



Immobilization of heavy metals in sludge using phosphoric acid and monobasic calcium phosphate*

Ping TANG¹, Yong-chao ZHOU^{†‡2}, Zhen-miao XIE¹

(¹College of Environment and Material Engineering, Hangzhou Dianzi University, Hangzhou 310027, China)

(²College of Civil Engineering and Architecture, Zhejiang University, Hangzhou 310027, China)

[†]E-mail: zhoutang@zju.edu.cn

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Abstract: The purpose of this research is to investigate the potential of pre-treatment with phosphoric acid (PA) and monobasic calcium phosphate (MCP) for the stabilization of heavy metals in sludge and its bottom ash. The tannery sludge samples were collected in Wenzhou, China and heavily contaminated with heavy metals, such as Pb, Cr and so on. The samples were pre-treated with PA or MCP. Then XRD and TCLP tests were adopted as the evaluating methods to characterize the Pb, Cr, Cu, Zn and Cd immobilization in the pre-treated sludge and its bottom ash. The results showed that this treatment effectively immobilized Pb and Cd in the sludge, lightly stabilized the metal Cu, and adversely, enhanced the leachability of Zn. After incineration at 900 °C, Pb and Cr in the bottom ash of pre-treated sludge were significantly stabilized due to the formation of their highly thermostable phosphates and pyromorphite-like minerals during the incineration process. However, an increase of Cu and Zn solubility was observed which might be attributable to the acidification of sludge due to the addition of PA or MCP.

Key words: Tannery sludge, Bottom ash, Heavy metals, Phosphate, Stabilization

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1 Introduction

Treatment of municipal wastewater inevitably leads to the generation of large volumes of sewage sludge. Large quantities of metal elements such as Cu, Cr, Pb and Zn, are discharged into sewer system from industrial wastewater; these sources cause sewage sludge to contain heavy metal precipitates (Karvelas *et al.*, 2003). Major disposal and recycling routes for sewage sludge are landfilling, agriculture uses and (co-)incineration. Among these routes, incineration has become the major disposal route due to its large volume reduction, thermal destruction of toxic organic constituents and pathogens, and recovery of

energy (Van de Velden *et al.*, 2008). However, the major problem associated with the thermal treatment of sludge is the possible release of heavy metals to the environment, such as metal volatilization during the process of incineration at high temperature, and metal dissolution through the disposal or recycling of bottom ash and other residuals.

Generally, it has been recognized that the apatite group minerals in nature (which can be expressed by the formula $A_5(PO_4)_3(F, Cl, OH)$, where A=Pb, Zn, Cd, Cu, etc.) are the most thermodynamically stable phosphate species and are relatively insoluble (Piantone *et al.*, 2003). Accordingly, various phosphorus-containing amendments, such as phosphate rock (Tang *et al.*, 2004; Brown *et al.*, 2005; Cao *et al.*, 2009), phosphoric acid (Cao *et al.*, 2009), hydroxyapatites (Mavropoulos *et al.*, 2002; Raicevic *et al.*, 2009; Mignardi *et al.*, 2012), apatites (Qian *et al.*, 2009; Padmi *et al.*, 2009), and phosphate-based salts

[‡] Corresponding author

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(Eighmy *et al.*, 1997), have been studied for their roles in the immobilization of heavy metals in soil and incineration residual. For the heavy metal-bearing sludge, phosphorus-containing amendment pre-treatment has also been increasingly applied to form apatite structure minerals. Moreover, the process plays an important role in the volatilization abatement of heavy metal during the process of incineration. The high efficiency of vaporization abatement of heavy metals during incineration was pointed out by various studies (Rio *et al.*, 2007; Tang *et al.*, 2008a; 2008b; Sun *et al.*, 2011), and allow us to understand the environmental benefits of incineration.

Incineration of phosphatized sludge leaves more heavy metal compounds in bottom ash because they are not volatilizing during incineration. The concentrations of heavy metals in bottom ash of pre-treated sludge are greater than in the bottom ash of untreated sludge. Considering the reutilization of the bottom ash, its environmental compatibility must also be guaranteed through lowering the leachability of heavy metals. Nevertheless, the knowledge about the influence of pre-treatment with phosphorus-based amendments on stabilization of heavy metals in bottom ash of pre-treated sludge is limited.

The purpose of this study is to evaluate the effectiveness of pre-treatment with phosphorus-based amendments on the immobilization of Cu, Zn, Cr, Pb and Cd in tannery sludge and its bottom ash. The specific aims are to compare the effects of phosphoric acid and monobasic calcium phosphate on heavy metal immobilization, and to examine the effectiveness of heavy metal immobilization before and after incineration.

2 Materials and methods

2.1 Materials

Tannery sludge was collected from Wenzhou, China in 2011. The water contained in the sludge was extracted by mechanical dewatering methods and the moisture content of the samples was decreased to about 75%. The samples were stirred uniformly and then dried at 65 °C. The chemical characteristics and heavy metal concentrations in the sludge were analyzed (Table 1).

Two different phosphorus-based amendments were used to stabilize heavy metals in sludge. One

was liquid acid, phosphoric acid (PA), and the other was slightly soluble salt solid, monobasic calcium phosphate (MCP). At room temperature, two groups of tannery sludge, each with six samples, were tested. For each sample, 30.0 g of material was added to a beaker at room temperature; the water content of each was then adjusted to 50% to exhibit the rheology of thixotropic slurry, thereby achieving the best compromise between minimum water input and optimal contact between the reactant and the solids (Piantone *et al.*, 2003). The PA (85% H₃PO₄) or MCP powders were doped according to different mass ratios between PO₄³⁻ and dried sludge (3%, 5%, 7%, 10%, and 20%) respectively, and then mixtures were agitated for 5 h with a magnetic stirrer to ensure thorough mixing before standing for 24 h. Then, the phosphatized sludge was put in a drying bed to avoid moisture interference. Finally, the formed products were utilized for follow-up experiments.

2.2 Apparatus and experimental procedure

As shown in Fig. 1, the incineration apparatus used in this study was composed of an electric-heated tube furnace and an air supply. The heart of the furnace was a quartz tube burner, 600-mm long and 40-mm in inner diameter. A porcelain boat moved by quartz rod was designed to feed the sludge into the combustion chamber. The combustion temperature at the center inside of the burner tube was monitored by a thermocouple and controlled by a programmed temperature controller. Finally, the oven was connected to two impingers filled with a solution of 5% HNO₃ allowing for the determination of the collection of the volatilization fraction of the heavy metals.

Table 1 Characteristics of the sludge

Composition	Value
Ultimate analysis (dry basis) (% in weight)	
C	18.95
H	3.12
O	16.21
N	2.85
S	0.64
Heavy metal analysis (dry basis) (mg/g)	
Zn	0.26
Cr	17.14
Pb	1.61
Cd	0.01
Cu	0.03

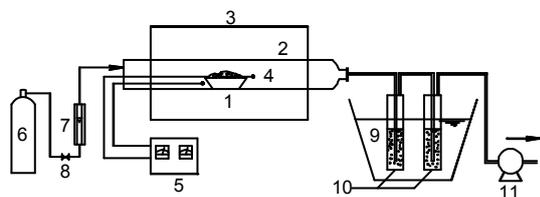


Fig. 1 Laboratory tube furnace for combustion experiment
1: porcelain boat; 2: quartz tube; 3: tube furnace; 4: thermocouple; 5: thermocontroller; 6: air supply; 7: flow meter; 8: regulating valve; 9: water cooler; 10: impingers (5% HNO₃); 11: aspirator pump

Experiments were carried out by the combustion of 10 g of prepared samples in a porcelain boat that was pushed into a quartz tube. During incineration experiments, air flow rate was fixed at 120 L/h and the incineration temperature was 900 °C.

2.3 Analysis methods

The leaching test was conducted according to US EPA (1992) SW-846 toxicity characteristics leaching procedure (TCLP) test method 1311 to evaluate the leaching behaviors of Cu, Cr, Pb, Zn and Cd in pre-treated sludge and its bottom ash. TCLP is commonly used to determine whether a waste is hazardous and if a treated waste meets the treatment standards for land disposal. This test provides useful information on the potential leachability of metals in sludge and bottom ash. A 5.7-ml aliquot of glacial acetic acid was diluted to 1.0 L with deionized water. The pH of the extracting solution was 2.88±0.05. The extracting solution was added according to the liquid to solid ratio of 20:1.

The mineral phases of samples were identified by X-ray diffraction (XRD) measurement. The XRD analysis was performed on a TD-3500 X-ray diffractometer using MDI Jade 5.0 software (Materials Data Inc., Liverpool, CA). The operating condition of X-ray is D/max-γ β X-ray diffractometer. XRD patterns were obtained from 10° to 80° (2θ) at a scanning speed of 6°/min.

3 Results and discussion

3.1 Results of leaching heavy metals from pre-treated sludge

The mobility of metals mobility is strongly associated with their water solubility. Overall, the raw

tannery sludge showed higher water solubility of Pb and Cr. Their concentrations were 0.426 mg/L and 0.454 mg/L. The high concentrations of soluble Pb and Cr were due to the high levels of Pb and Cr in the tannery sludge.

The results of the leaching tests are presented in Fig. 2. The results demonstrated that both PA and MCP used in this study lowered the Cu, Pb and Cd concentrations in the effluent resulting from TCLP experiments. The leachability of Cu in PA treated tannery sludge decreased from 0.228 mg/L to 0.181 mg/L, while it decreased to 0.196 mg/L when the sludge was pre-treated with MCP as shown in Fig. 2a. The extractable concentrations of Pb and Cd in the PA pre-treated sludge also decreased by about 32.6% and 44.7%, respectively. In comparison, the extractable concentrations of Pb and Cd decreased 26.05% and 30.3%, respectively, in MCP pre-treated sludge. On the other hand, stability of Zn was adversely affected from this treatment. Its solubility increased from the initial value of 0.087 mg/L up to 0.204 mg/L and 0.192 mg/L at the highest tested PA and MCP ratios, respectively (Fig. 2b).

For Cr, the leachability was increased greatly from 0.454 mg/L to 1.736 mg/L when PA increased from 0 to 5%, and the induction reached a peak when the addition of PA exceeded 7% as shown in Fig. 2e. Overall, the water solubility of Cr can be considered nearly unchanged when the sludge was treated with MCP.

3.2 Results of leaching heavy metals from bottom ash of pretreated sludge

Figs. 3a–3e shows the leaching results of Cu, Zn, Pb, Cd and Cr in bottom ash of pre-treated tannery sludge. With incineration, both PA and MCP pre-treatments significantly reduced water soluble Pb and Cr in the bottom ash. In a comparison between untreated sludge and the 20% PA pretreated sludge, the Pb concentration decreased from 0.41 mg/L to 0.036 mg/L, while the Cr decreased from 67.31 mg/L to 0.098 mg/L. Similarly, the concentrations of Pb and Cr resulting from MCP pre-treated sludge also decreased from 0.41 mg/L to 0.197 mg/L and from 67.31 mg/L to 0.261 mg/L, respectively. Fig. 3d shows that treatment of sludge with increasing ratios of PA or MCP resulted in the increased stabilization of Cd in its bottom ash. PA reduced Cd solubility from

the initial value of 0.054 mg/L down to 0.020 mg/L and MCP reduced to 0.034 mg/L.

Unlike Pb, Cr and Cd, water soluble Cu and Zn in bottom ash were elevated after sludge was pre-treated by PA and MCP as shown in Fig. 3a and Fig. 3b.

3.3 Results of XRD analysis

The XRD patterns of bottom ash of raw tannery sludge incinerated at the temperature of 900 °C, are recorded in Fig. 4. Results showed that the main crystal phases of heavy metals in the bottom ash were Cr_5O_{12} , CuO , $\text{Pb}_{11}\text{CrO}_{16}$, ZnCr_2O_4 and CdCa .

After sludge was pre-treated with different contents of PA, the XRD patterns of its bottom ash are presented in Fig. 5 (p.182). It was observed that some new mineral compounds, such as $\text{Ca}_9\text{Cr}(\text{PO}_4)_7$, $\text{Pb}_3\text{Cr}(\text{PO}_4)_3$, $\text{Zn}_3(\text{PO}_4)_2 \cdot 4\text{H}_2\text{O}$ (*Hopeite*), $\text{Cu}_3(\text{PO}_4)(\text{OH})_3$ (*Libethenite*), $\text{Cd}(\text{PO}_3\text{F})_2 \cdot 2\text{H}_2\text{O}$ and $\text{Pb}_2\text{P}_4\text{O}_{12} \cdot 2\text{H}_2\text{O}$, appeared as shown in Fig. 5. When the content of H_3PO_4 increased, the characteristic diffraction peaks near 2θ of 21° , 31° , 35° , and 41° were observed to appear and become obvious. From these peaks, it is almost confirmed that the main formations of heavy metals in bottom ash of sludge doped with PA.

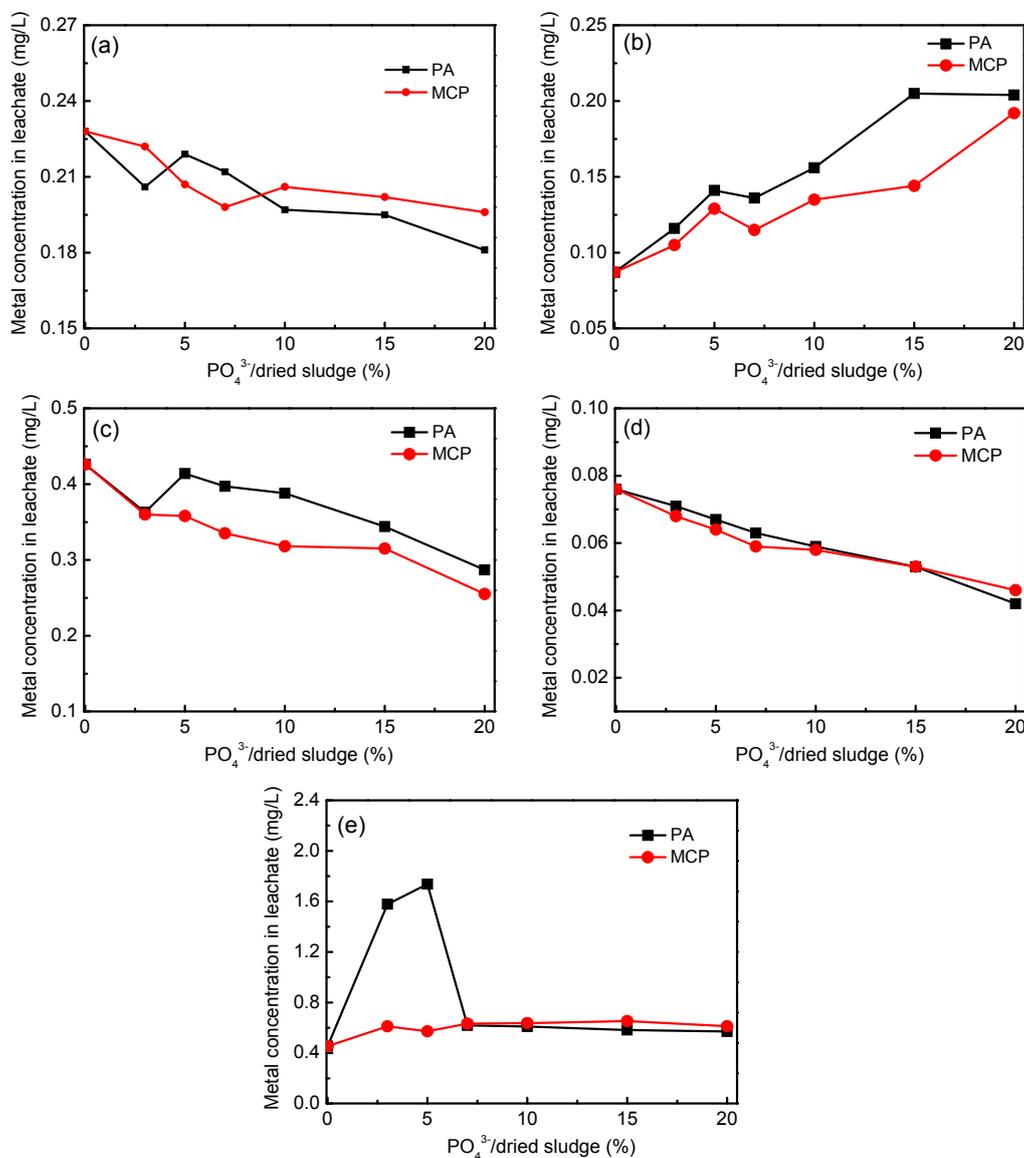


Fig. 2 TCLP concentration of tannery sludge pre-treated by PA and MCP
(a) Cu; (b) Zn; (c) Pb; (d) Cd; (e) Cr

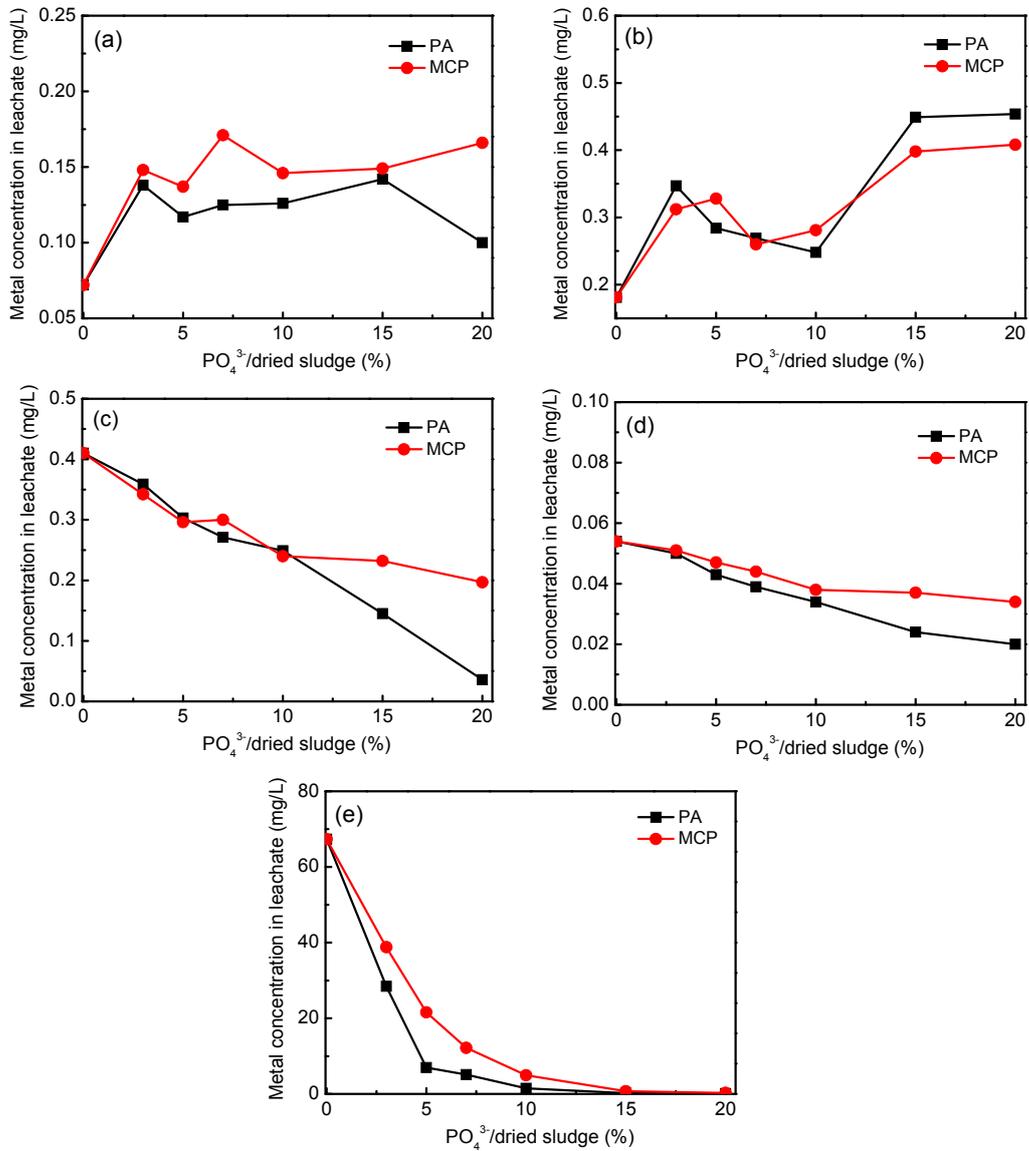


Fig. 3 TCLP concentration of the bottom ash of tannery sludge pre-treated by PA and MCP (a) Cu; (b) Zn; (c) Pb; (d) Cd; (e) Cr

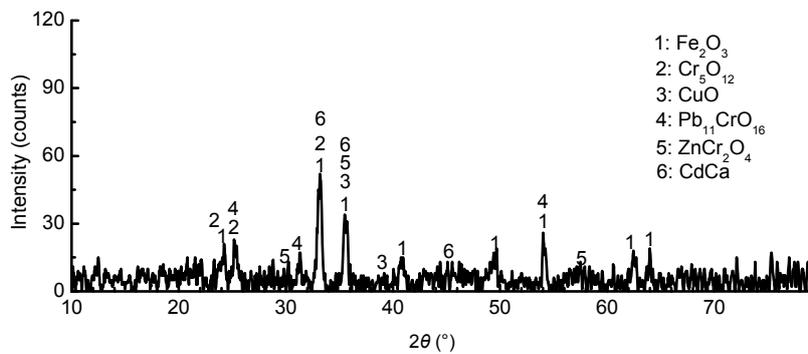


Fig. 4 XRD patterns of bottom ash of raw tannery sludge

Fig. 6 shows the XRD pattern of the bottom ash of sludge pre-treated with MCP after incineration at 900 °C. The pattern consists of strong intensity peaks corresponding to Fe_2O_3 and weak peaks of

$\text{Na}_3\text{Cr}(\text{PO}_4)_2$, $\text{Pb}_3\text{Cr}(\text{PO}_4)_3$, $\text{Na}(\text{Fe}, \text{Zn})\text{PO}_4$, $\text{Ca}_{19}\text{Cu}_2\text{H}_2(\text{PO}_4)_{14}$, $\text{Cu}_3(\text{PO}_4)(\text{OH})_3$ (*Libethenite*), $\text{Cd}(\text{H}_2\text{PO}_4)_2$ and $\text{Pb}_3\text{P}_4\text{O}_{13}$. When the content of MCP increased to 20%, the peaks of these minerals also

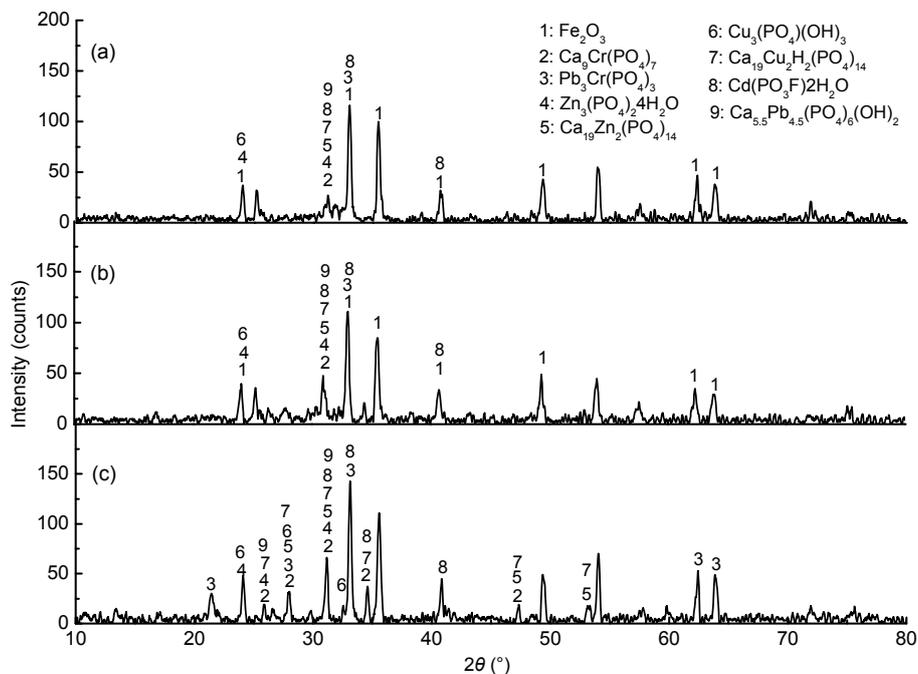


Fig. 5 XRD patterns of bottom ash of tannery sludge pretreated by 5% (a), 10% (b), and 20% (c) PA

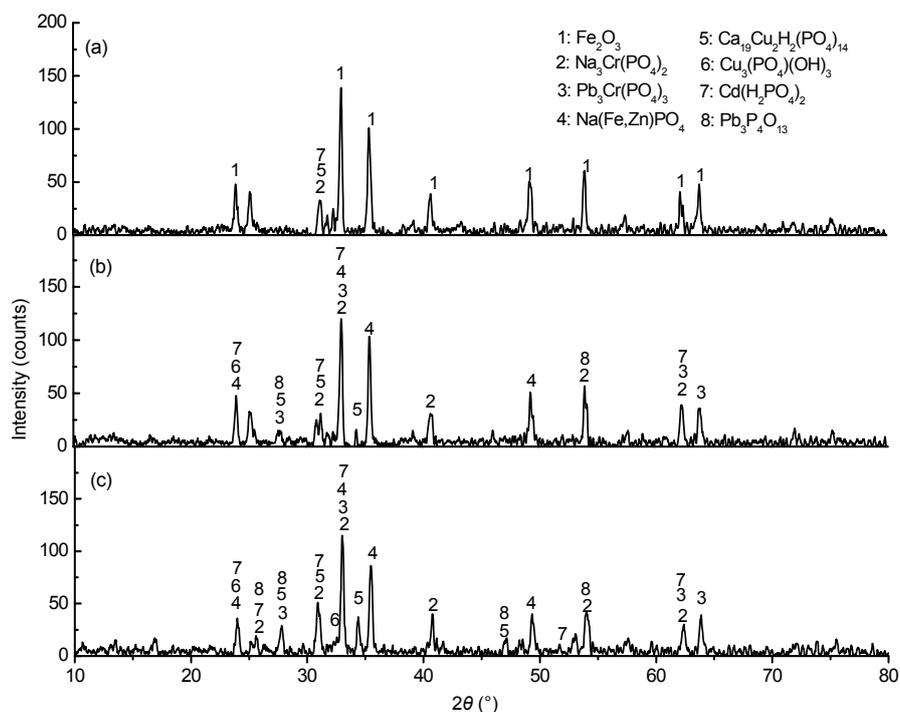


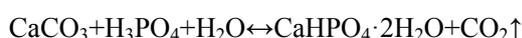
Fig. 6 XRD patterns of bottom ash of tannery sludge pre-treated by 5% (a), 10% (b), and 20% (c) MCP

became sharper and stronger, indicating that these crystals become the major phase in the bottom ash of sludge pre-treated with MCP.

The mineralogical major phases of the sludge and bottom ash before and after phosphate treatment can be included as shown in Table 2.

3.4 Discussion

When tannery sludge, which may contain CaCO_3 , was mixed with PA, the chemical reaction with H_3PO_4 lead to the formation of foam following the reaction

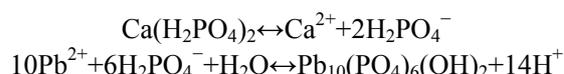


The foam was formed during the mixing process.

Although most of the PA reacts with CaCO_3 , the addition of phosphoric acid also allows the formation of other insoluble metal phosphates. As shown in Fig. 2, the reduction of water soluble Pb in the PA treatment was attributed to the transformation of Pb from soluble Pb to insoluble Pb phosphate (Table 2). It is thermodynamically favorable for dissolved Pb to react with P for formation of insoluble Pb phosphate, but less for Zn and Cu to form Zn- and Cu-phosphates (Cao *et al.*, 2009), so there are no obvious positive effects for Cu, Zn, Cd and Cr. Moreover, due to the formation of Ca-phosphate in the sludge, Cu and Cd can be slightly immobilized due to the ion exchange and complexation mechanisms as shown in Table 2 (Da Rocha *et al.*, 2002).

On the other hand, the exact reaction mechanism responsible for the removal of metal ions by MCP remains unknown. However, previous research suggested that the reaction mechanisms for metal immobilization by phosphate minerals include: (a)

ion exchange process; (b) surface complexation; (c) dissolution of the original phosphate minerals and precipitation of new metal phosphates; and, (d) substitution of Ca in phosphate by other metals during recrystallization (co-precipitation) (Jeanjean *et al.*, 1994; Ma *et al.*, 1994). Several groups suggested that phosphate anions, which can be provided through dissolution of MCP, reacted with lead cations and formed $\text{Pb}_{10}(\text{PO}_4)_6(\text{OH})_2$ (Ma *et al.*, 1994; Xu and Schwartz, 1994; Zhang *et al.*, 1997) as



Similarly, it also proved that Cd can be fixed in the formation of Cd-containing phosphates (Mignardi *et al.*, 2012). Therefore, the application of MCP efficiently reduced the extractable fractions of Pb and Cd in tannery sludge as shown in Fig. 2. Similar results were also found by Theodoratos *et al.* (2002) when they stated that the treatment with MCP stabilized Pb and Cd effectively. Moreover, the fixation mechanism of Cu and Zn involved both surface complexation and co-precipitation (Xu and Schwartz, 1994). Ma *et al.* (1994) also proved that Cu and Zn reacted with dissolved P through precipitation of amorphous to poorly crystalline metal phosphates. Thus, the treatment had slight positive effects for Cu. Contrastingly, addition of PA and MCP to the sludge significantly increased sludge acidity, and the pH of the suspensions decreased from 10.53 to 4.04 and 5.31, respectively after pre-treatment with PA and MCP. Therefore, a significant increase of Zn solubility was observed when the PA and MCP doses were increased. Results of this study were consistent with the previous studies (Theodoratos *et al.*, 2002; Cao *et al.*, 2009). It can be

Table 2 Major phases of the sludge and bottom ash before and after phosphate treatment

Sample	Major phase
Raw sludge	CaCO_3 ; $\text{Cu}_3(\text{CO}_3)_2\text{OH}_2$; $\text{Zn}_5(\text{CO}_3)_2(\text{OH})_6$; $\text{Ca}_6\text{Cr}_2(\text{SO}_4)_3(\text{OH})_{12}$; $\text{Pb}_2\text{Cu}(\text{CrO}_4)(\text{OH})_5$; $\text{CdSO}_4\text{H}_2\text{O}$
Bottom ash of raw sludge	Cr_5O_{12} ; CuO ; $\text{Pb}_{11}\text{CrO}_{16}$; ZnCr_2O_4 ; CdCa
Sludge pretreated with 20% PA (sludge I)	$\text{Pb}_3(\text{PO}_4)_2$; $\text{Pb}_5(\text{PO}_4)_3\text{OH}$; $\text{Cu}_3(\text{PO}_4)_2$; $\text{CaZn}_2(\text{PO}_4)_2$; CdCrO_4 ; $(\text{Cu,Zn})_3(\text{PO}_4)(\text{OH})_3$
Bottom ash of sludge I	$\text{Ca}_9\text{Cr}(\text{PO}_4)_7$; $\text{Pb}_3\text{Cr}(\text{PO}_4)_3$; $\text{Zn}_3(\text{PO}_4)_2\cdot 4\text{H}_2\text{O}$; $\text{Cu}_3(\text{PO}_4)(\text{OH})_3$; $\text{Cd}(\text{PO}_3\text{F})_2\text{H}_2\text{O}$; $\text{Pb}_2\text{P}_4\text{O}_{12}\text{H}_2\text{O}$
Sludge pre-treated with 20% MCP (sludge II)	$\text{Pb}_3(\text{PO}_4)_2$; $\text{Pb}_5(\text{PO}_4)_3\text{OH}$; $\text{Cu}_3(\text{PO}_4)_2$; $\text{Ca}_{19}\text{Zn}_2(\text{PO}_4)_{14}$; $\text{Ca}_9\text{Cr}(\text{PO}_4)_7$; $\text{Ca}_8\text{Pb}_2(\text{PO}_4)_6(\text{OH})_2$; $\text{Zn}_3(\text{PO}_4)_2\cdot 4\text{H}_2\text{O}$
Bottom ash of sludge II	$\text{Na}_3\text{Cr}(\text{PO}_4)_2$; $\text{Pb}_3\text{Cr}(\text{PO}_4)_3$; $\text{Na}(\text{Fe,Zn})\text{PO}_4$; $\text{Ca}_{19}\text{Cu}_2\text{H}_2(\text{PO}_4)_{14}$; $\text{Cu}_3(\text{PO}_4)(\text{OH})_3$; $\text{Cd}(\text{H}_2\text{PO}_4)_2$; $\text{Pb}_3\text{P}_4\text{O}_{13}$

inferred that the increase of Zn solubility was attributed to the weak bonds of surface complex mechanism between Zn and phosphate. This finding also explained why the leachability of Zn was greater in the bottom ash of PA pre-treated sludge than in the bottom ash of MCP treated sludge as shown in Fig. 2b.

With respect to Cr, the initial elevation of Cr in the case of PA treatment might also be the result of sludge acidification via PA addition. When the PA concentration was further increased, the leachability of Cr decreased to the level observed without treatment. It could be interpreted that at high levels of PA, the extra PA reacted with CaCO_3 which resulted in the reduction of Cr solubility. However, in agreement with the results of previous study (Quina *et al.*, 2010), the stabilization treatment with PA or MCP does not have a marked positive effect on Cr stabilization.

After incineration at the temperature of 900 °C, the metal phosphates of heavy metals were stabilized in the bottom ash due to their high thermostability. $\text{Zn}_3(\text{PO}_4)_2 \cdot 4\text{H}_2\text{O}$ (*Hopeite*), $\text{Cu}_3(\text{PO}_4)(\text{OH})_3$ (*Libethenite*), $\text{Pb}_3\text{P}_4\text{O}_{12}$, $\text{Cd}(\text{H}_2\text{PO}_4)_2$ were identified in the XRD patterns of bottom ash as major phases (Fig. 5 and Fig. 6). Some of the metal phosphates were apt to bond to each other and form complexes in the combustion process because of the following reaction,



Therefore, the minor phases of minerals, such as $\text{Ca}_{19}\text{Zn}_2(\text{PO}_4)_{14}$ (*Scholzite*) and $\text{Ca}_{19}\text{Cu}_2\text{H}_2(\text{PO}_4)_{14}$, appeared in the bottom ash as shown in Fig. 5 and Fig. 6. Those minerals were more thermally stable and resulted in the accumulation of the heavy metals in the bottom ash during the incineration process (Tang *et al.*, 2008b; Sun *et al.*, 2011). Similarly, addition of PA and MCP can significantly increase bottom ash acidity. Previous research has proved that the solubility of Cu and Zn were significantly increased when the pH decreased within a certain range (Cao *et al.*, 2004). Therefore, sludge pre-treatment with PA and MCP increased Cu and Zn solubility in resulting bottom ash as shown in Figs. 3a and 3b.

Lead phosphates, in particular pyromorphite, are the most insoluble forms of Pb minerals in soils under a wide range of environmental conditions (Lindsay, 1979; Nriagu, 1984). The formation of $\text{Pb}_3\text{Cr}(\text{PO}_4)_3$ in the combustion also improved the stability of Pb

and Cr (Fig. 5 and Fig. 6). Hence, the pre-treatments with PA and MCP were seen to efficiently stabilize Pb and Cr in the bottom ash of pre-treated sludge. A significant reduction in water soluble Pb and Cr in bottom ash of PA and MCP treated sludge was achieved as shown in Figs. 3c and 3e. For Cd, it also showed low leachability in general agreement with the formation of insoluble phases, such as $\text{Cd}(\text{PO}_3\text{F})_2 \cdot \text{H}_2\text{O}$ and $\text{Cd}(\text{H}_2\text{PO}_4)_2$. On the other hand, the effectiveness of PA on the immobilization of Pb, Cd and Cr in bottom ash was much better than MCP as shown in Figs. 3c–3e. It may be due to the greater availability of P in the PA. However, pre-treatment with MCP was similarly effective with respect to PA in immobilizing Cr in bottom ash. Although less effective, the application of MCP to reduce heavy metal emission from the bottom ash may minimize the potential risk of eutrophication resulting from the use of highly soluble phosphate amendments. Thus, we conclude that MCP is appropriate in the heavy metal immobilization in pre-treatment of tannery sludge that is high in Cr content before incineration.

4 Conclusions

In this study, the pre-treatment of tannery sludge with PA and MCP was tested as a potential heavy metal emission control option. This treatment was shown to effectively stabilize Pb and Cd in the tannery sludge. Pb and Cd leachability, as determined by TCLP leaching tests, decreased with increasing P amendment addition rate by 32.6% and 44.7% for PA treatment and 40.1% and 39.5% for MCP treatment, respectively. Cu could be slightly immobilized by PA and MCP pre-treatment, falling by 19.6% and 14.1%, respectively, whereas pre-treatment process had no obvious positive effect for Cr. However, an increase in Zn leachability was observed, resulting from the acidification of sludge due to the addition of PA or MCP.

After incineration at a temperature of 900 °C, pre-treatment of sludge with phosphorus-containing amendments significantly lowered the water solubility of Pb and Cr in the bottom ash. With the increase of PA or MCP addition, Pb and Cr leachability decreased by 91.2% and 99.8% for the PA pre-treatment and 52.0% and 99.6% for the MCP pre-treatment,

respectively. Cd could also be effectively stabilized in the bottom ash. The stabilization of these metals was due to the formation of their highly thermostable minerals, such as Pb-phosphates, Cd-phosphates and pyromorphite-like minerals during the incineration process. The results proved that Pb, Cr and Cd in bottom ash had high chemical stability when sludge was pre-treated by phosphorus-containing amendments before incineration. On the other hand, pre-treatment with PA had more effect on heavy metals immobilization than MCP, which may be due to the higher availability of P in PA. However, the acid extractability of Cu and Zn in the bottom ash was increased in the pre-treatment with PA or MCP. This study demonstrates that both PA and MCP pre-treatment approaches are suitable for the prevention of heavy metal emission during the incineration of sludge with high Pb, Cd and Cr contents.

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