



A numerical approach to the interaction between airflow and a high-speed train subjected to crosswind*

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Abstract: Aerodynamic forces and dynamic performances of railway vehicles are coupled and affected by each other. On the one hand, aerodynamic forces change the displacements of a train. On the other hand, displacements affect aerodynamic forces. Based on vehicle-track coupling dynamics and aerodynamics, a numerical approach to the interaction between airflow and a high-speed train is presented in this paper. Aerodynamic forces and dynamic performances of a high-speed train subjected to crosswind were numerically simulated. Results showed that the interaction between airflow and a high-speed train has a significant influence on displacements and aerodynamic forces of the head coach. Therefore, it is necessary to consider the interaction between airflow and a high-speed train subjected to crosswind.

Key words: High-speed train, Crosswind, Aerodynamics, Co-simulation, Interaction

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1 Introduction

The crosswind stability of railway vehicles has been studied for several decades, motivated by overturning accidents (Cheli *et al.*, 2010; Li *et al.*, 2011a). Most studies on crosswind stability have focused on aerodynamic issues.

Aerodynamics of railway vehicles subjected to crosswind can be investigated by experiments in wind tunnels and numerical simulations. Wind tunnel experiments have played an important role in determining the aerodynamic characteristics of trains for years. In (Orellano *et al.*, 2006), experimental results for aerodynamic forces were reported, and comparisons were made with regard to different levels of geometric complexity addressing the issues of bogies and spoilers. There was only a small effect for the coefficients, which contributed most to overturning,

i.e., the roll moment and the side force. Cheli *et al.* (2010) presented a numerical experimental procedure for the aerodynamic optimization of AnsaldoBreda EMUV250. Wind tunnel experiments (Suzuki *et al.*, 2003; Bocciolone *et al.*, 2008) were performed to evaluate the aerodynamic characteristics of railway vehicles on typical infrastructures, such as bridges and embankments. To date, the only full-scale experiments were performed on a coastal site at Eskmeals in Cumbria (northwest England) (Baker *et al.*, 2004). Thorough reviews were given by Baker (1991).

In addition, several numerical simulations of aerodynamic characteristics of railway vehicles subjected to crosswind were performed. The unsteady aerodynamic forces of a high-speed train were analyzed in a variety of unsteady crosswinds (Xu and Ding, 2006; Baker, 2010; Thomas *et al.*, 2010; Baker *et al.*, 2011; Shao *et al.*, 2011). A 3D source/vortex panel method (Chiu, 1995) was developed to predict the aerodynamic loads on an idealized railway train model in crosswind at large yaw angles. Numerical results of the airflow passing a simplified train under different yawing conditions were summarized (Khier *et al.*,

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2000). Diedrichs (2003) and Diedrichs *et al.* (2007) discussed the aerodynamic characteristics of the air-flow passing a train and found that the 6-m high embankments reduced the permissible crosswind velocity by approximately 20%. Moreover, numerical simulations were carried out using the commercial code FLUENT or STAR-CD (Diedrichs *et al.*, 2007; Cheli *et al.*, 2010).

The dynamic response of a railway vehicle subjected to crosswind was calculated using a vehicle model. Baker (1991) and Ding *et al.* (2008) used the simple vehicle models to evaluate the running safety against crosswind. In fact, the vehicle and track subsystems were coupled through wheel/rail interaction (Zhai *et al.*, 1996). A detailed vehicle-track coupling model was established for the first time (Zhai *et al.*, 1996); the model has been widely applied.

The crosswind stability in the aforementioned studies was evaluated using an off-line simulation method. Firstly, aerodynamic forces of a train subjected to crosswind were calculated by computational fluid dynamics (CFD), and then, the dynamic response of the train subjected to crosswind was simulated using a vehicle or vehicle-track model. The influence on the aerodynamic forces of displacements was neglected using the off-line simulation. In fact, aerodynamic forces and dynamic performances of railway vehicles were coupled. On the one hand, the aerodynamic forces change the displacements of the train. On the other hand, the displacements affect the aerodynamic forces. To date, there has been no research to simulate the interaction between airflow and a high-speed train.

In this paper, a numerical approach to the interaction between airflow and a high-speed train was presented. The vehicle-track coupling model was adopted to calculate the dynamic response of the train subjected to crosswind. Dynamic performances of a high-speed train subjected to crosswind were discussed in detail.

2 Governing equations

2.1 Equations of fluid dynamics

The flow field around a train subjected to crosswind can be considered as a 3D incompressible viscous turbulent flow. To describe the flow field around the train, a k - ε turbulence model is adopted.

The equations of the standard k - ε two-equation model are written as

$$\begin{aligned} \frac{\partial}{\partial t} \int_V \rho \phi dV + \int_A \mathbf{n}(\rho(\mathbf{u} - \bar{\mathbf{u}})\phi) dA \\ = \int_A \mathbf{n}(\Gamma \text{grad}\phi) dA + \int_V \mathbf{S} dV, \end{aligned} \quad (1)$$

where V is an arbitrary control volume, A is the surface of the volume V , t is the time, ρ is the air density, \mathbf{u} is the velocity vector of the flow, $\bar{\mathbf{u}}$ is the velocity vector of the surface A , ϕ is the vector of fluxes, \mathbf{n} is the normal direction vector of the surface A , \mathbf{S} is the source term, and Γ is the generalized diffusion coefficient. The vector ϕ includes the flow velocity u_i , the turbulent kinematics energy k , and turbulent dissipation ε .

2.2 Equations of vehicle-track coupling dynamics

Vehicle-track coupling dynamics mainly consist of vehicle dynamics, track dynamics, and wheel-rail interaction.

A four-axle railway vehicle with two suspension systems, which is a common railway vehicle used in China, was chosen in this study. The vehicle shown in Fig. 1a consists of a carbody, two bogies, four wheelsets, and two suspension systems. The carbody, bogies, and wheelsets are regarded as rigid components, and their elastic deformations are neglected. Every rigid component is assigned five degrees of freedom: the vertical displacement, the lateral displacement, the roll displacement, the yaw displacement, and the pitch displacement with respect to its mass center.

The track subsystem shown in Fig. 1b is modeled as an infinite Euler beam, which is supported on a discrete-elastic foundation consisting of three layers. The sleeper is assigned three degrees of freedom: the vertical displacement, the lateral displacement, and the roll displacement. To account for the shearing continuity of the particles between the adjacent ballasts, linear springs and dampers are introduced to model the shear coupling effects. Moreover, the ballasts are assigned only one degree of freedom: the vertical displacement.

Wheel-rail interaction involves two basic issues: the geometric relationship and the contact forces. The Hertz contact theory is used to solve the vertical

normal forces. The creep forces are calculated using the Shen-Hedrick-Elkins theory. More detailed descriptions of the normal and creep forces can be found in (Zhai et al., 1996). In this study, rail irregularities are measured from high-speed railways in China.

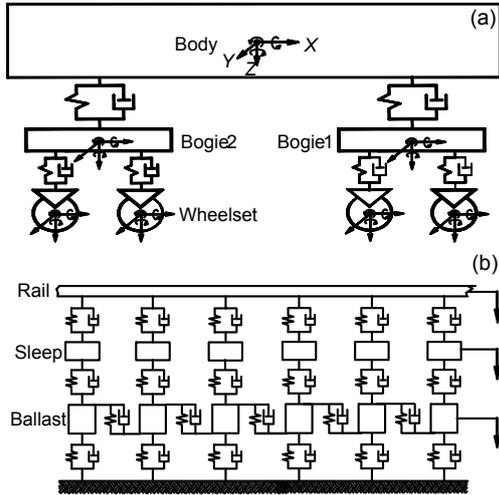


Fig. 1 Vehicle-track coupling system
(a) Vehicle system; (b) Track system

The equation of the vehicle-track dynamics (Zhai et al., 1996) is written as

$$M\ddot{X} + C\dot{X} + KX = F, \quad (2)$$

where M , C , and K are the mass, damping, and stiffness matrices of the vehicle-track system, respectively. X , \dot{X} , and \ddot{X} are the generalized displacement, velocity, and acceleration vectors of the system, respectively. F is the generalized force vector including wheel rail contact forces and aerodynamic forces.

3 Numerical approach to the interaction

3.1 Vehicle-track dynamics solution technique

The equations of vehicle-track dynamics were solved using the Zhai method (Zhai et al., 1996). The integral format of the Zhai method is written as

$$\begin{cases} X_{n+1} = X_n + \dot{X}_n \Delta t + (1/2 + \mu)\ddot{X}_n \Delta t^2 - \mu\ddot{X}_{n-1} \Delta t^2, \\ \dot{X}_{n+1} = \dot{X}_n + (1 + \lambda)\ddot{X}_n \Delta t - \lambda\ddot{X}_{n-1} \Delta t, \end{cases} \quad (3)$$

where λ and μ are integral parameters, Δt is the time

step and the subscript n denotes the iteration number of the time step.

Eq. (3) at the time $t=(n+1)\Delta t$ is given by

$$M\ddot{X}_{n+1} + C\dot{X}_{n+1} + KX_{n+1} = F_{n+1}. \quad (4)$$

Substituting Eq. (3) into Eq. (4), \ddot{X}_{n+1} can be obtained.

The code for the vehicle-track coupling dynamics was written in the programming language Fortran and verified to be trustworthy (Li et al., 2011a).

3.2 Dynamic mesh technique

Re-mesh and spring analogy methods (Li et al., 2011b) were adopted to renew the mesh of CFD. If the spring analogy method fails to renew the mesh, the re-mesh method is adopted. The spring analogy method is simple but highly efficient. The stiffness of a given edge $i-j$ is defined as $K_{ij}=1/r_{ij}$, where K_{ij} is the stiffness, and r_{ij} is the distance between the i th and j th nodes.

The displacements of nodes are obtained:

$$\sum_j^{N_i} K_{ij} \Delta r_j = 0, \quad (5)$$

where N_i is the total number of nodes connected to the i th node, and Δr_j is the displacements of the j th node.

The new position of the i th node is determined by

$$\bar{r}_i = r_i + \Delta r_i. \quad (6)$$

3.3 Solution strategies

Co-simulation means that aerodynamic forces and dynamic performances of a high-speed train are calculated alternatively; namely, the interaction between airflow and a high-speed train is considered.

Fig. 2 shows a schematic diagram of the numerical approach to the interaction between airflow and a high-speed train. The aerodynamic forces F include the side force, the lift force, the roll moment, the pitch moment, and the yaw moment. The displacements of the train D include the lateral displacement y , the vertical displacement z , the roll displacement θ , the yaw displacement ψ , and the pitch displacement β .

Δt_f and Δt_v represent the time step sizes in the computational fluid dynamics and vehicle-track dynamics, respectively. Generally, the orders of magnitude of Δt_f and Δt_v are 1.0×10^{-3} s and 1.0×10^{-5} s, respectively. As shown in Fig. 2, the procedure for the numerical approach to the interaction between airflow and a high-speed train can be summarized as follows:

1. Calculate the aerodynamic forces of the train in an initial static status until the forces reach relatively steady values, such as the fluctuation is less than 3%.
2. Transfer the message of aerodynamic forces to the user-defined-function (UDF), which is an interface of the commercial code FLUENT, and then invoke the code for the vehicle-track coupling dynamics.
3. Load the above aerodynamic forces onto the vehicle-track model and calculate the dynamic response of the vehicle. The number of time step iterations for the vehicle-track dynamics is $\Delta t_f / \Delta t_v$.
4. Transfer the message of displacements to the commercial code FLUENT.
5. Renew the mesh of CFD using the dynamic mesh technique described in Section 3.2.
6. Keep solving Eq. (1) and calculate the aerodynamic forces of the train in the above displacements.
7. Repeat steps 2–6 until the number of time step iterations reaches the expected value.

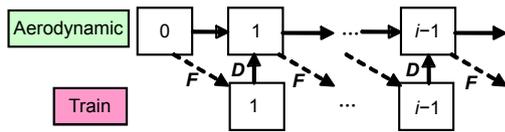


Fig. 2 Numerical procedure

4 Computational model and domain

A schematic diagram of the computational domain of a high-speed train subjected to crosswind is shown in Fig. 3. The ballast, sleeper, and rails are neglected in the computational fluid dynamics. Unstructured tetrahedral meshes were adopted.

The running speed of the train u_t and crosswind velocity u_w were specified at the inlet boundary, i.e., $u_{inlet} = -u_t$; $v_{inlet} = u_w$. In addition, traction-free and symmetry conditions were specified at the outlet and top boundaries, respectively. The slip condition was

specified at the wall boundary, i.e., $u_{wall} = -u_t$. Although natural wind was turbulent and a boundary layer existed near the ground, the effect of the boundary layer was neglected and a uniform inflow was adopted. The calculation was performed for the high-speed train at $u_t = 350$ km/h and subjected to crosswind $u_w = 13.8$ m/s. The combined wind velocity was 98.2 m/s and the yaw angle was 8.08° , as shown in Fig. 4.

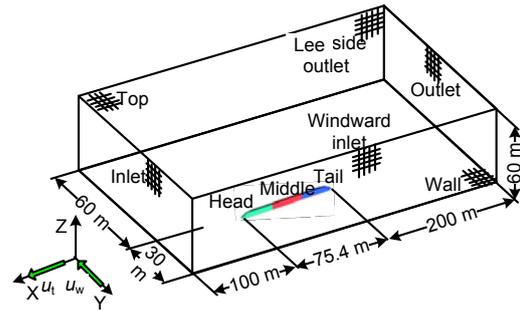


Fig. 3 Schematic diagram of computational domain



Fig. 4 Schematic diagram of the combined wind velocity β : yaw angle; V_c : combined velocity

Fig. 5 shows a schematic diagram of aerodynamic forces and moments. Aerodynamic forces include the side force F_y , the lift force F_z , the roll moment M_x , the pitch moment M_y , and the yaw moment M_z . The reference points of the moment of head, middle, and tail coaches are $(-13.2, 0.0, 1.72)$, $(-38.2, 0.0, 1.72)$ and $(-63.2, 0.0, 1.72)$, respectively.

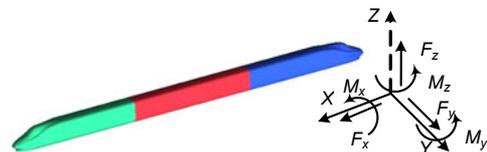


Fig. 5 Schematic diagram of aerodynamic forces

In order to describe the flow field around a train and the wall-stress on the train surface, a $k-\epsilon$ turbulence model with a wall function treatment was adopted. The Reynolds averaged Navier-Stokes (RANS) equations were used to simulate the flow field around the train and solved by the finite volume

method (FVM). The velocity-pressure coupling was achieved by using the SIMPLE (semi-implicit method for pressure linked equations) scheme. The techniques for solving the fluid dynamics in this study were similar to those in (Diedrichs *et al.*, 2007). Numerical simulations were carried out using the commercial code FLUENT.

Table 1 shows the effect of aerodynamic forces on the maximum mesh sizes of the train surface. It is shown that aerodynamic forces are almost stable when the maximum mesh sizes of head, middle, and tail coaches are 80 mm, 100 mm, and 80 mm, respectively. Therefore, these sizes were chosen.

Table 1 Effect of aerodynamic forces on mesh sizes

Mesh sizes (mm)			F_y (kN)		F_z (kN)	
Head	Mid	Tail	Head	Tail	Head	Tail
120	150	120	-49.22	-16.87	4.46	11.97
100	120	100	-48.72	-16.06	5.42	11.30
80	100	80	-47.22	-15.25	6.38	10.83
60	80	60	-46.71	-14.99	6.46	10.63

Table 2 shows the effect of aerodynamic forces on the computational domain including the length L , width W , and height H . For example, the length 75+150 means that the distance between the inlet surface and nose of the head coach is 75 m, and the distance between the outlet surface and the nose of the tail coach is 150 m. The aerodynamic forces are almost stable when the length, width, and length of the domain are 375.4 m, 90 m, and 60 m, respectively. Therefore, that domain was chosen.

Table 2 Effect of aerodynamic forces on domain

Domain (m)			F_y (kN)		F_z (kN)	
L	W	H	Head	Tail	Head	Tail
75+150	30+40	30	-48.47	-16.34	7.63	11.97
75+200	30+50	40	-47.35	-15.42	6.52	11.02
100+200	30+60	60	-47.22	-15.25	6.38	10.83

Table 3 shows the effect of aerodynamic forces on turbulent models including standard $k-\varepsilon$, re-normalization group (RNG) $k-\varepsilon$, realizable $k-\varepsilon$, standard $k-\omega$, and shear stress transports (SST) $k-\omega$ models. It is shown that the differences between standard $k-\varepsilon$ model and the other models are small except the standard $k-\omega$ model. Therefore, the standard $k-\varepsilon$ model was chosen.

Table 3 Effect of aerodynamic forces on turbulence models

Method	F_y (kN)			F_z (kN)	
	Head	Mid	Tail	Head	Tail
Standard $k-\varepsilon$	-47.22	-8.62	-15.25	6.38	10.83
RNG $k-\varepsilon$	-47.02	-8.65	-15.14	6.32	10.91
Realizable $k-\varepsilon$	-47.16	-8.56	-15.27	6.08	10.92
Standard $k-\omega$	-48.20	-9.65	-15.77	5.79	10.54
SST $k-\omega$	-47.22	-8.61	-15.37	6.09	10.92

The time step sizes in CFD and vehicle-track dynamics are 2.0×10^{-3} s and 5.0×10^{-5} s, respectively. Calculations were performed using 4 CPUs of X5650 on a DELL 7500 mainframe. Approximately 30 time step iterations per hour were achieved for the current meshes.

The vector of aerodynamic load \hat{F}_a loaded to the vehicle-track model is described as

$$\hat{F}_a(t) = \begin{cases} F_a(t), & t \geq t_0, \\ \frac{t}{t_0} F_a(t), & t < t_0, \end{cases} \quad (7)$$

where F_a is the vector of aerodynamic forces, t_0 is a constant and $t_0=4.5$ s.

5 Numerical simulation

The calculation was performed for a high-speed train at $u_t=350$ km/h and subjected to crosswind $u_w=13.8$ m/s.

5.1 Aerodynamics and displacements

In this section, we describe the aerodynamic characteristics and displacements of the train subjected to crosswind.

5.1.1 Head coach

Figs. 6a–6j show a comparison of the responses of the head coach calculated by off-line simulation and co-simulation methods. When the interaction between airflow and a high-speed train is considered, the changes are as follows:

1. The magnitude of the side force increases by approximately 5 kN, which is over 10% greater than that calculated by the off-line simulation method. The magnitude of the lateral displacement increases by approximately 15 mm.

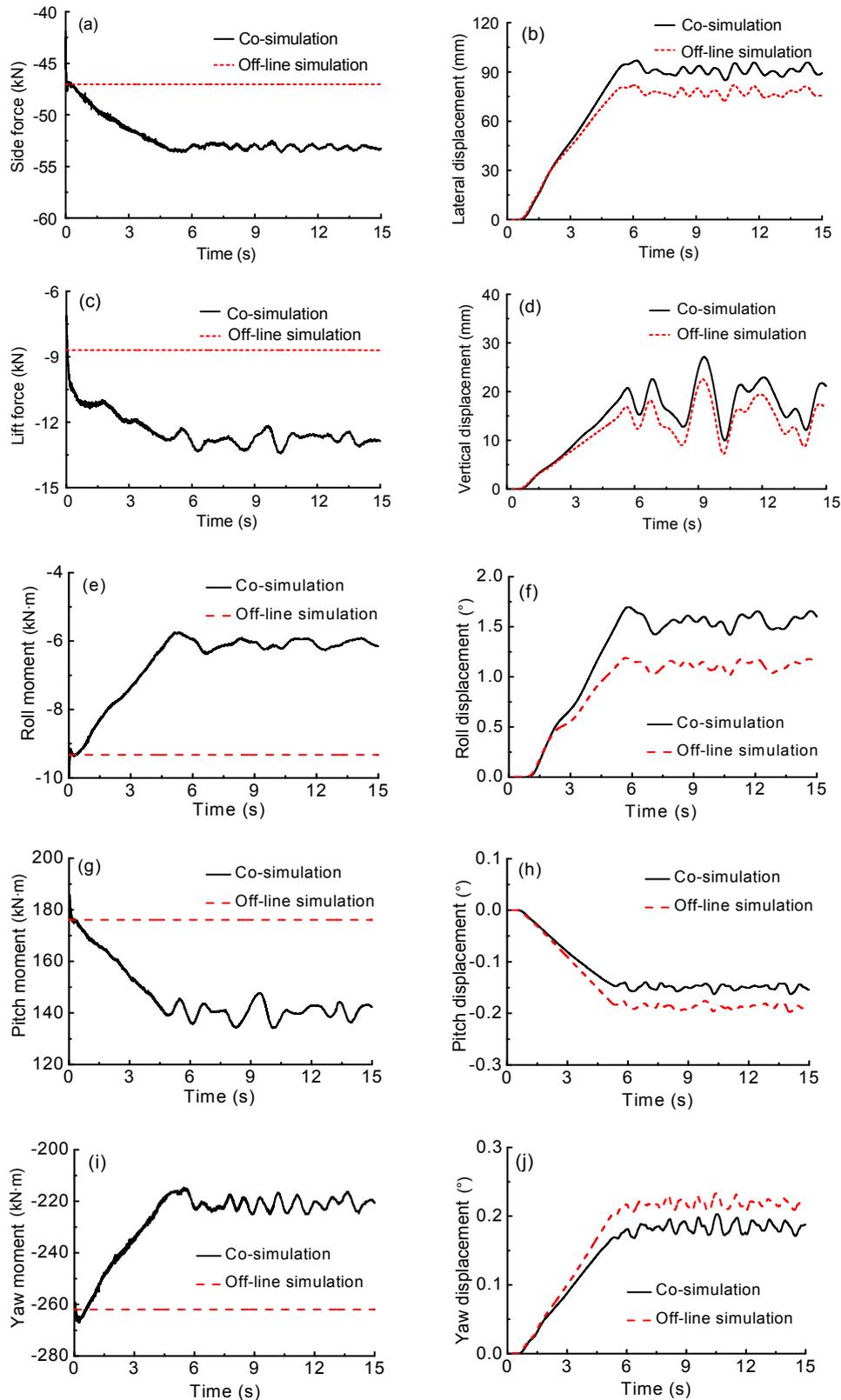


Fig. 6 Responses of the head coach calculated by off-line simulation and co-simulation methods
 (a) Side force; (b) Lateral displacement; (c) Lift force; (d) Vertical displacement; (e) Roll moment; (f) Roll displacement;
 (g) Pitch moment; (h) Pitch displacement; (i) Yaw moment; (j) Yaw displacement

2. The magnitude of the lift force and the vertical displacement increases by approximately 4 kN and 6 mm, respectively. The trends are consistent because the coordinate systems of the vehicle-track coupling dynamics and the aerodynamics are different in the y direction.

3. The magnitude of the roll moment decreases by approximately 3.5 kN·m. The variation trend of the roll moment depends on the reference point of the moment. However, the magnitude of the roll displacement increases by approximately 0.3° , which is over 25% greater than that calculated by the off-line simulation method.

4. The magnitude of the pitch moment and the pitch displacement decreases.

5. The magnitude of the yaw moment and the yaw displacement decreases.

Baker *et al.* (2004) conducted that the magnitude of side and lift forces would increase with the consideration of the rolling motion of the carbody. The trends in the numerical results in this study are consistent with those of Baker *et al.* (2004)'s experiments.

The magnitude of the side force and the roll moment is closely related to pressure differences between windward and leeward sides of the train. Figs. 7a and 7b show the pressure differences along the vertical dimension of the head coach, where d indicates the longitudinal distance between the cross-section and nose. There are two cross-sections: one at $d=5$ m located in the streamlined nose and the other one at $d=18$ m located in the non-streamlined region. Pressure differences at almost all vertical positions are higher in the co-simulation as the pressure on the windward side of the head coach increases. Therefore, the magnitude of the side force of the head coach increases by 10%. Consequently, the magnitude of the roll moment of the head coach increases.

The magnitude of the lift force is closely related to pressure differences between the top and bottom of the train. Figs 8a and 8b show pressure differences along the lateral dimension of the head coach. The pressure on the bottom of the head coach increases because of the rolling motion of the train body. The integral of pressure differences is greater in the co-simulation. As a result, the magnitude of the lift force increases.

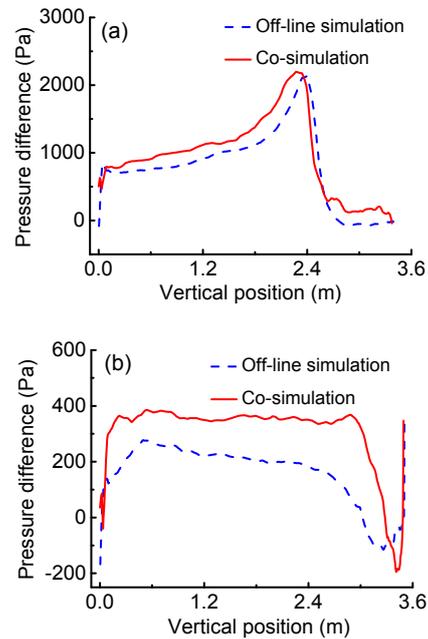


Fig. 7 Pressure differences along the vertical dimension of the head coach: $d=5$ m (a) and $d=18$ m (b)

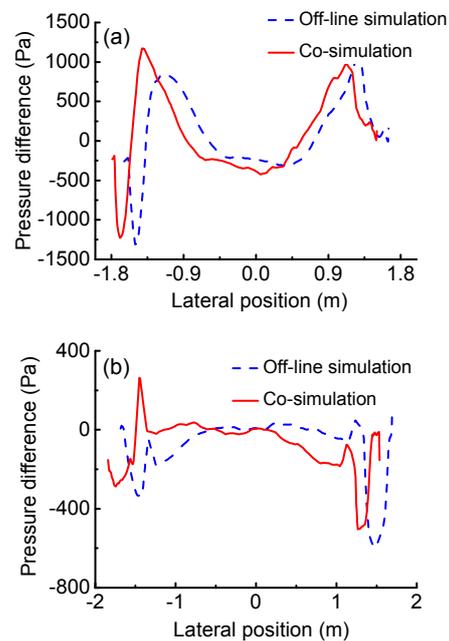


Fig. 8 Pressure differences along the lateral dimension of the head coach: $d=5$ m (a) and $d=18$ m (b)

5.1.2 Middle coach

Figs. 9a–9j show a comparison of the responses of the middle coach calculated by off-line simulation and co-simulation methods. When the interaction

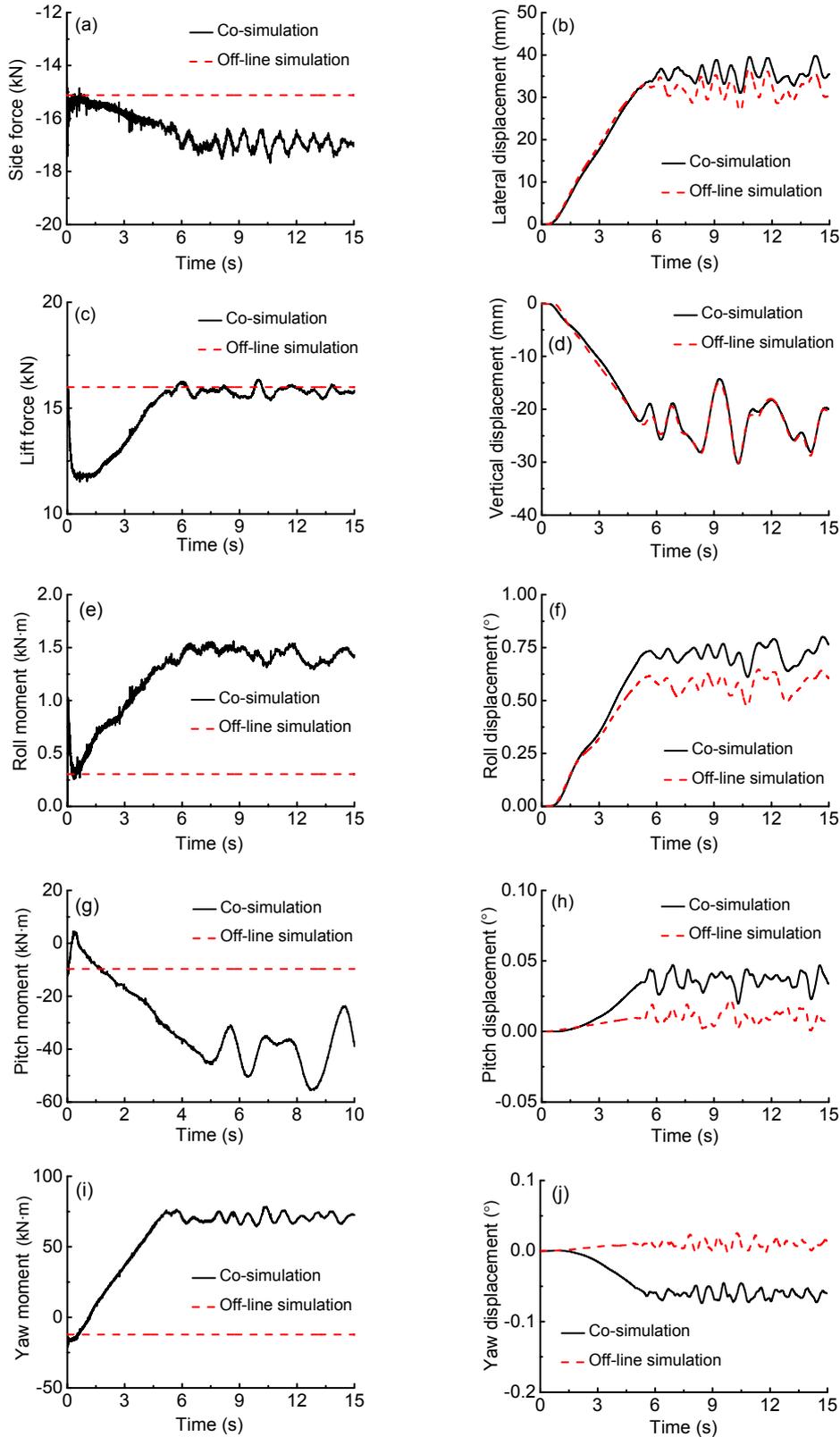


Fig. 9 Responses of the middle coach calculated by off-line simulation and co-simulation methods
 (a) Side force; (b) Lateral displacement; (c) Lift force; (d) Vertical displacement; (e) Roll moment; (f) Roll displacement;
 (g) Pitch moment; (h) Pitch displacement; (i) Yaw moment; (j) Yaw displacement

between airflow and a high-speed train is considered, the changes are as follows:

1. The magnitude of the side force and the lateral displacement increases by approximately 2 kN and 5 mm, respectively.

2. The magnitude of the lift force and the vertical displacement changes slightly.

3. The magnitude of the roll moment and the roll displacement increases by approximately 0.5 kN·m and 0.15°, respectively.

4. The magnitude of both the yaw and pitch moments increases.

The pressure on two different cross-sections of the middle coach is in agreement because of the steady flow field around the middle coach. The pressure on the windward side of the middle coach almost increases and the pressure on the leeward side almost decreases. It is seen that the magnitude of the side force on the middle coach increases. According to Figs. 10a and 10b, pressure differences along the lateral dimension increase and the magnitude of the lift force on the middle coach decreases to some extent.

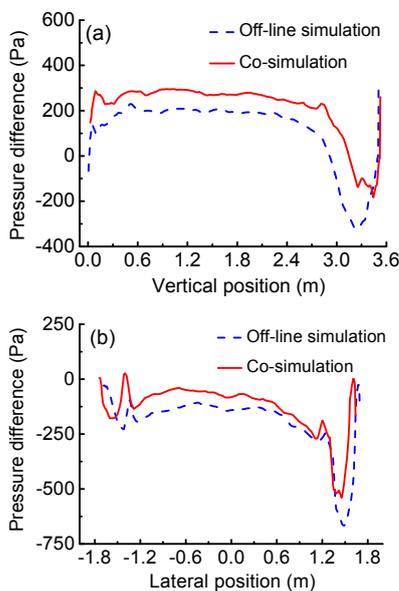


Fig. 10 Pressure differences along vertical and lateral dimensions of the middle coach: vertical (a); lateral (b)

5.1.3 Tail coach

Figs. 11a–11j show a comparison of the responses of the tail coach calculated by off-line simulation and co-simulation methods. When the interaction between airflow and a high-speed train is considered, the changes are as follows:

1. The magnitude of the side force and the lateral displacement increases by approximately 3 kN and 10 mm, respectively. Besides, the direction of the side force is opposite to those of the head and middle coaches.

2. The magnitude of the lift force increases and the magnitude of the vertical displacement increases to some extent.

3. The magnitude of the roll moment decreases; however, the magnitude of the roll displacement increases by approximately 0.3°.

4. The magnitude of the yaw and pitch moments decreases. Correspondingly, the magnitude of the yaw and pitch displacements decreases.

In the streamlined region, pressure differences between windward and leeward sides are much less than zero. Therefore, the direction of the side force on the tail coach is windward. Moreover, the pressure on the windward side of the tail coach increases. Figs. 12a and 12b show pressure differences along the vertical dimension of the tail coach. There are two cross-sections: one at $d=65$ m located in the non-streamlined region and the other at $d=72.5$ m located in the streamlined nose. In the non-streamlined region, pressure differences at almost all vertical positions are greater in the co-simulation. Figs. 13a and 13b show pressure differences along the lateral dimension of the tail coach at different cross-sections. In the streamlined region, the pressure differences are smaller in the co-simulation. As a result, the magnitude of the lift force increases.

5.2 Dynamic performances of vehicle-track

In this section, we describe the running safety of the train subjected to crosswind. Table 4 shows comparisons of the displacement calculated by different simulation methods. Displacements of the train include the lateral displacement y , the vertical displacement z , the roll displacement θ , the yaw displacement ψ , and the pitch displacement β . The values given in the table are the maximum or minimum values of the indexes. The lateral displacements of the head and middle coaches are toward the leeward side, which are opposite to that of the tail coach. Each component of the performance indexes of the head coach is the largest among the three coaches. Besides, the magnitude of displacements increases when the interaction is considered.

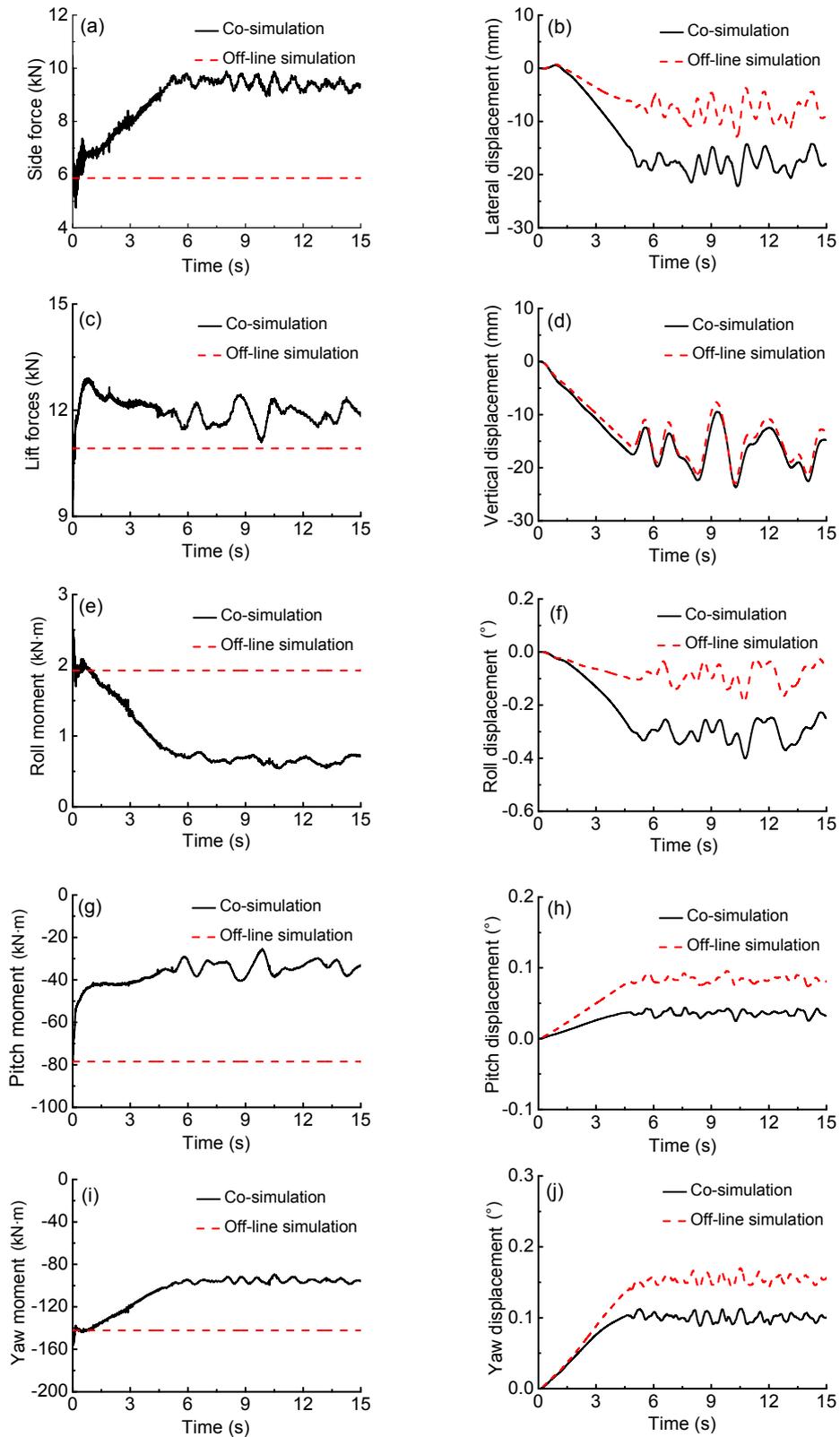


Fig. 11 Responses of the tail coach calculated by off-line simulation and co-simulation methods
 (a) Side force; (b) Lateral displacement; (c) Lift force; (d) Vertical displacement; (e) Roll moment; (f) Roll displacement;
 (g) Pitch moment; (h) Pitch displacement; (i) Yaw moment; (j) Yaw displacement

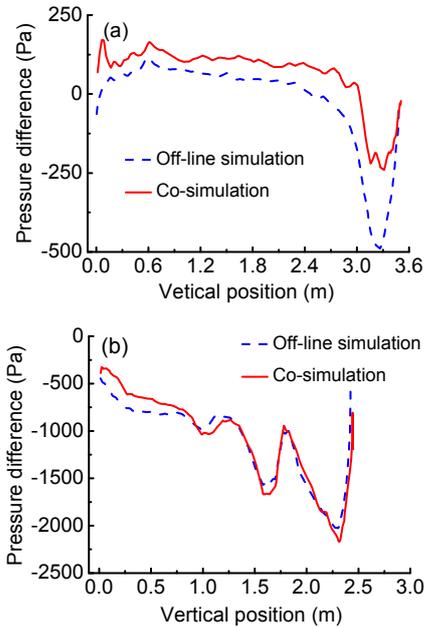


Fig. 12 Pressure differences along the vertical dimension of the tail coach: $d=65$ m (a) and $d=72.5$ m (b)

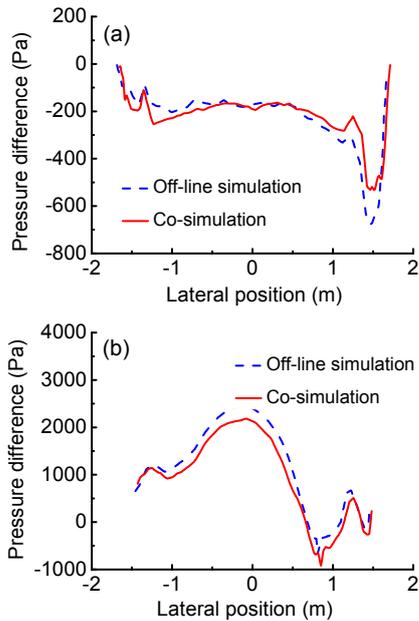


Fig. 13 Pressure differences along the lateral dimension of the tail coach: $d=65$ m (a) and $d=72.5$ m (b)

The most important indexes of vehicle-track dynamics are safety indexes, including the wheel/rail vertical force, the lateral wheelset force, the derailment coefficient, and the wheel unloading rate. Table 5 shows comparisons of safety indexes calculated by different simulation methods. Among the three coaches, the head coach shows the largest increments in the safety indexes. The magnitude of the wheel

unloading rate increases. The running safety of the train becomes worse with the consideration of the rolling motion of the carbody. Besides, the magnitude of the wheel set unloading rate and the derailment coefficient of the head coach increase by approximately 0.14 and 0.02, respectively.

Figs. 14a and 14b show a comparison of the accelerations of the head coach calculated by different simulation methods. There is a slight difference in accelerations of the head coach.

Table 4 Comparisons of displacements calculated by different simulation methods

Train type	Method	y (mm)	z (mm)	θ (°)	β (°)	ψ (°)
Head	Off-line simulation	82.03	22.52	1.17	-0.16	0.23
	Co-simulation	95.33	27.14	1.65	-0.19	0.20
Middle	Off-line simulation	36.87	-30.17	0.65	0.04	0.02
	Co-simulation	39.53	-30.27	0.79	0.02	-0.07
Tail	Off-line simulation	-12.88	-7.55	-0.19	0.09	0.17
	Co-simulation	-22.18	-9.48	-0.40	0.04	0.11

Table 5 Comparisons of safety indexes calculated by different simulation methods

Train type	Method	Wheel/Rail vertical force (kN)	Lateral wheelset force (kN)	Derailment	Wheel unloading
Head	Off-line simulation	92.80	28.69	0.32	0.65
	Co-simulation	96.40	32.84	0.34	0.79
Middle	Off-line simulation	77.51	13.32	0.19	0.44
	Co-simulation	85.32	15.20	0.20	0.45
Tail	Off-line simulation	73.95	12.30	0.17	0.39
	Co-simulation	81.92	13.89	0.19	0.40

6 Conclusions

A numerical approach to the interaction between airflow and a high-speed train is presented in this paper.

1. The interaction between airflow and a high-speed train significantly affects displacements and aerodynamic forces of the train subjected to crosswind.
2. The running safety of the train subjected to crosswind deteriorates when the interaction between airflow and a high-speed train is considered; however, there is a slight difference in accelerations of the head coach.

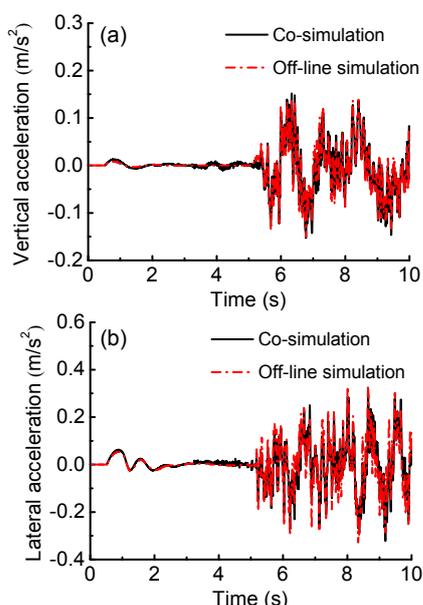


Fig. 14 Vertical (a) and lateral (b) accelerations of the head coach

3. Among the three coaches, each component of the dynamic performance indexes of the head coach is the largest, and the head coach shows the largest increments in the safety indexes.

4. It is necessary to consider the interaction between airflow and a high-speed train subjected to crosswind.

References

- Baker, C.J., 1991. Ground vehicles in high cross winds part III: The interaction of aerodynamic forces and the vehicle system. *Journal of Fluids and Structures*, **5**(2):221-241. [doi:10.1016/0889-9746(91)90478-8]
- Baker, C.J., 2010. The simulation of unsteady aerodynamic crosswind forces on trains. *Journal of Wind Engineering and Industrial Aerodynamics*, **98**(2):88-99. [doi:10.1016/j.jweia.2009.09.006]
- Baker, C.J., Jones, J., Lopez-Calleja, F., Munday, J., 2004. Measurements of the cross wind forces on trains. *Journal of Wind Engineering and Industrial Aerodynamics*, **92**(7-8):547-563. [doi:10.1016/j.jweia.2004.03.002]
- Baker, C.J., Hemida, H., Iwnicki, S., Xie, G., Ongaro, D., 2011. Integration of crosswind forces into train dynamic modelling. *Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit*, **225**(2):154-164. [doi:10.1177/2041301710392476]
- Bocciolone, M., Cheli, F., Corradi, R., Muggiasca, S., Tomasini, G., 2008. Crosswind action on rail vehicles: Wind tunnel experimental analyses. *Journal of Wind Engineering and Industrial Aerodynamics*, **96**(5):584-610. [doi:10.1016/j.jweia.2008.02.030]
- Cheli, F., Ripamonti, F., Rocchi, D., Tomasini, G., 2010. Aerodynamic behaviour investigation of the new EMUV250 train to cross wind. *Journal of Wind Engineering and Industrial Aerodynamics*, **98**(4-5):189-201. [doi:10.1016/j.jweia.2009.10.015]
- Chiu, T.W., 1995. Prediction of the aerodynamic loads on a railway train in a cross-wind at large yaw angles using an integrated two- and three-dimensional source/vortex panel method. *Journal of Wind Engineering and Industrial Aerodynamics*, **57**(1):19-39. [doi:10.1016/0167-6105(94)00099-Y]
- Diedrichs, B., 2003. On computational fluid dynamics modeling of crosswind effects for high-speed rolling stock. *Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit*, **217**(3):203-226. [doi:10.1243/095440903769012902]
- Diedrichs, B., Sima, M., Orellano, A., Tengstrand, H., 2007. Crosswind stability of a high-speed train on a high embankment. *Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit*, **221**(2):205-225. [doi:10.1243/0954409JRRT126]
- Ding, Y., Sterling, M., Baker, C.J., 2008. An alternative approach to modeling train stability in high cross winds. *Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit*, **222**(1):85-97. [doi:10.1243/09544097JRRT138]
- Khier, W., Breuer, M., Durst, F., 2000. Flow structure around trains under side wind conditions: a numerical study. *Computers & Fluids*, **29**(2):179-195. [doi:10.1016/S0045-7930(99)00008-0]
- Li, T., Zhang, J.Y., Zhang, W.H., 2011a. Performance of vehicle-track coupling dynamics under crosswinds. *Journal of Traffic and Transportation Engineering*, **9**:55-60 (in Chinese).
- Li, T., Zhang, J.Y., Zhang, W.H., 2011b. Nonlinear characteristics of vortex-induced vibration at low Reynolds number. *Communications in Nonlinear Science and Numerical Simulation*, **16**(7):2753-2771. [doi:10.1016/j.cnsns.2010.10.014]
- Orellano, A., Schober, M., 2006. Aerodynamic Performance of a Typical High-speed Train. Proceedings of the 4th WSEAS International Conference on Fluid Mechanics and Aerodynamics, Elounda, Greece, p.18-25.
- Shao, X.M., Wan, J., Chen, D.W., Xiong, H.B., 2011. Aerodynamic modeling and stability analysis of a high-speed train under strong rain and crosswind conditions. *Journal of Zhejiang University-SCIENCE A (Applied Physics & Engineering)*, **12**(12):964-970. [doi:10.1631/jzus.A11GT001]
- Suzuki, M., Tanemoto, K., Maeda, T., 2003. Aerodynamic characteristics of train/vehicles under cross winds. *Journal of Wind Engineering and Industrial Aerodynamics*, **91**(1-2):209-218. [doi:10.1016/S0167-6105(02)00346-X]
- Thomas, D., Diedrichs, B., Berg, M., Stichel, S., 2010. Dynamics of a high-speed rail vehicle negotiating curves at unsteady crosswind. *Proceedings of the Institution of Mechanical Engineers, Part F: Journal of Rail and Rapid Transit*, **224**(6):567-579. [doi:10.1243/09544097JRRT335]
- Xu, Y.L., Ding, Q.S., 2006. Interaction of railway vehicles with track in cross-winds. *Journal of Fluids and Structures*, **22**(3):295-314. [doi:10.1016/j.jfluidstructs.2005.11.003]
- Zhai, W.M., Cai, C.B., Guo, S.Z., 1996. Coupling model of vertical and lateral vehicle/track interactions. *Vehicle System Dynamics*, **26**(1):61-79. [doi:10.1080/00423119608969302]