more closely match the characteristics of natural bone [38, 40, 200, 201]. These gradient designs allow for a more seamless integration with the native bone, thereby enhancing the functionality and effectiveness of the implant. By mimicking the natural gradation found in bone tissue, these TPMS-based implants can offer improved mechanical compatibility and biological performance, ultimately leading to better outcomes in bone regeneration and repair.

Furthermore, fatigue resistance was evaluated to examine the long-term durability of TPMS-based implants under cyclic loading conditions [106, 118, 133]. Fatigue tests simulate the repetitive stresses that implants may experience during daily activities to ensure that they can withstand mechanical wear over extended periods without structural failure. The interconnected network of pores within TPMS structures enhances their fatigue resistance by evenly distributing stress throughout the implant, thereby reducing the likelihood of crack propagation and failure. Speirs et al. [133] investigated the compression fatigue behavior of several TPMS scaffolds and found that TPMS offers superior static mechanical properties and fatigue resistance compared to conventional structures. Yang et al. [118] examined the compression–compression fatigue behavior of the gyroid cellular structures and found that cyclic ratcheting and fatigue damage contribute to failure, typically resulting in nearly 45° fracture bands. The fatigue ratio was increased after sandblasting, which enhanced the fatigue resistance by removing adhered powder particles, inducing compressive residual stress, and creating a nanocrystalline zone, thus outperforming many other lattice structures. Tilton et al. [106] revealed new insights into the fatigue performance of Ti-6Al-4V scaffolds fabricated using TPMS. They found that the Schoen-IWP scaffolds exhibited a significantly higher fatigue life than the primitive scaffolds at similar porosity and applied stress amplitude, although the primitive scaffolds better mimicked the compressive mechanical properties of the trabecular bone. These findings are crucial for the spatial microarchitectural design of load-bearing orthopedic implants.

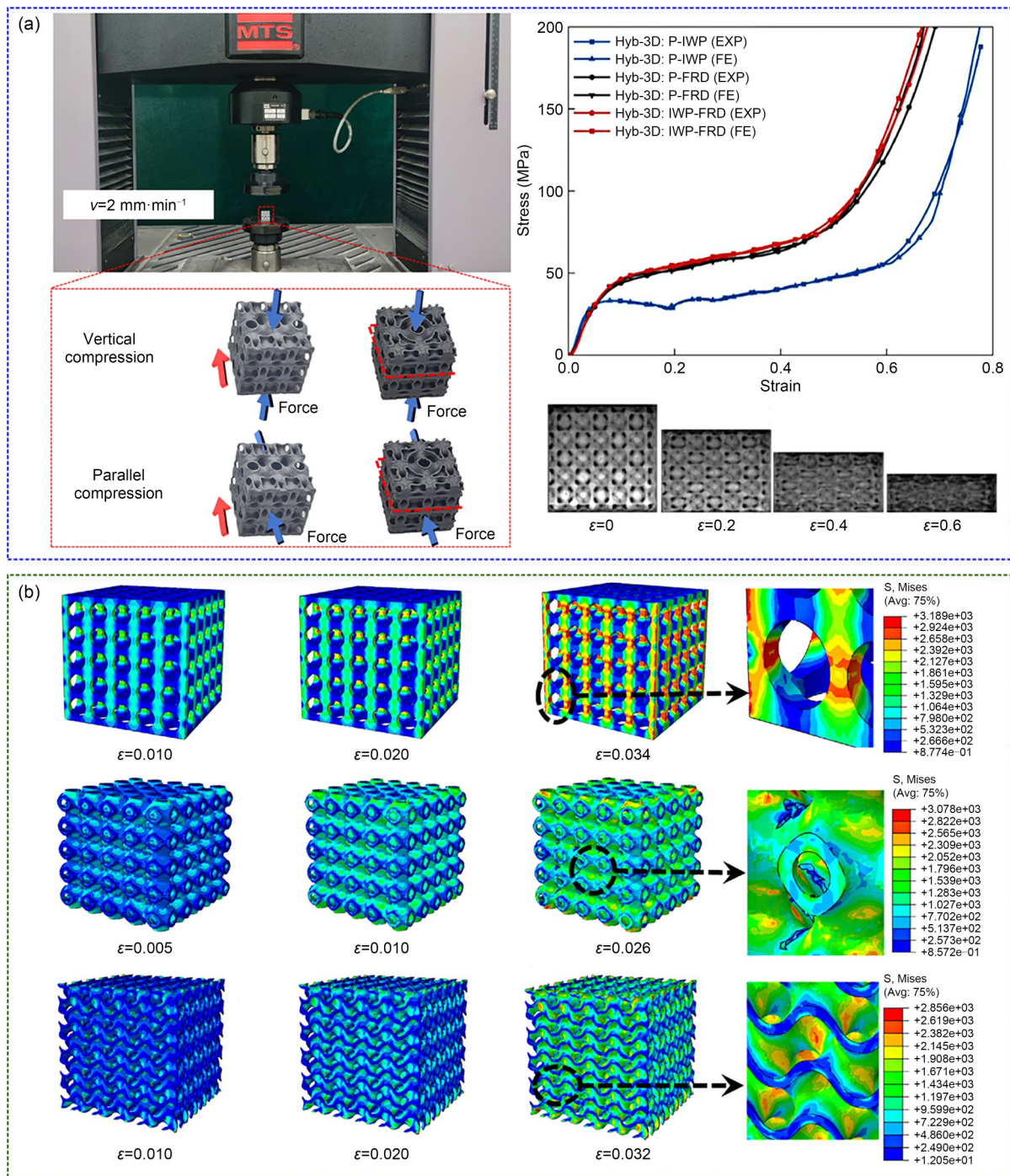


Fig. 14 Investigation of the mechanical properties of TPMS-based scaffolds. (a) Experimental method (reproduced from [93], Copyright 2024, with permission from Elsevier). (b) Numerical method (reproduced from [199], Copyright 2023, with permission from Elsevier)

Therefore, the mechanical properties of TPMS-based bone implants are carefully engineered to replicate and enhance the biomechanical functions of natural bone. Moreover, TPMS-based implants offer promising solutions for improving the longevity and performance of orthopedic implants in clinical practice by optimizing compressive strength, modulus of elasticity, and fatigue resistance

through advanced fabrication techniques and material selection.

4.2 Permeability

Permeability is another critical characteristic of TPMS-based bone implants that influences their ability to facilitate

nutrient transportation, waste removal, and cell migration within the porous structure of the implant [202]. TPMS structures, inspired by natural bone's trabecular architecture, are designed to optimize permeability while maintaining mechanical integrity. The intricate network of interconnected pores in TPMS implants allows for efficient fluid flow and gas exchange, which are crucial for cellular activities, such as proliferation, differentiation, and tissue regeneration [49, 50].

Numerous experimental studies combined with computational simulations have been conducted to comprehensively examine the permeability of TPMS-based implants. Permeability experiments involve measuring the flow of fluids through the implant under controlled conditions and providing quantitative data on how well fluids can penetrate and permeate through the scaffold's porous network. The constant head permeability test setup is commonly used to experimentally measure the permeability of scaffolds, with the samples tightly fixed using two clamps between two reservoirs [43]. Computational fluid dynamics (CFD) simulations complement these experiments by predicting fluid flow patterns and pressure gradients within the TPMS structure, providing insights into the transport properties of implants under varying physiological conditions [10, 63, 203–207] (Fig. 15).

The permeability of TPMS-based implants is influenced by several factors, including the pore size, shape, interconnectivity, and overall porosity [208]. Larger pores and interconnected channels enhance permeability by reducing the flow resistance, thereby allowing for better nutrient diffusion and waste removal. However, the permeability must also be optimized while maintaining sufficient mechanical strength and structural integrity to support the surrounding tissue and withstand physiological loads. Therefore, the permeability of TPMS-based bone implants plays a crucial role in their biological performance by facilitating fluid exchange and nutrient transport, which are crucial for cellular activities and tissue regeneration [116, 204]. Recent advances in experimental techniques and computational modeling have continuously refined our understanding of how TPMS structures can be tailored to maximize permeability while satisfying the mechanical and biological requirements for successful orthopedic applications.

4.3 Biocompatibility

Biocompatibility is a very important criterion for the successful application of TPMS-based bone implants, which ensures that the implants interact favorably with biological systems [41, 200]. To comprehensively evaluate biocompatibility, *in vitro* and *in vivo* studies have been conducted, focusing on key aspects like cell adhesion, proliferation, and inflammatory responses [195, 209].

In vitro studies are typically the first step in assessing the biocompatibility of TPMS-based bone implants. These studies involve culturing various types of cells, such as osteoblasts or BMSCs, on the implant surfaces to observe cell adhesion, spreading, and proliferation. Successful cell adhesion indicates a surface that supports cellular attachment, which is a critical factor for subsequent tissue integration. Ma et al. [41] conducted cell–culture experiments to investigate the effects of pore size and scaffold porosity on cell growth. The fabricated TPMS scaffolds exhibited good biocompatibility, and the surface area and permeability can affect the degrees of cell adhesion and proliferation. Jin et al. [43] conducted *in vitro* studies by infiltrating the soft gelatin methacryloyl (GelMA) hydrogel matrix into the pores of the fabricated scaffolds to demonstrate its biocompatibility. The results provide insights into the design and application of porous scaffolds in bone implants. Xu et al. [200] conducted an *in vitro* biomineralization and biological testing and found that the TPMS scaffolds showed excellent calcium-phosphorus formation induction and biocompatibility (Fig. 16a).

In vivo studies provide a more comprehensive assessment of biocompatibility by implanting TPMS-based scaffolds into animal models [186, 197]. These studies examine the overall body response to implants, focusing on tissue integration, inflammatory reactions, and bone regeneration [187, 210]. Histological analyses are conducted to evaluate the extent of new bone formation, vascularization, and the integration of the implant with surrounding tissue. These analyses often include staining techniques to identify specific cell types and the deposition of a new bone matrix. Shen et al. [195] analyzed rabbit experiments *in vivo* to show that although bone regeneration is delayed in sheet-TPMS pore geometries, diamond and gyroid pore scaffolds significantly enhance early-stage osteogenesis and achieve uniform bone tissue formation by seven weeks. This finding highlights the effectiveness of diamond and gyroid architectures in accelerating bone regeneration and improving scaffold performance in bone defect repair. Khan et al. [211] conducted an *in vivo* study to evaluate the integration of gyroid-based Ti6Al-4V implants over six weeks using a rabbit tibia model (Fig. 16b). Histopathological examination revealed superior osteointegration in the gyroid structures, as evidenced by neovascularization, in-bone growth, and the presence of a Haversian system. Zhao et al. [44] conducted an *in vivo* study on Zn-based bone implants and demonstrated expedited bone ingrowth and regeneration through the sustained release of divalent metal cations. These implants significantly enhanced osteogenesis, immunoregulation, angiogenesis, and anti-infective activity, highlighting their promising potential for clinical translation in repairing load-bearing bone defects. Wang et al. [212] conducted *in vivo* tests on Zn–2Mg alloy scaffolds to demonstrate

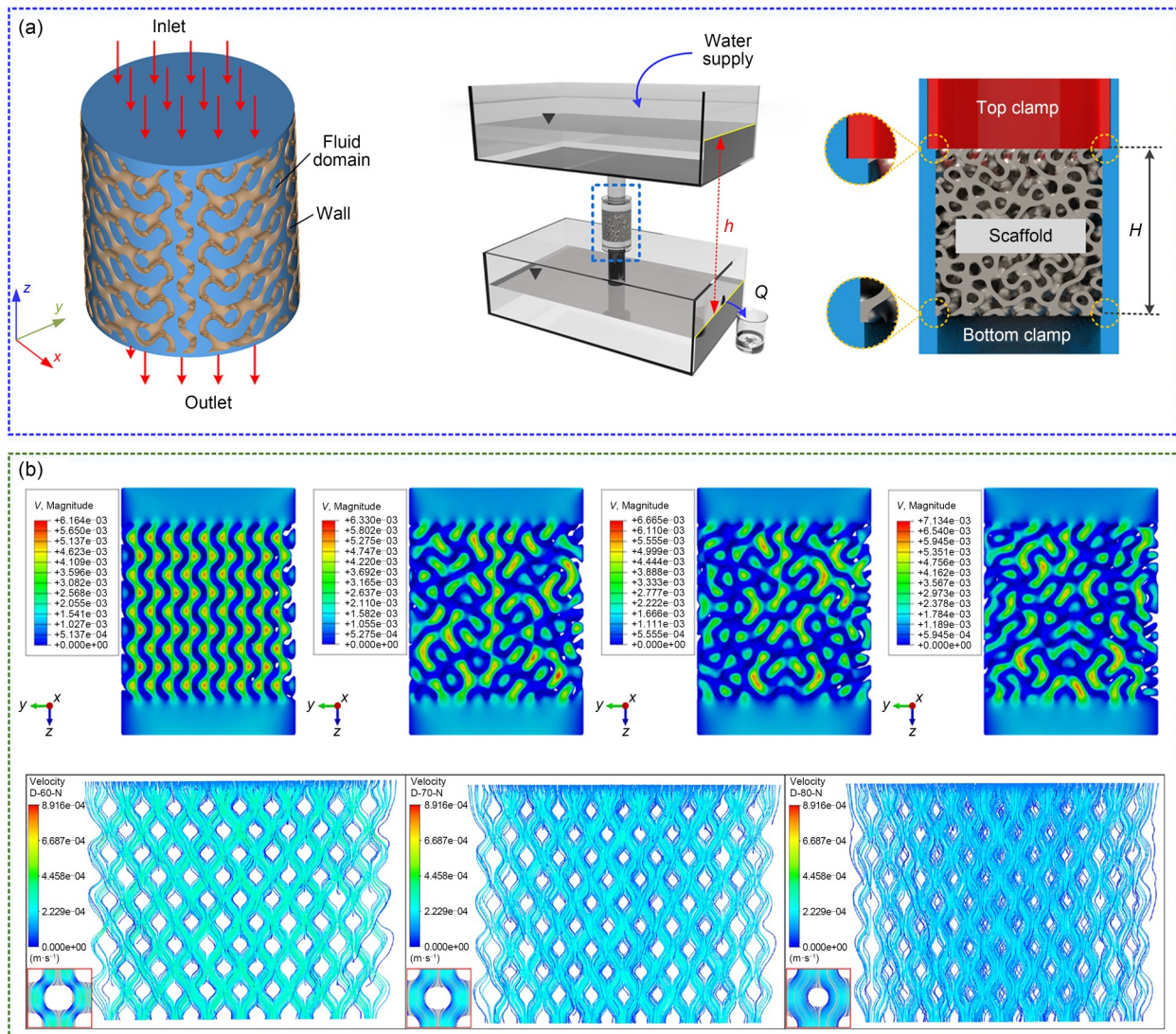


Fig. 15 Investigation of the permeability of TPMS-based scaffolds. (a) Experimental setup of the constant head method and boundary conditions for the CFD analysis (reproduced from [43], Copyright 2022, with permission from Elsevier). (b) Results from CFD analysis (reproduced from [43] (Copyright 2022, with permission from Elsevier) and [207] (Copyright 2023, with permission from IPeM))

their satisfactory biocompatibility and osteogenic ability. They found that scaffolds with lower porosities and smaller unit sizes exhibited superior osteogenesis because of their optimal pore size and larger surface area. These findings indicate that the biodegradable performance of these scaffolds can be precisely regulated through their structural design, making them highly effective for treating bone defects.

Overall, the biocompatibility of TPMS-based bone implants has been extensively evaluated via *in vitro* and *in vivo* studies. These studies focused on essential factors like cell adhesion, proliferation, and inflammatory responses to ensure that implants interact positively with biological systems. The primary objective is to develop implants that support tissue integration and regeneration to provide a reliable solution for bone repair and regeneration.

5 Conclusions and future perspectives

This review presented a comprehensive overview of the current state-of-the-art research on bone implants with TPMS architectures, focusing on their design, fabrication, and biological performance. The integration of TPMS structures into bone implants has shown significant promise because of their ability to closely mimic the intricate geometry and mechanical properties of natural bone. However, there are several key challenges that must be addressed to fully exploit the potential of TPMS-based bone implants in clinical applications.

The design of TPMS-based bone implants offers a unique advantage in terms of mechanical properties that can be fine-tuned to match those of natural bone. The TPMS

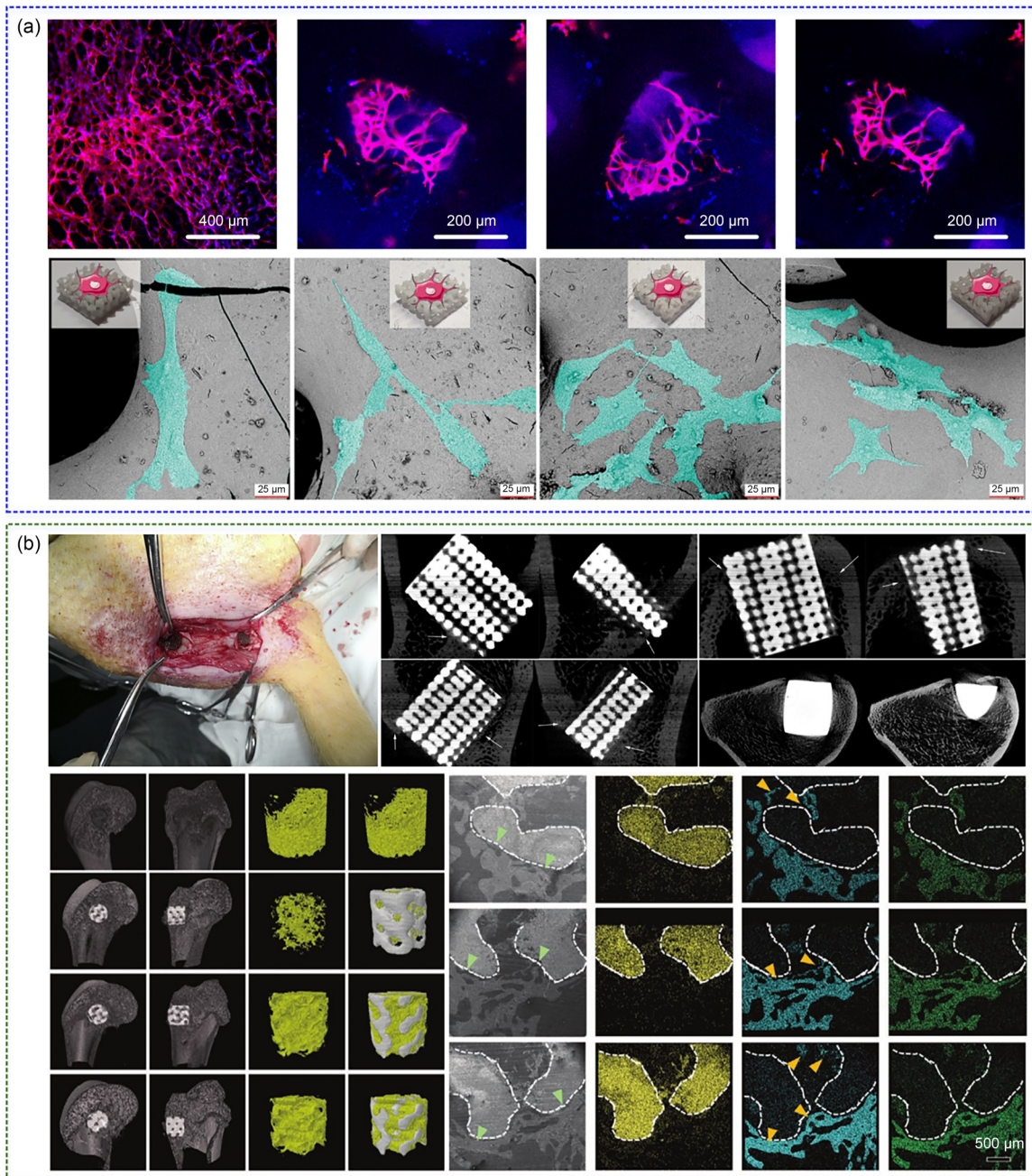


Fig. 16 Studies on the biocompatibility of TPMS-based scaffolds. (a) In vitro experiment (reproduced from [43] (Copyright 2022, with permission from Elsevier) and [200] (Copyright 2024, with permission from Elsevier)). (b) In vivo experiment (reproduced from [210] (Copyright 2019, with permission from the authors, licensed under CC BY-NC-ND) and [44] (Copyright 2023, with permission from Wiley-VCH GmbH))

structures, such as gyroid, diamond, and Schoen’s IWP, provide a balance between strength and porosity, which is essential for load-bearing applications and for facilitating bone ingrowth. However, optimizing these designs requires further exploration of the specific mechanical and biological requirements of different types of bone defects and patient-specific conditions. The existing gradient, hierarchical, and hybrid designs are often based on idealized and generalized models obtained from medical imaging,

including finite element analysis of the post-design medical mechanical properties. Due to the complex properties, loads, and boundary conditions of the corresponding materials in the human body, it is difficult to evaluate them with high accuracy in the design stage due to the limitations of computer operations and medical detection methods. In other words, we can only set one or a few goals for optimization, and it is difficult to achieve a quantitative analysis of the customized design and subsequent interface response

for existing patients. In particular, for the local matching problem of bone defects and joint replacements, it is necessary to consider the integration of biomechanics and mechanobiology with existing bone segments to solve stress shielding and implant settlement potential. Future research should focus on developing advanced computational models and simulation techniques to predict the performance of these implants more accurately under physiological conditions.

The fabrication of TPMS-based bone implants has been revolutionized by advancements in AM technologies, especially LPBF and DLP. These methods enable the precise creation of complex TPMS structures with high resolution and reproducibility. Despite these advancements, there are still challenges, such as the scalability of production, material limitations, and the integration of multiple materials to enhance the functional properties of implants. The existing AM accuracy is insufficient to support our design exploration of TPMS bone implants. There are various manufacturing defects at scales below 100 μm , and some surface modification methods are also difficult to meet the requirements of this complex structure. The differences between design and manufacturing greatly reduce the original design goals, and the ideal effects could be observed in subsequent *in vitro* and *in vivo* experiments. Future work should aim at refining these fabrication techniques to improve their efficiency, cost-effectiveness, and ability to produce multimaterial implants with integrated functionalities.

In terms of biological performance, TPMS-based implants have exhibited enhanced osteogenesis, vascularization, and integration with host bone tissue. The interconnected porous networks of the TPMS structures facilitate nutrient and waste exchange, promoting cell proliferation and differentiation. This can be achieved by adjusting the volume fraction and inner-to-outer pore volume ratio, which respectively influence the scaffold's elastic modulus and permeability. By fine-tuning these parameters, implants that provide the necessary mechanical support can be created while also ensuring effective mass transport, which is crucial for the success of the implant *in vivo*. As discussed in this review, previous studies have shown promising results in terms of bone regeneration and implant stability. However, the long-term biological effects and potential complications related to the degradation products of these implants require further investigation. Future research should include long-term *in vivo* experiments and clinical trials to comprehensively evaluate the safety and efficacy of TPMS-based implants.

In addition to the discussed aspects, future developments of TPMS-based bone implants should explore the integration of advanced functionalities, such as metamaterials. These materials can offer unique properties not found in traditional materials, such as negative Poisson's ratio or tunable acoustic properties, which could enhance the overall

performance and adaptability of bone implants. Incorporating metamaterials into TPMS designs can improve biomechanical compatibility and promote more effective load transfer during bone regeneration. Furthermore, the use of biodegradable materials is a promising area for future research. These materials can gradually transfer the load to the regenerating bone while maintaining mechanical integrity, thereby promoting natural healing processes. Advancements in material science have led to the development of biodegradable alloys and composites that balance degradation rates with mechanical strength, thereby optimizing long-term implant performance.

In conclusion, although significant progress has been made in the design, fabrication, and biological performance of TPMS-based bone implants, future research should focus on integrating metamaterials, advancing biodegradable materials, and leveraging personalized medicine approaches. These strategies can revolutionize the field of orthopedic implantology by providing safer, more effective, and personalized solutions for bone defect repair and regeneration.

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Author contributions JHL: conceptualization, investigation, data analysis, writing—original draft, and writing—review & editing. HTF: investigation, data analysis, writing—original draft, and resources. LCH: investigation, data analysis, supervision, and resources. JKD: methodology, supervision, resources, and project administration. YH: conceptualization, methodology, supervision, resources, and project administration. YAJ: conceptualization, methodology, supervision, writing—original draft, project administration, and funding acquisition.

Declarations

Conflict of interest YH is an associate editor for *Bio-Design and Manufacturing* and was not involved in the editorial review or the decision to publish this article. The authors declare that they have no conflict of interest.

Ethical approval This study does not contain any studies with human or animal subjects performed by any of the authors.

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